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Comparative Studies of Carbon Materials Synthesized from Waste as Catalysts for Ozonation of Real Textile Wastewater

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Abstract

In the present work, evaluation of two catalysts, Activated carbon (AC) synthesized from agricultural waste and Multiwalled carbon nanotubes (MWCNT) synthesized from plastic waste, were done for the ozonation of real textile wastewater using *para*- chloro benzoic acid (*p*-CBA) as a probe compound. The effect of pH and catalyst dose were studied in terms of •OH exposure, Rct, rate of *p*-CBA degradation and ozone degradation. The rate constant for the reaction of organic matter with hydroxyl radicals was determined using competition kinetics. The threshold ozone dose for real textile wastewater was found to be 0.51 gm/gm of TOC. With an increase in specific ozone dose, the rate of *p*-CBA degradation was found to be increasing and has shown a positive effect on •OH exposure and Rct. The increasing pH had shown a positive effect on the rate of degradation and decomposition of *p*-CBA and ozone respectively in the case of AC catalyzed ozonation. A similar trend was observed in the case of MWCNTs catalyzed ozonation. A positive effect of pH was observed on •OH exposure and Rct, in AC as well as MWCNTs catalyzed ozonation. The effect of catalyst loading has shown significant enhancement in *p*-CBA degradation, ozone decomposition, •OH exposure and Rct in both AC as well as MWCNTs catalyzed ozonation. However, MWCNTs have proved better than AC as a catalyst for ozonation in studied experimental parameters.

Key words: Activated carbon, Multiwalled carbon nanotubes, Ozonation, •OH exposure, Specific ozone dose

1 Introduction

Ozone (O₃), a powerful oxidant capable of reacting with organic and inorganic compounds, has been widely applied for water and wastewater treatment (Bielski et al. 1985, Hoigné, 1998). The transformation of organic pollutants with ozone occurs via direct reaction with molecular ozone or with hydroxyl radicals (•OH) resulting from ozone decomposition in water [von Gunten, 2003]. Molecular ozone has a limitation of selectively reacting with organic pollutants having single bonds and aromatics substituted with electron withdrawing groups (Langlais et al. 1991). To overcome the limitation of molecular ozone, advanced

37 oxidation processes (AOPs) based enhanced formation of •OH radicals have been developed
38 (Glaze et. al.1987). Ozone goes through chain reactions and forms several secondary
39 oxidants, prominently, hydroxyl radical, a strongest and most non selective oxidant in water.
40 It readily attacks most of the organic pollutants and converts them into less complex and less
41 harmful intermediate products (Langlais et. al. 1991). In recent times, catalytic ozonation has
42 proven to be an effective technique for aqueous pollutant degradation (Kasprzyk-Hordern et.
43 al.2003). In 1970, heterogeneous catalytic ozonation was likely presented (Chen et. al.1977).
44 Heterogeneous ozonation offers certain favourable circumstances over homogeneous
45 ozonation, for example, cleaner process, independent of additional stoichiometric reagents
46 (Fan et. al. 2014.). Carbon materials, for example, activated or synthetic carbons, have been
47 considered for catalytic ozonation since the 1990s (Jans and Hoigné 1998). Because of
48 supportive properties of carbon materials like ready at a lower price, availability of several
49 pores structures and no metal leaching from synthetic carbon, these materials turned into an
50 attractive alternative for catalytic ozonation. (Fan et.al.2014). The integrated utilization of
51 ozone and activated carbon (AC) has been widely researched by Jans and Hoine (Jans and
52 Hoigné 1998) to eliminate toxic and low biodegradable compounds from water. The process
53 amalgamates the calibre of high oxidative strength of ozone and transformation of ozone into
54 hydroxyl radicals by AC, which can degrade aqueous organic compounds. Numerous
55 aqueous compounds have been successfully degraded by AC catalyzed ozonation. (Fontanier
56 et al.2005, Rodrguez et al. 2008). Nanostructured carbon materials, for example, nanotubes
57 and nanofibres, have diverse surface properties when contrasted with particulate carbon
58 materials, for example, activated carbon. Carbon nanotubes display a great capacity to adsorb
59 compounds from water. (Chiang and Wu, 2010, Yu et. al.2011) The major limitation of AC
60 in liquid media is the diffusion of solute in its micro pores may be very slow; it can be even
61 more disastrous in aqueous media due to the hydrophobic nature of the carbon surface. In
62 contrast, the mesoporus nature of nanocarbon material facilitates diffusion through pore
63 network. (Job et.al. 2006). In literature, there are a few studies reported on multiwalled
64 carbon nanotube (MWCNT) as a very promising material for catalytic ozonation. MWCNT
65 of commercial grade was used in catalytic ozonation of oxalic acid, (Liu et.al.2009) SMX,
66 (Goncalves et al.2012) bezafibrate (Goncalves et. al.2013) and atrazine (Fan et. al. 2014)
67 successfully.

68 The hydroxyl radical concentration is a crucial parameter for determination of the reaction
69 rate. Due to the low concentration of hydroxyl radicals, its quantitative measurement is rather
70 difficult. On the contrary, ozone concentration can be measured by several methods.
71 (Langlais et al. 1999) For the prediction of hydroxyl radical concentration, a few computer
72 models have been developed.(Chelkowska et al. 1992) An indirect method, using para
73 chlorobenzoic acid (p-CBA), was developed by Elovitz and von Gunten (Elovitz and Von
74 Gunten 1999). Up to recent times, several studies have been conducted to evaluate the
75 effectiveness of AOPs like O₃+ UV, O₃/H₂O₂, O₃/ H₂O₂/UV in terms of hydroxyl radical
76 generation. Most of the studies used municipal wastewater. (Wert et al. 2009, Lee et al. 2013,
77 Lee et al. 2014, Guo et al.2018, Liu et al. 2019, Liu et al. 2020),hospital wastewater (Lee et.
78 al. 2014) and industrial wastewater (Liu et. al. 2020). Very few studies have evaluated
79 catalytic performance for hydroxyl radical generation. (Ahn et al.2017, Guo et al.2018, Guo

80 et al.2019, Guo et al.2020). There are no studies reported on evaluation of catalytic
81 performance for hydroxyl radical generation in industrial wastewater. In this study, the textile
82 industry wastewater was used to evaluate the effectiveness of activated carbon and
83 multiwalled carbon nanotubes for hydroxyl radical generation. The effect of different
84 parameters such as catalyst, ozone dose, and pH were studied. The total scavenging rate of
85 hydroxyl radicals was evaluated. This study is an attempt to portray a real time picture of
86 hydroxyl radial generation in industrial wastewater with activated carbon and multiwalled
87 carbon nanotubes.

88 **2 Materials and Method**

89 **2.1 Water Sampling**

90 A wastewater effluent sample was collected from the equalization tank of the textile industry
91 near Nagpur district, Maharashtra, India. The sample was used without any dilution or
92 additional filtration prior to ozonation experiments. The sample was kept in a refrigerator at
93 4⁰ C before further usage.

94 **Table 1: Characterization of textile wastewater**

95 **2.2 Analytical methods**

96 The ozone concentrations in the stock solution were determined by the indigo method.
97 Concentrations of hydroxyl radicals probe compound *p*-chlorobenzoic acid (*p*-CBA) were
98 determined by high performance liquid chromatography (HPLC) with reverse phase column
99 and UV-Vis wavelength detector.

100 **2.3 Experimental set-up**

101 A fresh ozone stock solution (50-60 mgL⁻¹) was prepared by bubbling ozone gas into a one
102 litre gas washing bottle which was ice cooled and contained demineralised water. The ozone
103 gas was generated using ozone generator (Faraday Ozone, India). The catalyst solutions were
104 prepared in wastewater samples with varying concentrations of catalyst and adjusted to pH 5,
105 7, 8 and 9 using 0.1 N H₂SO₄ and NaOH. The desired ozone dose was achieved by varying
106 ratios of sample and stock solution. The initial concentration of *p*-CBA was 1 μM.

107 **2.4 Preparation of Activated carbon**

108 *Cajanus cajan* husk was obtained from the pulse processing industry in Nagpur. It was
109 washed with water and double distilled water to remove dust particles. It was then dried to
110 remove moisture content in a hot air oven at about 110⁰C for 8 hrs. It was crushed and sieved
111 so as to get particles in the size range of 50 to 100 μm. Then it was carbonized in a muffle
112 furnace at about 450⁰C for 4 hours. It was treated with concentrated hydrochloric acid to
113 remove ash from carbon. The pH was brought to 7 by repeated washing of carbon using
114 distilled water. Then it was dried in a hot air oven at 110⁰ C for 8 hrs to remove the moisture
115 content. It was activated by treating it with conc. sulfuric acid at the ration of 1:10 (wt.of

116 carbon/volume of sulfuric acid) for 10 hrs. The mixture was filtered and the filtrate was
117 repeatedly washed with double distilled water to bring the pH to 7. To remove the moisture
118 content, it was dried in a hot air oven at 110⁰C for 4 hrs. Then it was heated in a muffle
119 furnace at 800⁰C for 2 hours for activation. The scanning electron microscopy image of
120 activated carbon is shown in fig. 1 and the XRD patterns of AC are as shown in fig. 2. The
121 SEM image of activated carbon (AC) shows a plate-like structure with an average thickness
122 of 1-2 micrometers. The SEM image indicates no specific shape and size of materials, i.e.
123 uneven shape and size distribution. The diameters of MWCNTs range from 15.5-22.5 nm in
124 SEM images. It is difficult to determine the % purity of MWCNTs from SEM image. The
125 catalyst appears at the tip of the MWCNTs. The HRTEM analysis shows well aligned
126 graphene walls of around 25-35 with 2-3 nm inner diameters. The XRD scan of AC
127 corresponds to its SEM image showing a high amount of noise which resembles an uneven
128 size and shape. The XRD peak corresponds with carbon peak $2\theta = 26.26$ (At (002) plane).
129 The smooth curve in the XRD pattern indicates high amorphous material. The XRD patterns
130 show a well resolved peak similar to AC for graphite at $2\theta = 26.62$ and indicates the absence
131 of amorphous carbon and asserts the formation of MWCNTs.

132 Fourier transform infrared spectroscopy (FTIR) and Brunauer-Emmet-Teller (BET) for
133 surface morphology are available in the literature. (Bhusari et al.2020)

134 **Figure 1: SEM image of Activated carbon**

135 **Figure: 2 XRD Pattern for Activated Carbon**

136

137 **2.5 Preparation of Multiwalled carbon nanotubes**

138 The MWCNTs were synthesized from polypropylene (PP) bottles used for packing
139 chemicals. The small pieces of PP at an approximate size of 1cm × 1cm were made from
140 cleaned bottles of PP. The mixture of shredded PP and the desired amount of Ni/Mo/MgO
141 catalyst was taken into a silica crucible covered with a lid and kept in an electrically heated
142 muffle furnace at the desired temperature. The red hot crucible was removed from the furnace
143 after 10 min. and was cooled to room temperature. To remove the catalyst particles, the
144 synthesized MWCNTs were ultrasonicated with concentrated hydrochloric acid for 30 mins.
145 By oxidising MWCNTs in a muffle furnace at 400⁰C for 2 hrs, the amorphous carbon in the
146 product was removed. The XRD patterns show a well resolved peak for graphite at $2\theta =$
147 26.62 which indicates absence of amorphous carbon and asserts formation of MWCNTs. The
148 diameters of MWCNTs range from 15.5-22.5 nm in SEM images. It is difficult to determine
149 the purity of MWCNTs from SEM images. The catalyst appears at the tip of the MWCNTs.
150 The HRTEM analysis shows well aligned graphene walls of around 25-35 with 2-3 nm inner
151 diameters. The preparation and characterization of multiwalled carbon nanotubes is discussed
152 in the literature (Bajad et.al.2015). The BET surface area of MWCNTs is 28.5 Sq.m./gm.

153 **3 Results and Discussions**

154 **3.1 Ozone and •OH Exposure**

155 The ozone exposures were calculated from the area under the ozone decay curves. (von
 156 Gunten and Hoigne 1994). The Indigo method was used to determine the residual ozone.
 157 (Bader and Hoigne, 1981). *p*CBA (para-chlorobenzoic acid) is usually used as a probe
 158 compound due to its low apparent second order reaction rate constant with ozone (< 0.1 M⁻¹
 159 s⁻¹) and its high reaction rate with •OH (5.0×10⁹ M⁻¹ s⁻¹)(von Sonntag and von Gunten
 160 2012, Rosenfeldt and Linden 2007) The •OH exposure is calculated by equation 1:

$$\int \bullet\text{OH} dt = \frac{\ln[p\text{CBA}]_0 - \ln[p\text{CBA}]}{k_{\bullet\text{OH},p\text{CBA}}} \quad (1)$$

163
 164 The Rct represents a dimensionless number comparing the potential for oxidation by •OH to
 165 the potential for oxidation by O₃. The Rct value is not just the ratio of •OH exposure to O₃
 166 exposure as shown in equation 2, but it is the ratio of total initiation capacity to total
 167 inhibition capacity in a system.(Yong and Lin 2012).

$$\text{Rct} = \frac{\int [\bullet\text{OH}] dt}{\int [\text{O}_3] dt} \quad (2)$$

169 At different reaction times, the measured concentration in the experimental solutions was
 170 calculated. Ozone exposures at specific ozone doses are shown in fig.3A. With increasing
 171 specific ozone dose, the ozone exposure increases during ozonation. The ozone exposure was
 172 (0.625-3.3)*10⁻³ M s for the textile wastewater. At a lower specific ozone dose of 0.3 gm
 173 O₃/gm TOC, it was not possible to measure ozone exposure. It seemed that ozone was rapidly
 174 decomposed during instantaneous ozone demand (IOD) or consumed by water matrix. At
 175 different specific ozone doses, the ozone decay was completed within ≤15 min.

176 It can be seen from fig.3A, that •OH Exposure increases with an increase in specific ozone
 177 dose. It shows a linear relation of ozone exposure and specific ozone dose (R²=0.94) which is
 178 agreement with (Audenaert et.al.2013). The •OH Exposure increased from 0.04*10⁻¹⁰ to
 179 1.4*10⁻¹⁰ for an increment of specific ozone dose of 0.5 to 1.5 gm O₃/gm TOC. From the
 180 linear regression, it was possible to determine the threshold ozone dose. The intercept of the
 181 linear line represents the value of threshold ozone dose, for which little •OH is formed from
 182 ozone consumption in wastewater effluent. [Lee et.al.2013] Fig.3B shows the *p*-CBA
 183 degradation at different specific ozone doses. The *p*-CBA degradation increased from 5 to
 184 62%, for an increase in specific ozone dose of 0.5 to 1.5 gm O₃/gm TOC. As shown in fig.1B,
 185 the *p*-CBA degradation increases from 2% at a specific ozone dose of 0.5 to 51% at a specific
 186 ozone dose of 1.5 gm O₃/gm TOC. At higher ozone dose, decreased *p*-CBA concentration
 187 indicates that ozone dose is a significant factor influencing •OH exposure. As mentioned in
 188 Table 2, Rct value increases about 2.74 times at the highest specific ozone dose when
 189 compared with the lowest specific ozone dose. Fig. 3C, shows the effect of specific ozone
 190 dose on the rate of *p*-CBA degradation. With an increase in specific ozone dose, the rate of *p*-

191 CBA degradation increases. When the specific ozone dose was increased from 0.5 to 1.5 gm
192 ozone/ gm TOC, the rate of *p*-CBA degradation was observed to increase from 0.002 to 0.022
193 min⁻¹ i.e. nearly 11 times increment in rate constant was observed. The increased specific
194 ozone dose enhances the availability of ozone, which can be further decomposed in to •OH
195 and promotes *p*-CBA degradation.

196 **Figure 3:(A) Effect of specific ozone dose on •OH exposure (B) Effect of specific ozone**
197 **dose on *p*-CBA degradation (C) Effect of specific ozone dose on rate of *p*-CBA**
198 **degradation**

199 **Table 2: Effect of specific ozone dose on Rct, ozone and •OH Exposure**

200

201 **3.2 Effect of pH on the performance of catalytic ozonation**

202 The value pH plays a vital role in the decomposition of ozone in the aqueous system. In
203 aqueous systems, the chain reaction transforms O₃ into •OH. The pH can accelerate the
204 initiation of the chain reaction. The role of initiator, promoters and inhibitors can be played
205 by several compounds.(Staelin and Hoigne,1985). The formation of •O₂⁻ is due to the
206 initiator. The promoters are attributed to the regeneration of •O₂⁻ ions from hydroxyl radicals
207 and the inhibitor compounds are capable of consuming hydroxyl radicals without
208 regeneration of superoxide anions. The *p*-CBA degradation depends on ozone decomposition.
209 Therefore, *p*-CBA degradation is an indirect measure of ozone decomposition. In the case of
210 AC catalyzed ozonation, an increase in pH level from 5 to 9, observed 25 to 60% increment
211 in *p*-CBA degradation and •OH exposure increased from 5.75*10⁻¹¹ to 1.83*10⁻¹⁰ M.s as
212 shown in Table 3 and fig 4A. The rate constant of *p*-CBA degradation increases from 0.008
213 to 0.030 min⁻¹ depicted in fig. 4B. The MWCNT catalyzed shows a similar trend of an
214 increment in *p*-CBA degradation with an increase in pH level. At pH 5, 30% *p*-CBA removal
215 was observed and was increased to 70% at 9 pH and the corresponding increase in •OH
216 exposure was from 7.13*10⁻¹¹ to 2.40*10⁻¹⁰ M.s as shown in fig. 5A and Table 4. Fig.5B
217 shows that, the rate constant for *p*-CBA degradation was increased nearly five times for pH 9
218 when compared with 5 pH (0.008 to 0.041 min⁻¹). The Rct increment for AC catalyzed
219 ozonation is nearly 29 times i.e. from 1.12*10⁻⁸ to 3.25*10⁻⁷ and in the case of MWCNT
220 catalyzed ozonation, the increment was observed to be nearly 42 times at 9 pH when
221 compared pH level of 5 as shown in Table 3&4 respectively. The positive effect of
222 increasing pH was also observed in the rate of ozone decomposition. Both the catalyst AC
223 and MWNCTs have shown enhancement in ozone decomposition rate constant with
224 increasing pH. In the case of AC, for a change in initial pH from 5 to 9, the corresponding
225 change in ozone decomposition rate is from 0.176 to 0.448 min⁻¹. In the case of MWCNTs,
226 for the same change in pH, decomposition rate changes from 0.163 to 0.491min⁻¹ as shown in
227 figures 4C and 5C respectively. Because there are more hydroxyl ions accessible under basic
228 conditions for launching radical chain reactions, changes in pH can have a direct influence on
229 liquid phase chain reactions. As a result, at higher pH levels, liquid phase reactions triggered
230 by OH⁻ may account for the bulk of the produced hydroxyl radicals.

231 **Figure 4: Effect of pH on (A) *p*-CBA degradation of AC catalyzed ozonation (B) rate of**
232 ***p*-CBA degradation of AC catalyzed ozonation (C) rate of ozone decomposition in AC**
233 **catalyzed ozonation**

234 **Table 3: Effect of pH on Rct , ozone and ·OH Exposure in AC catalyzed ozonation**

235 **Figure 5: Effect of pH on (A) *p*-CBA degradation of MWCNTs catalyzed ozonation (B)**
236 **rate of ozone decomposition of MWCNTs catalyzed ozonation (C) rate of ozone**
237 **decomposition of MWCNTs catalyzed ozonation**

238 **Table 4: Effect of pH on Rct, ozone and ·OH Exposure in MWCNTs catalyzed**
239 **ozonation**

240 **3.3 Effect of catalyst loading**

241 The effect of AC and MWCNTs loading on *p*-CBA degradation is as shown in fig.6A & 6B.
242 The pH was maintained at 9. As the dose of AC increased from 50 to 100 mg, *p*-CBA
243 degradation was observed to increase by 9% and further increment to 200 mg had shown 12
244 % enhancement in *p*-CBA degradation when compared with 50mg dose as shown in fig.6A.
245 The rate of *p*-CBA degradation was observed to increase with an increment in AC dose as
246 depicted in fig 6C. With a fourfold increase in AC dose, i.e., from 50 to 200 mg, the rate of *p*-
247 CBA degradation was observed to enhance by 1.47% times when compared with the 50 mg
248 dose. The ·OH exposure also increases with an increase in AC dose. For increment of AC
249 dose from 50 to 200 mg, the ·OH exposure increased from 1.83×10^{-10} to 2.54×10^{-10} . The
250 corresponding increase in Rct was observed from 3.25×10^{-7} to 1.51×10^{-6} as shown in the
251 table 5.

252 An increment in MWCNTs dose showed enhanced *p*-CBA degradation, increased ·OH
253 exposure and increased Rct. When MWCNTs dose was increased from 50 to 100 mg, *p*-CBA
254 degradation was increased by 4% and further increment of MWCNTs dose to 200 mg
255 resulted in 10% enhancement in *p*-CBA degradation as shown in fig.4B. The rate of *p*-CBA
256 degradation was increased by 1.39 times, for increment of MWCNTs dose from 50 to 200mg,
257 when compared with the 50mg dose as shown in fig.4D. The ·OH exposure was increased
258 from 2.4×10^{-10} to 3.22×10^{-10} for an increment of 50 to 200mg and the corresponding
259 increase in Rct was from 1.497×10^{-8} to 6.42×10^{-7} as shown in the table 6.

260 The ozone decomposition follows pseudo first order kinetics. The rate of ozone
261 decomposition increases with an increase in AC dose. When AC loading was increased from
262 50 to 100mg, the corresponding increase in ozone decomposition rate constant was found to
263 increase from 0.625 to 1.005 min^{-1} and further increase in AC dose to 200mg had shown an
264 ozone decomposition rate of 1.354 min^{-1} in fig.6E. An increase in MWCNTs dose has shown
265 enhancement in ozone decomposition rate constant. For an increase in MWCNTs dose from
266 50 to 100 mg, the rate constant of ozone decomposition increases from 0.638 to 1.354 min^{-1} .
267 Further increment in MWCNTs loading to 200mg, did not show any increment in ozone
268 decomposition rate constant as illustrated in fig 4F. The positive effect of catalyst loading in

269 the case of AC and MWCNTs was observed for % increment of *p*-CBA degradation, rate of
 270 *p*-CBA degradation and rate of ozone decomposition. The enhancement in $\cdot\text{OH}$ exposure and
 271 R_{ct} was also observed with increasing dose of AC and MWCNTs. This is attributed to the
 272 fact that an increase in catalyst dose provides a greater number of surface active sites and
 273 facilitates decomposition of ozone molecules into hydroxyl radicals.

274 **Figure 6: Effect of catalyst loading on(A) *p*-CBA degradation in AC catalyzed ozonation**
 275 **(B) *p*-CBA degradation of MWCNTs catalyzed ozonation (C) rate of *p*-CBA**
 276 **degradation in AC catalyzed ozonation (D) rate of *p*-CBA degradation in MWCNTs**
 277 **catalyzed ozonation (E) rate of ozone decomposition of in AC catalyzed ozonation (F)**
 278 **rate of ozone decomposition of in MWCNTs catalyzed ozonation**

279 **Table 5: Effect of catalyst loading on R_{ct} , ozone and $\cdot\text{OH}$ Exposure in AC catalyzed**
 280 **ozonation**

281

282 3.4 Determination of rate constant for reaction of organic matter with hydroxyl radicals

283 The competition kinetic method (Liu et al. 2019) was used to estimate the rate constant of
 284 reaction of organic matter with hydroxyl radicals, using *p*-CBA as a probe component and t-
 285 butanol as a competitive scavenger

286 The selected wastewater matrix $\ddot{Y}\cdot\text{OH}$ scavenging (k_1) was determined by the steady-
 287 state $\ddot{Y}\cdot\text{OH}$ concentration. The steady-state $\ddot{Y}\cdot\text{OH}$ concentration followed equation 3 and 4
 288 (Liu et. 2019):

$$k = k_{OH,pCBA}[\cdot\text{OH}]_{ss} \quad (3)$$

$$[\cdot\text{OH}]_{ss} = \frac{\alpha_{OH}}{k_a} \quad (4)$$

289

290 Where, is *p*-CBA apparent rate constant of degradation, is the selected wastewater matrix
 291 $\ddot{Y}\cdot\text{OH}$ scavenging rate constant, is the $\ddot{Y}\cdot\text{OH}$ formation rate. $[\cdot\text{OH}]_{ss}$ is the steady-state $\cdot\text{OH}$
 292 concentration.

293 Substituting equation 4 into equation 3 and then inverting both sides' results in:

$$\frac{1}{k} = \frac{k_1}{k_{OH,pCBA}\alpha_{OH}} \quad (5)$$

294

295 In this study, the major $\dot{Y}OH$ scavengers during ozone-based AOPs in the water matrix are
 296 DOM (dissolved organic matters), nitrite (NO_2^-) and carbonate/bicarbonate (CO_3^{2-}/HCO_3^-).
 297 Therefore, the selected wastewater matrix $\dot{Y}OH$ scavenging rate constant followed equation 5:

$$k_a = k_{OH,DOM}[DOM] + k_{OH,NO_2^-}[NO_2^-] + k_{OH,CO_3^{2-}}[CO_3^{2-}] \quad (6)$$

$$+ k_{OH,HCO_3^-}[HCO_3^-] + k_{OH,pCBA}[pCBA]$$

$$+ k_{OH,t-BuOH}[t-BuOH]$$

298 And substituting equation 6 into equation 5 results in:

$$\frac{1}{k}$$

$$= [t-BuOH] \frac{k_{OH,t-BuOH}}{k_{OH,pCBA}\alpha_{OH}}$$

$$+ \frac{k_{OH,DOM}[DOM] + k_{OH,NO_2^-}[NO_2^-] + k_{OH,CO_3^{2-}}[CO_3^{2-}] + k_{OH,HCO_3^-}[HCO_3^-]}{k_{OH,pCBA}\alpha_{OH}} \quad (7)$$

$$+ \frac{k_{OH,pCBA}[pCBA]}{k_{OH,pCBA}\alpha_{OH}}$$

299 Furthermore, *p*-CBA abatement follows pseudo-first-order kinetics.

$$\ln \frac{[pCBA]_t}{[pCBA]_0} = -k \times t \quad (8)$$

Where, $[pCBA]_t$ and $[pCBA]_0$ are the concentration of *p*-CBA at time *t* and zero. As such, *k* can be determined by means of measurement of *p*-CBA concentration. By plotting $1/k$ as a function of the *t*-BuOH concentration resulting in $1/k$ and the *t*-BuOH concentration are first-order linear relationships (Fig.S1):

$$Y = A[t-BuOH] + B \quad (9)$$

$$Y = \frac{1}{k} \quad (10)$$

$$A = \frac{k_{OH,t-BuOH}}{k_{OH,pCBA}\alpha_{OH}} \quad (11)$$

$$B = \frac{k_{OH,DOM}[DOM] + k_{OH,NO_2^-}[NO_2^-] + k_{OH,CO_3^{2-}}[CO_3^{2-}] + k_{OH,HCO_3^-}[HCO_3^-]}{k_{OH,pCBA}\alpha_{OH}} \quad (12)$$

$$+ \frac{k_{OH,pCBA}[pCBA] + k_{OH,H_2O_2}[H_2O_2]}{k_{OH,pCBA}\alpha_{OH}}$$

300 Dividing equation 11 by equation 10 results in:

$$k_{OH,DOM} = \frac{1}{[DOM]} \left(\frac{B}{A} k_{OH,t-BuOH} - k_{OH,NO_2^-} [NO_2^-] - k_{OH,CO_3^{2-}} [CO_3^{2-}] - k_{OH,HCO_3^-} [HCO_3^-] - k_{OH,pCBA} [pCBA] \right) \quad (13)$$

301

302 The wastewater effluent samples, which were used to determine the selected wastewater $\dot{Y}OH$
 303 scavenging. The results on scavenging kinetics are shown in Fig.7. The results of slope A and
 304 intercept B were 2.3×10^6 s and 33.2×10^3 s M^{-1} ($R^2 \approx 0.987$), respectively. Therefore, the
 305 total $\dot{Y}OH$ scavenging rate constant $1.6 \times 10^4 s^{-1}$

306 **Figure 7: Competition kinetics plot for determination of the $\dot{Y}OH$ scavenging rate**
 307 **constant**

308 3.5 Effect of AC and MWCNT catalyzed ozonation on TOC and COD removal

309 The effect of AC and MWCNT on COD and TOC removal is as shown in the fig.8A & 8B.
 310 The catalyst dose, Ph and ozone dose were optimized as earlier. The catalyst dose for AC was
 311 200 mg/L, for MWCNTs was 100mg/L, pH was maintained at 9 and the specific ozone dose
 312 was 1.2 gm of ozone /gm of TOC. It can be inferred from fig. COD removal in the case of
 313 MWCNTs is comparatively higher than AC catalyzed ozonation. The TOC removal in the
 314 case of MWCNT catalyzed ozonation was observed to be higher when compared with AC
 315 catalyzed ozonation.

316 **Figure 8: Effect of AC and MWCNT catalyzed ozonation on (A) COD removal (B) TOC**
 317 **removal**

318 4 Conclusions:

319 In the catalytic ozonation of textile wastewater, two catalysts were used. Activated carbon
 320 was synthesized from agricultural waste and Multiwalled carbon nanotubes were synthesized
 321 from plastic waste. The minimum requirement of ozone dose to form hydroxyl radicals was
 322 found in terms of specific ozone dose. Hydroxyl radical exposure was found to be increasing
 323 with an increased specific ozone dose. The rate of *p*-CBA degradation was observed to
 324 increase with increase in specific ozone dose and Rct.

325 Increasing pH from 5 to 9 had shown significant enhancement in hydroxyl radical exposure,
 326 rate of *p*-CBA degradation, Rct and rate of ozone decomposition. This trend was observed in
 327 AC as well as MWCNT catalysed ozonation. The MWCNT catalyzed ozonation has shown
 328 superior performance when compared with AC catalysed ozonation.

329 With increase in catalyst loading, the remarkable increment in hydroxyl radical exposure, rate
 330 of *p*-CBA degradation, Rct and rate of ozone decomposition were observed. The impact of

331 catalyst loading was found dominantly positive in case of MWCNT catalysed ozonation. The
332 competition kinetic method was used to estimate the rate constant of reaction of organic
333 matter with hydroxyl radicals, using *p*-CBA as a probe component and t-butanol as a
334 competitive scavenger.

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339 **Declarations:**

340 **Ethics approval and consent to participate:** All authors have approval and consent to
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342 **Consent for publication:** Not applicable.

343 **Competing interests:** The authors declare no competing interests.

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Figures

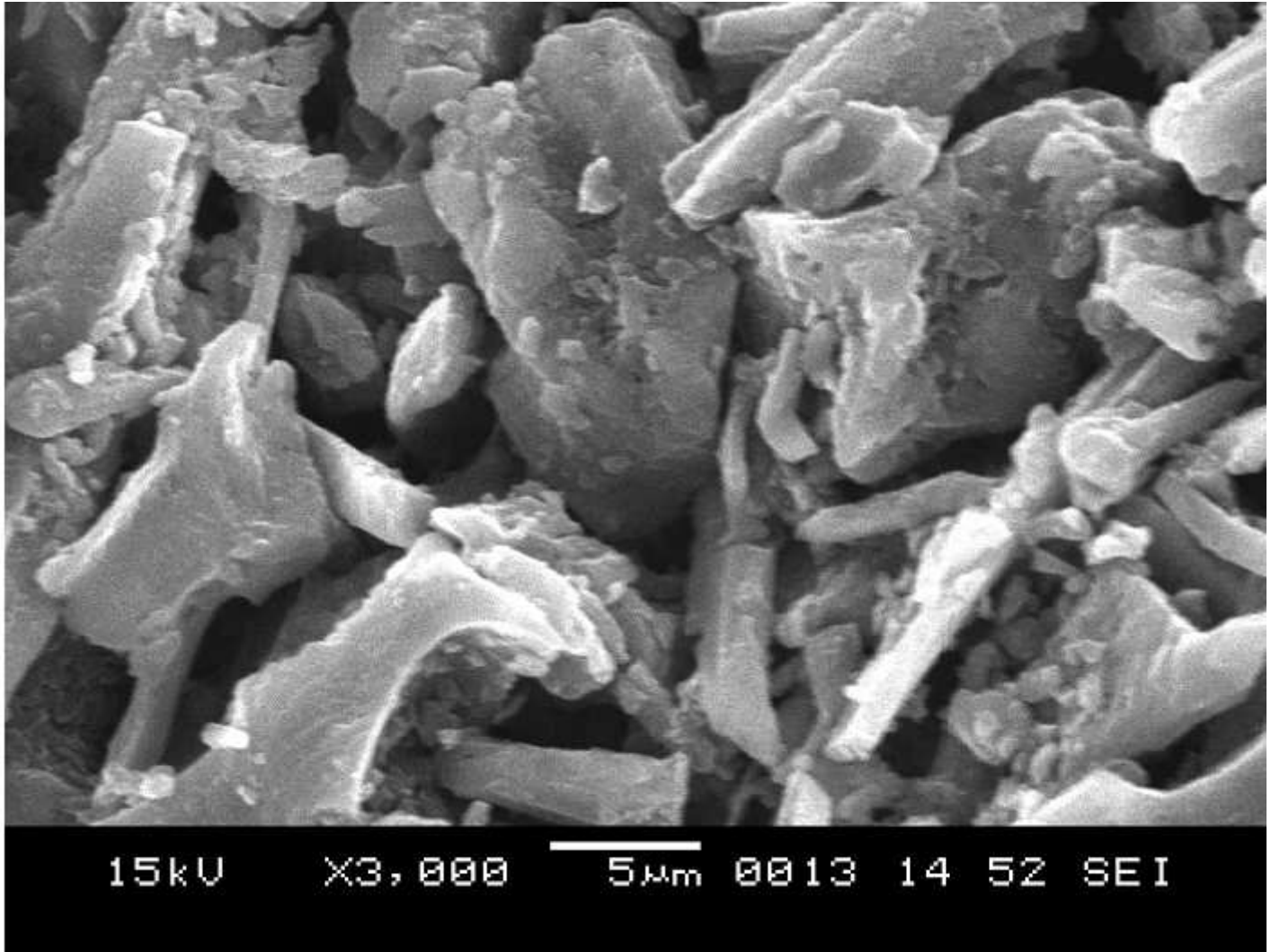


Figure 1

SEM image of Activated carbon

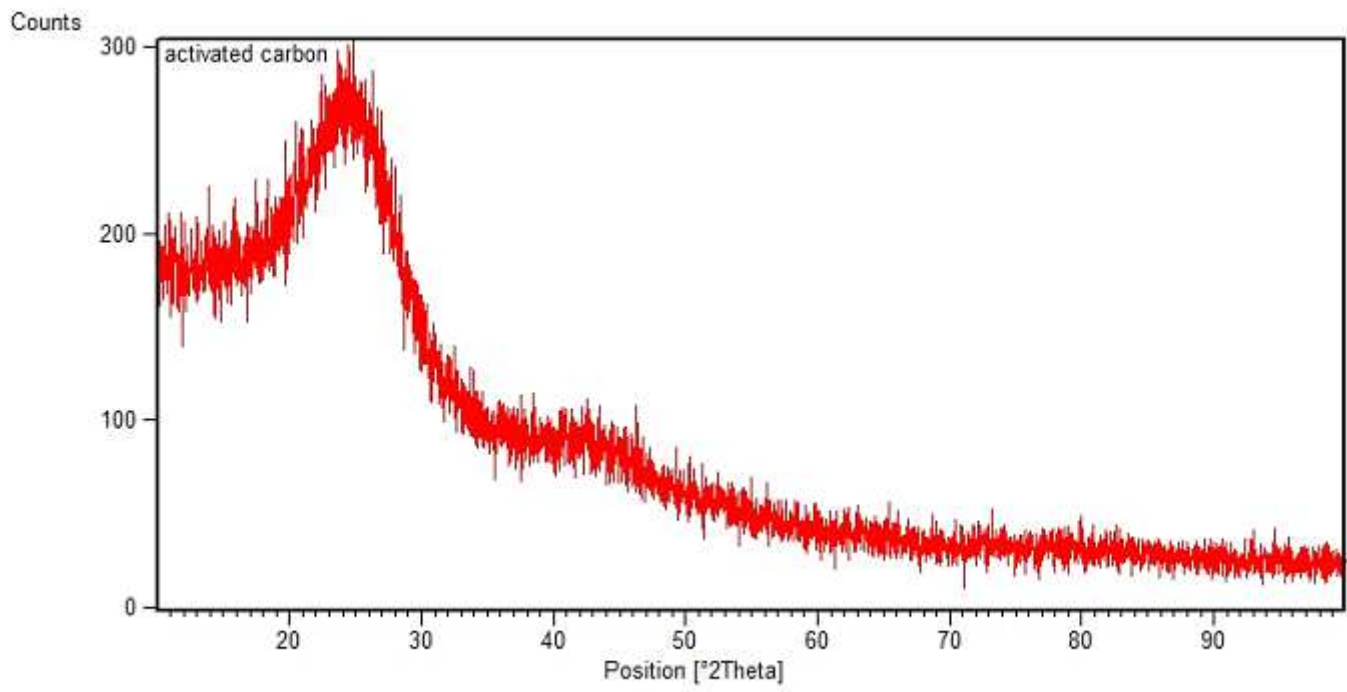
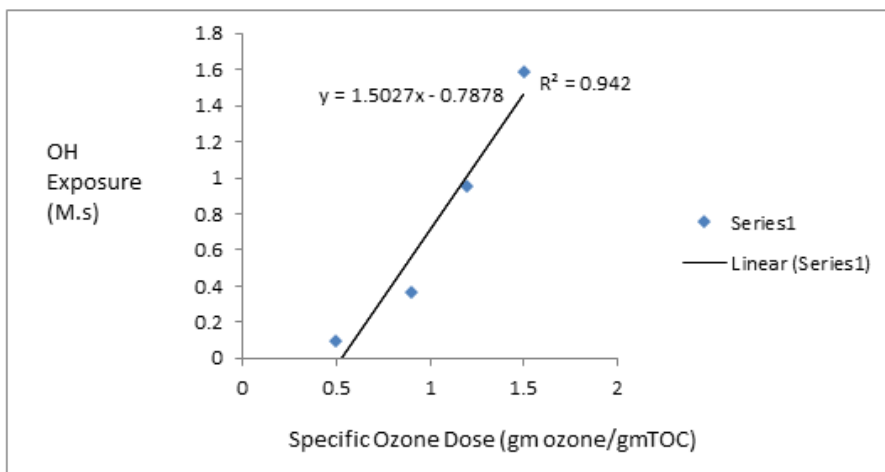
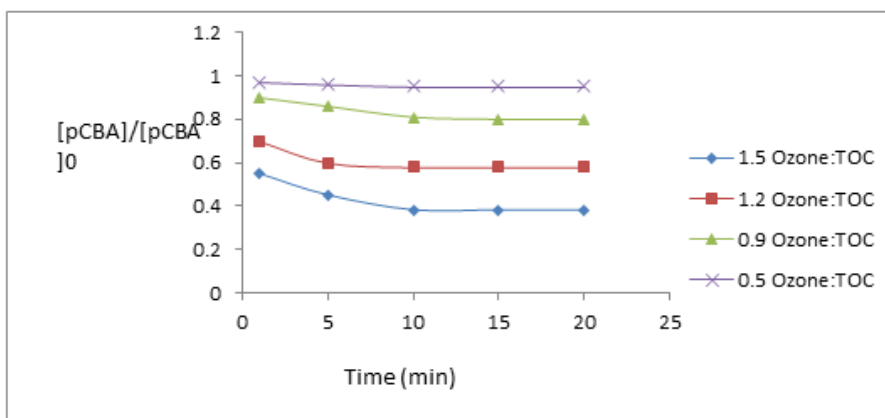
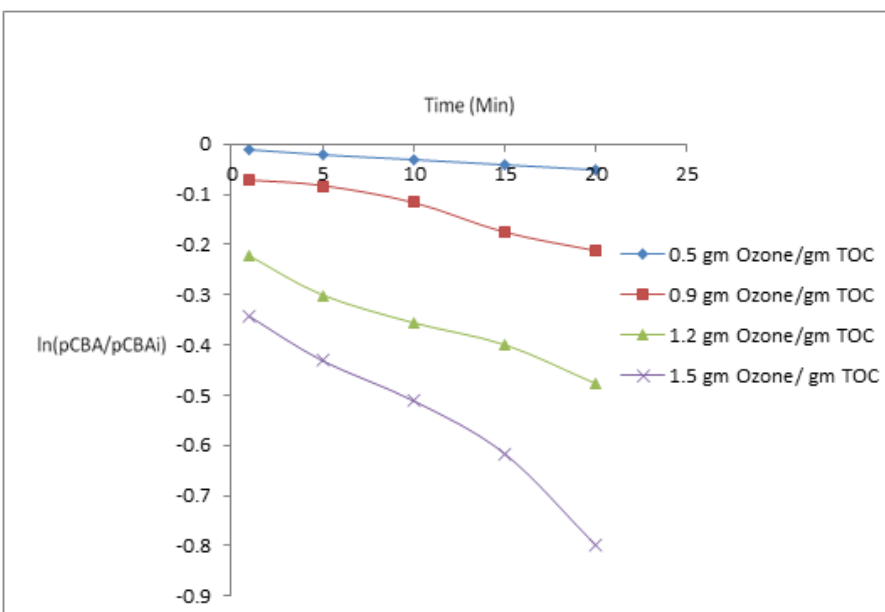
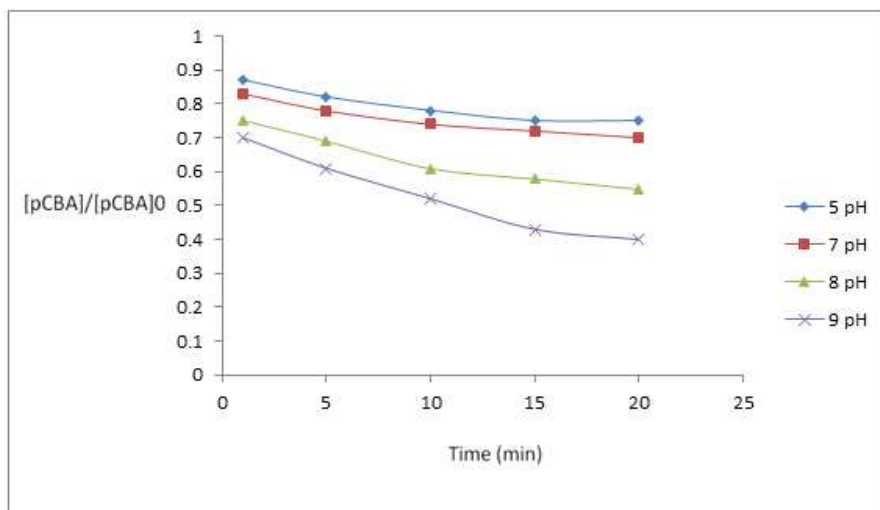
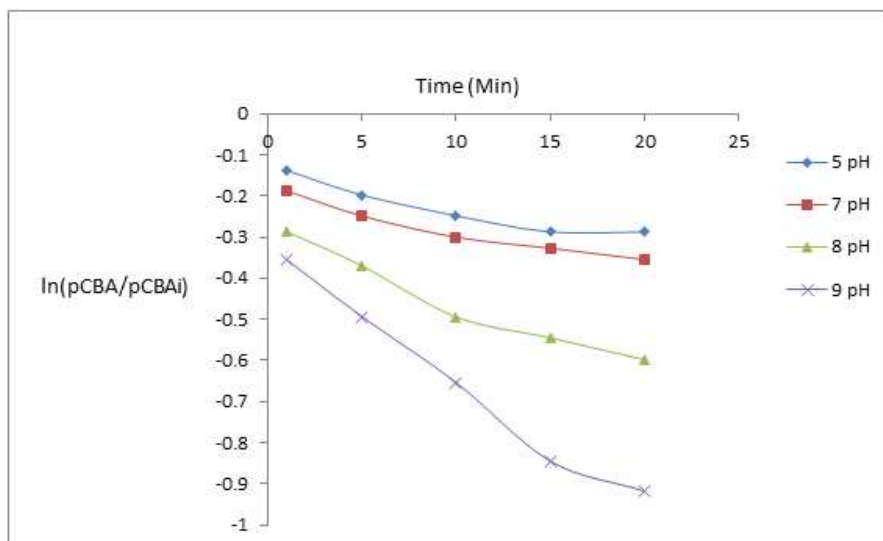
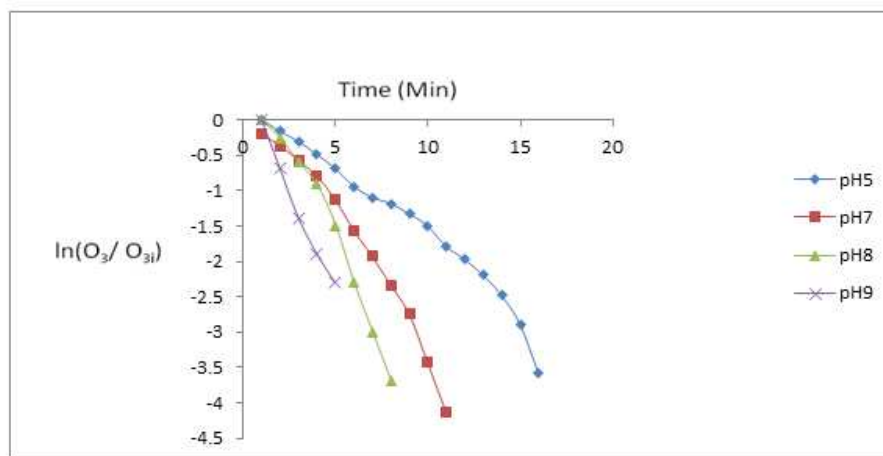


Figure 2

XRD Pattern for Activated Carbon

A**B****C****Figure 3**

(A) Effect of specific ozone dose on $\cdot\text{OH}$ exposure (B) Effect of specific ozone dose on p-CBA degradation (C) Effect of specific ozone dose on rate of p-CBA degradation

A**B****C****Figure 4**

Effect of pH on (A) p-CBA degradation of AC catalyzed ozonation (B) rate of p-CBA degradation of AC catalyzed ozonation (C) rate of ozone decomposition in AC catalyzed ozonation

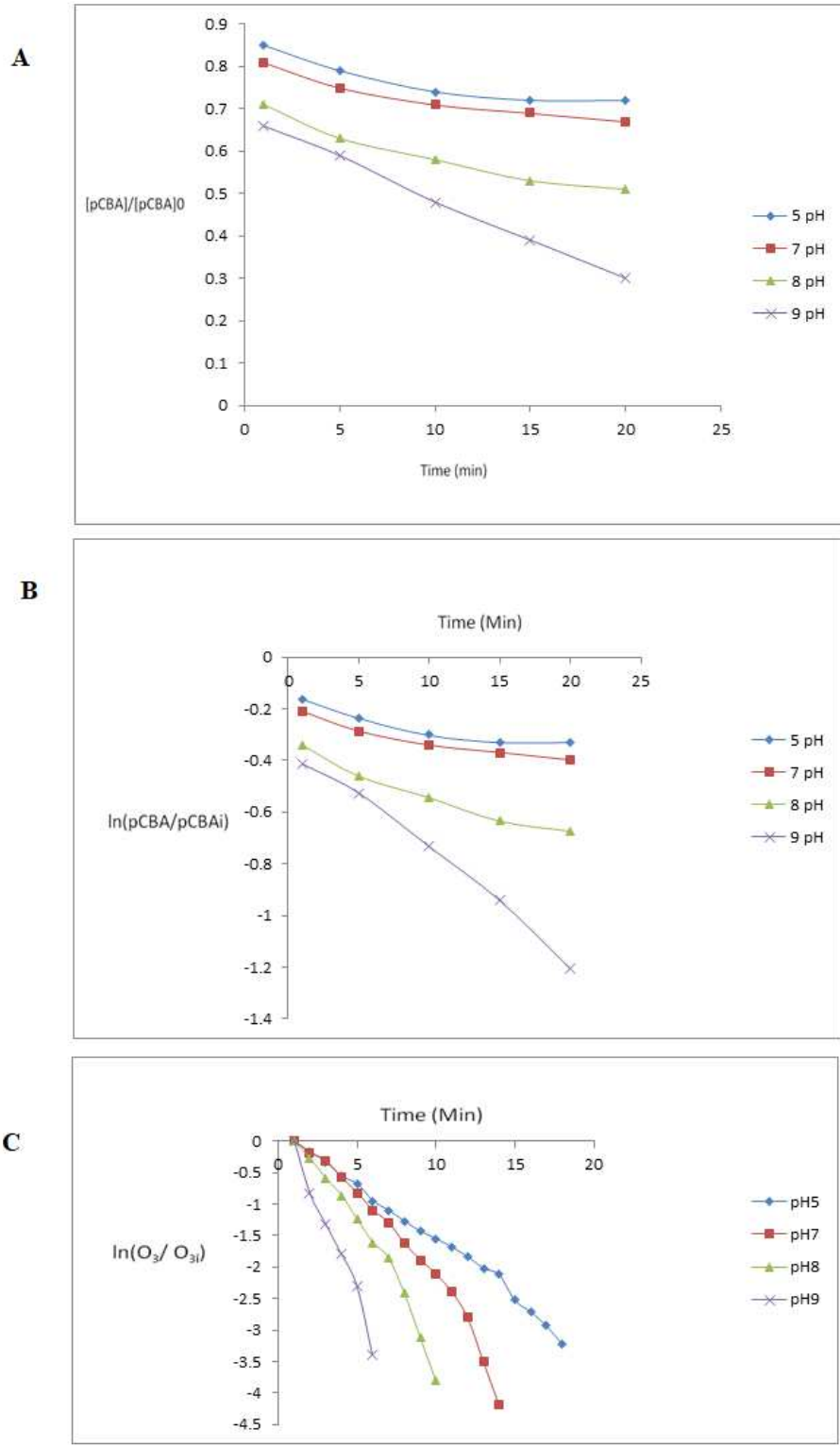


Figure 5

Effect of pH on (A) p-CBA degradation of MWCNTs catalyzed ozonation (B) rate of ozone decomposition of MWCNTs catalyzed ozonation (C) rate of ozone decomposition of MWCNTs catalyzed ozonation

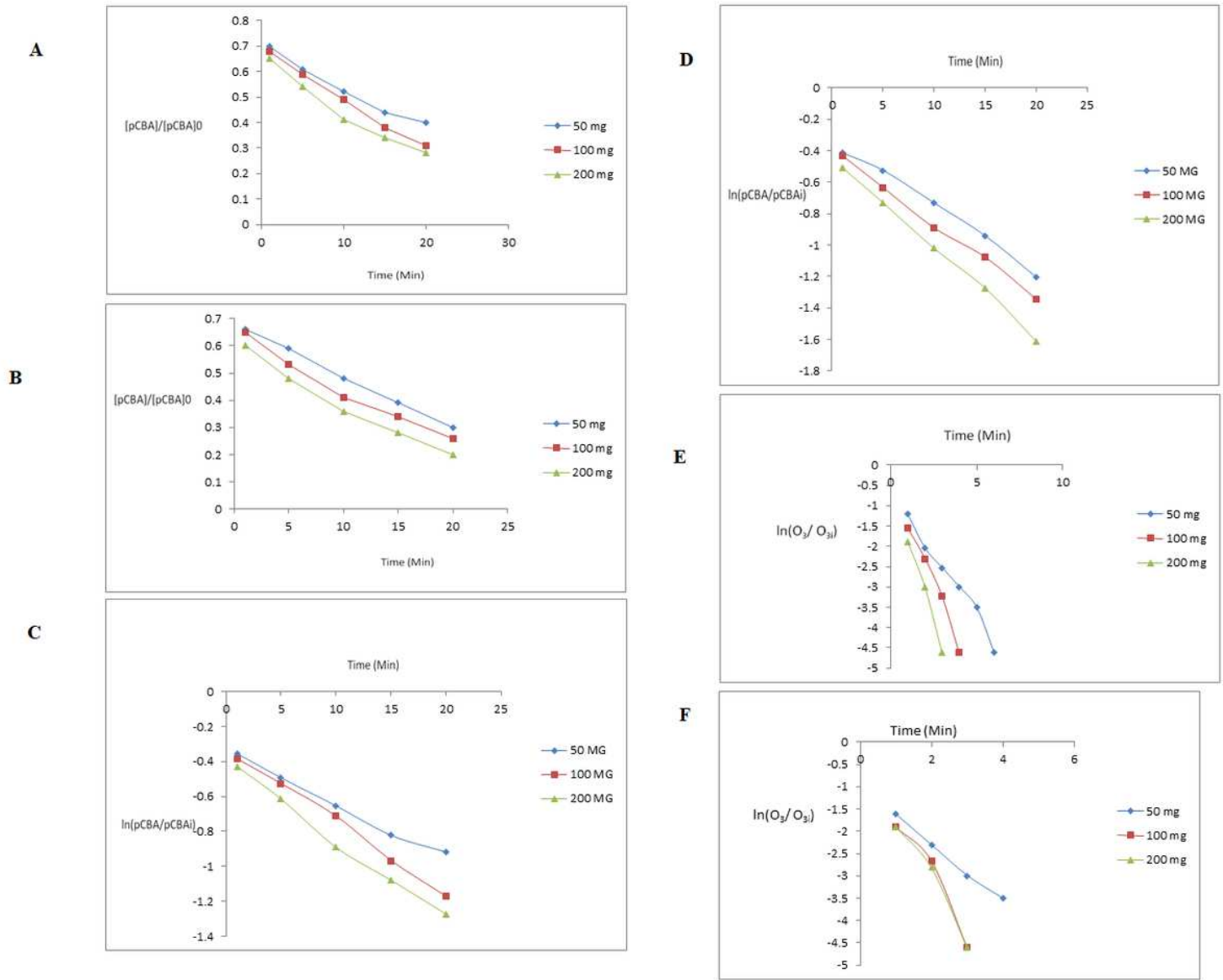


Figure 6

Effect of catalyst loading on (A) p-CBA degradation in AC catalyzed ozonation (B) p-CBA degradation of MWCNTs catalyzed ozonation (C) rate of p-CBA degradation in AC catalyzed ozonation (D) rate of p-CBA degradation in MWCNTs catalyzed ozonation (E) rate of ozone decomposition of in AC catalyzed ozonation (F) rate of ozone decomposition of in MWCNTs catalyzed ozonation

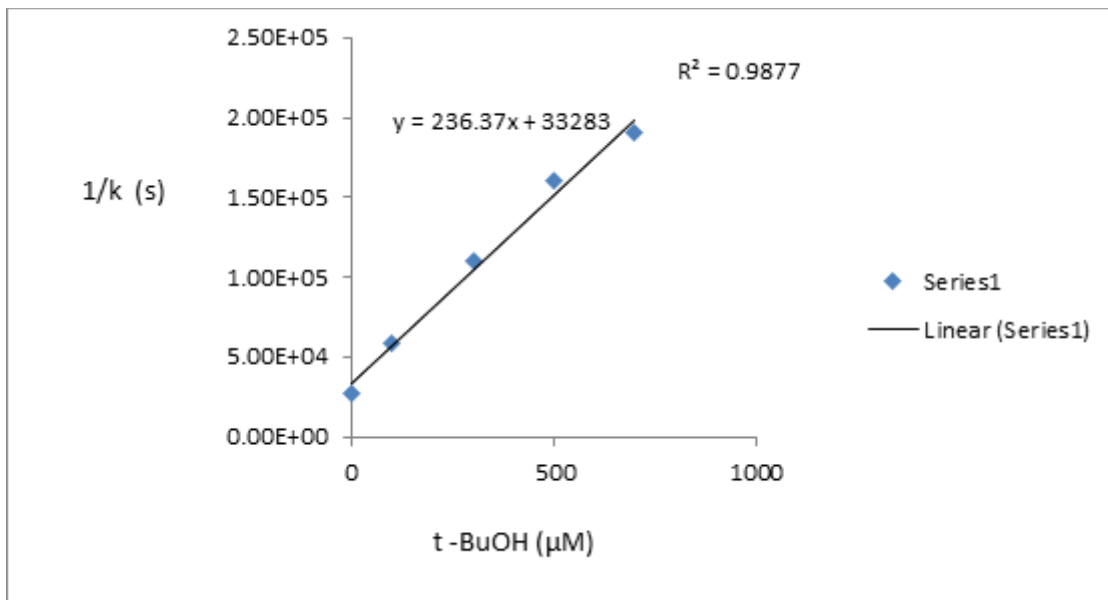
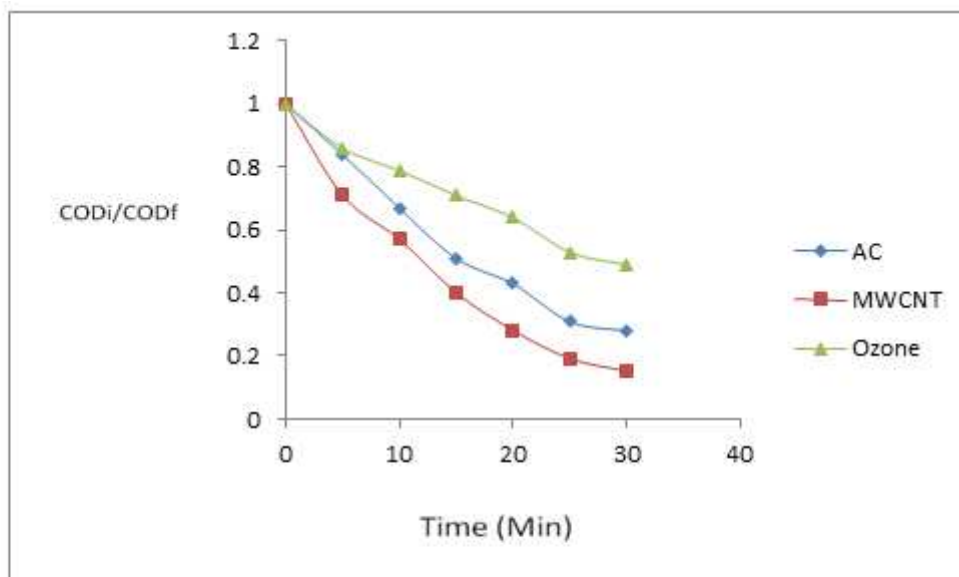
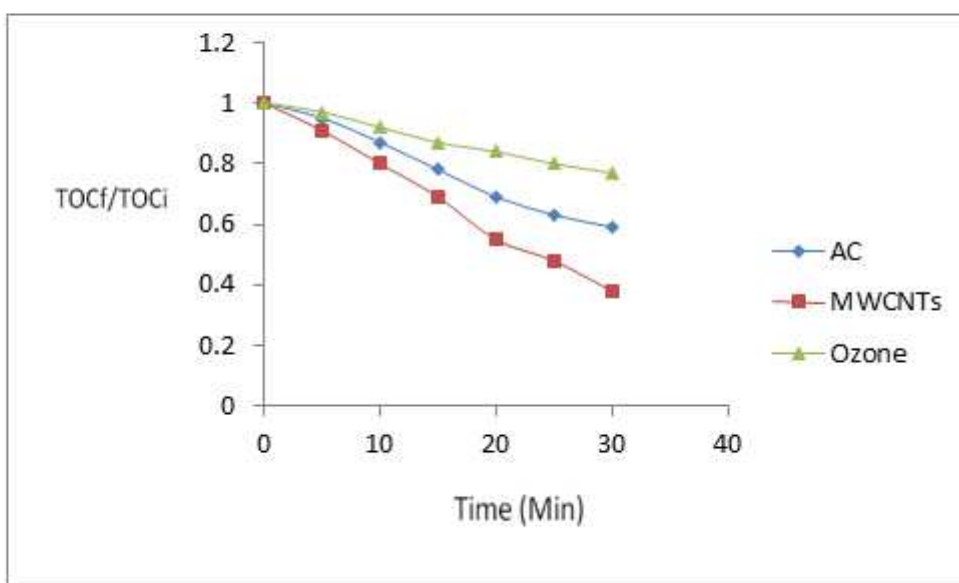


Figure 7

Competition kinetics plot for determination of the $\cdot\text{OH}$ scavenging rate constant

A**B****Figure 8**

Effect of AC and MWCNT catalyzed ozonation on (A) COD removal (B) TOC removal

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