Artificial Flexible Sperm-like Nanorobot Based on Self-assembly and Its Magnetically Actuated Propulsion Property

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Abstract

Sperm cells can move at a high speed in biofluids based on the flexible flagella, which inspire novel flagellar micro-/nanorobots to be designed. However, mass fabrication of vivid sperm-like nanorobots with flagellar flexibility is still challenging. In this work, a facile and efficient strategy is proposed to produce flexible sperm-like nanorobots with self-assembled head-to-tail structure. The nanorobots were composed of a superparamagnetic head and a flexible Au/PPy flagellum, which were covalently linked via biotin-streptavidin bonding. Under a precessing magnetic field, the head drove the flexible tail to rotate and generated undulatory bending waves propagating along the body. Bidirectional locomotion of the nanorobot was investigated, and moving velocity as well as direction varied with the actuating conditions (field strength, frequency, direction) and the nanorobot’s structure (tail length). Effective flagellar locomotion was observed near the substrate and high velocities were attained in both forward and backward directions. Typical modelling based on elastohydrodynamics and undulatory wave propagation were utilized for propulsion analysis. This research presents novel artificial flexible sperm-like nanorobots with delicate self-assembled head-to-tail structures and remarkable bidirectional locomotion performances, indicating significant potentials for nanorobotic design and future biomedical application.

Introduction

Micro-/nanorobots with excellent swimming capability in fluids have become highly attractive due to their great potentials in biomedical applications \(^1\)–\(^5\). These untethered robots can generate effective propulsion in fluidic environment and access desired sites at small scale to achieve special tasks. To date, various types of micro-/nanorobots have been developed via taking biological inspiration from motile microorganisms \(^6\)–\(^8\). For example, inspired by corkscrew propulsion of \textit{E. coli} bacteria, several researches have presented helical micro-/nanorobots actuated by rotating magnetic fields \(^9\)–\(^{13}\). In fact, undulating propulsion is an easy-to-think motion method which is commonly utilized in nature from fishes to monotrichate eukaryotes \(^14\)–\(^17\). In this case, sperm cell is typical with flagellar self-propulsive capability, which can move forward in low Reynolds number biofluids through the flagellum-generated transverse waves \(^18\), and also provides us with possibilities to realize effective flagellar propulsion at micro-/nanoscale.

To date, many researches are focused on designing and fabricating sperm-based micro-/nanorobots. Among these researches, some are focused on direct utilization of living motile sperm’s driving force, which can be integrated with magnetic guidance to form biohybrid microswimmers \(^19\)–\(^21\). However, environmental sensitivity and inconsistent activity of the sperm cells greatly limit the practical applications. The other is to use the sperm’s overall shape and morphology as biotemplates to synthesize microrobots with magnetized elastic flagellar structures \(^22,23\), yet the fabrication is uncontrollable which hinders homogeneity in size as well as propulsion capability.

Enlightened by periodic undulations of the sperms, artificial sperm-shaped micro-/nanorobots have also
researches, some are focused on integrated synthesis based on micro lithography or electrospinning technique, to construct a composite structure containing a magnetic head with a flexible polymer tail. However, the relatively large size and complex fabrication process greatly limit biomedical uses of such millimeter-sized microrobots. Thereon, sperm-shaped self-assembled nanorobots with modular designs stand out, which integrate a tiny head with a slender tail for flagellar construction, and can be treated as an optimal way for essential imitation of the sperms. For example, a Fe$_3$O$_4$ microsphere could be connected with rigid Ni nanorod for sperm-shaped configuration, yet the desired flexibility was lacked; or be linked with repolymerized bacterial flagellum to achieve flagellar propulsion, yet great diversity existed compared with the sperm's shape. Despite these tremendous efforts, to the best of our knowledge, no research has realized flexible sperm-like nanorobots with assembled head-to-tail structures. Thus it is imperative to develop facile and reliable fabrication methods to construct artificial sperm-like nanorobots, and study the corresponding flagellar propulsion at low Reynolds numbers.

Here, we propose artificial flexible sperm-like nanorobot synthesized via a facile self-assembly strategy using Fe$_3$O$_4$ nanobeads and flexible polymer flagella for the first time, which can generate bidirectional flagellar propulsion under precessing magnetic fields. Template-assisted electrochemical deposition was used to synthesize Au/PPy nanowires, and the streptavidin modified tails could be bonded with biotinylated magnetic nanobeads to form the sperm-like nanorobots. The self-assembled nanorobot was actuated in viscous glycerin and exhibited effective locomotion in forward or backward directions. A series of actuation experiments were conducted to characterize flagellar propulsion of the nanorobots, and bidirectional locomotion velocity under precessing magnetic fields of diverse parameters (strength, frequency, precession angle and direction) were studied in detail. Under a magnetic field of 70 Gs, 40 Hz and precession angle at 30°, the nanorobot could be actuated forward to reach a high velocity at 4.86 µm/s, and backward velocity at 3.17 µm/s could also be achieved when turning the precession axis around. Such vivid sperm-like nanorobot with flexible propulsion performance under magnetic actuation provides possibilities for flagellar nanorobot design and fabrication, and also indicates significant potentials for applications at low Reynolds numbers.

**Methods**

**Reagents and materials.** In the experiments, sodium hypophosphite (NaH$_2$PO$_2$·H$_2$O), chloroauric acid (HAuCl$_4$·4H$_2$O), trisodium citrate (Na$_3$C$_6$H$_5$O$_7$·2H$_2$O), citric acid (C$_6$H$_8$O$_7$), pyrrole (C$_4$H$_5$N), boric acid (H$_3$BO$_3$), ferric chloride (FeCl$_3$·6H$_2$O), ferrous chloride (FeCl$_2$·4H$_2$O), sodium hydroxide (NaOH), glycerol (C$_3$H$_8$O$_3$), dimethyl sulfoxide (DMSO), dithio-bis-succinimidypropionate (DTSP), biotin and streptavidin solutions were all purchased from Lan Yi Chemical Reagent Company (Beijing, China). Biotin modified Fe$_3$O$_4$ nanoparticles (SVM-025-5H) were purchased from Spherotech.

**Synthesis of the flexible Au/PPy nanowires.** The commercial AAO template with pore size of 200 nm was purchased from Whatman Anodisc. Firstly, 100 nm of gold was coated on one side of the template, acting as a conducting working electrode via magnetic sputtering technique. Then the AAO template was
placed in a self-made electrodeposition container, and Ag/AgCl reference electrode as well as Pt wire electrode was used for subsequent deposition. The Au-coated membrane was immersed in the prepared gold plating solution (containing 30 g/L H$_3$BO$_3$ and 34 g/L HAuCl$_4$·4H$_2$O), and the Au section was deposited at a DC voltage of -0.2 V. Next, deposition of PPy nanorods was conducted using prepared PPy plating solution (containing 19.25 g/L citric acid and 6.95 mL/L pyrrol) at +0.8 V. PPy flagella of various lengths could be synthesized via adjusting the deposition time. After that, mechanical polishing was conducted with 3–4 µm alumina powder to remove the sputtered sacrificial gold layer.

**Modification process of the nanowires.** Firstly, the Au ends of the nanowires (retained in the AAO templates) were exposed to a DMSO solution containing DTSP (4 mM), and immersed for 6 hours at 25°C to modify a self-assembled monolayer of DTSP on the end of gold segment. Then, streptavidin solution (0.5 mg/mL) was added to immerse the polished surface at room temperature for 6 hours, to covalently bond streptavidin to the DTSP modified Au ends. After streptavidin functionalization, template removing and nanowire releasing was achieved using NaOH (0.1 M) solution for 3 hours. Finally, the nanowires were washed with PBS solution (pH = 7.4) and centrifuged (10000 rpm, 5 min) for three times, and finally stored in PBS solution (4°C) for further uses.

**Fabrication and characterization of the sperm-like nanorobots.** The as-prepared Au/PPy nanowires and biotin modified Fe$_3$O$_4$ nanoparticles were mixed in solution at a ratio of 1:1, and gently shaken at room temperature for 30 minutes. Due to the solid bonding between biotin and streptavidin, artificial sperm-like nanorobots were formed via self-assembly and nanorobots with one single flagellum could be mostly investigated in the experiments. The morphology and main elements of the as-prepared flagella and nanorobots were characterized by a field emission scanning electron microscope (SU-8010LA, Hitachi) equipped with an energy dispersive spectrometer.

**Magnetic actuation experiments of the sperm-like nanorobots.** A custom-made triaxial Helmholtz coil system was used to actuate the nanorobotic sperms, and the details were demonstrated in our previous published papers 10,35. To actuate the sperm-like nanorobot and test its propulsion performance, a precessing magnetic field was generated via the coils, in which the resultant field vector at the head of the nanorobot was rotating in a cone-like path. The field strength, frequency and spatial directions could be precisely tuned via a programmed current controller coupled with the coils. Locomotion of the nanorobots could be recorded in real time through a CMOS camera installed on the microscope. In our experiments, the as-prepared nanorobotic sperms were dispersed in 60% glycerin solution and transferred into a PDMS chamber at the coil center for magnetic actuation tests. In the viscous medium, the nanorobots could be considered as floating and adverse effect of the substrate surface was eliminated. For velocity measurement and locomotion direction tests, three times of experiments were conducted, and average velocity as well as standard deviations were calculated based on the experimental data.

**Results And Discussion**
Preparation and characterization of the sperm-like nanorobot. The fabrication process of sperm-like nanorobots was briefly shown in Fig. 1a. Firstly, we prepared flexible Au/PPy composite nanowires with the Au ends modified using streptavidin, which could act as artificial flagella of the nanorobots to generate undulatory wave propagation. Here, multi-step electrochemical deposition and monolayer modification were combined for fabrication. Au segments of 3 µm and PPy tails of given lengths were deposited in sequence. After mechanical polishing of the sacrificial gold layer, the Au tips of the nanowires were exposed and coated with monolayer of DTSP molecules, which could increase the contact area and improve the assembly efficiency for the following process. Then wet-etching of the Al₂O₃ templates was conducted and the nanowires were released to be modified with streptavidin. After that, the nanowires were mixed with biotin-coated Fe₃O₄ nanoparticles for bonding and formed the final sperm-like nanorobots. In this case, the Fe₃O₄ head endows the nanorobot with magnetic response and the flexible flagellum ensures undulatory propagation for effective propulsion.

Morphology and elemental analysis of the artificial flagella were conducted, and the SEM and EDS results were shown in Fig. 1b and 1c. Distinct two-stage structure can be observed on the nanowire, which corresponds to the Au tip and the PPy body, respectively. Flexibility of the artificial flagellum is presented with slightly bending in this view. Schematics of the self-assembled nanorobot’s head-to-tail structure and the corresponding SEM image were shown in Fig. 1d and 1e, respectively. It can be observed that an intact self-assembled microstructure has been successfully achieved between the magnetic head and the flexible flagellum, to form the sperm-like nanorobot.

Theoretical analysis of the nanorobot’s propulsion. The nanorobot in this study is fabricated via self-assembly using a superparamagnetic nanobead and an artificial flexible ultra-thin nanorod. Assuming the head has a magnetic moment \(M\) in the direction under the magnetic field, the flexible flagellum has a body length \(L\) with a given elasticity modulus. For an arbitrary point \(P\) along the tail, we mark it with a generalized coordinate \(q\) respective to the head and describe its position at time \(t\) with vector \(p(q, t)\), which can also be transferred to the head’s frame as

\[
p(q, t) = (q \phi_y(q, t) \phi_z(q, t))
\]

where \(\phi_y(q,t)\) and \(\phi_z(q,t)\) represent the corresponding deformation along Y and Z axis, respectively.

Then the moving Frenet-Serret frame can be established on point \(P\) along local tangent, normal, and bi-normal directions:

\[
t = \frac{dp(q, t)}{dq} \left| \frac{dp(q, t)}{dq}\right|, \quad n = \frac{dt/ dq}{||dt/ dq||}, \quad b = t \times n
\]
the flexible flagellum. According to the typical resistive force theory, the force and torque balance based on magnetic and fluidic fields can be expressed as:

\[
\begin{bmatrix}
F_m + F_d \\
T_m + T_d
\end{bmatrix} = 0
\]  

(3)

Here, gravity is neglected, \(F_m\) and \(T_m\) are magnetic force and torque that can be expressed as:

\[
\begin{bmatrix}
F_m \\
T_m
\end{bmatrix} = \begin{bmatrix}
V(M \cdot \nabla)B \\
VM \times B
\end{bmatrix}
\]  

(4)

\(F_d\) and \(T_d\) are fluidic drag force and torque, which can be decomposed into contributions of the head and the tail:

\[
\begin{bmatrix}
F_{d, \text{head}} \\
T_{d, \text{head}}
\end{bmatrix} = \begin{bmatrix}
D_h & -D_h S_h \\
S_h D_h & N_h
\end{bmatrix} \begin{bmatrix}
V \\
\Omega
\end{bmatrix}
\]  

(5)

\[
\begin{bmatrix}
F_{d, \text{tail}} \\
T_{d, \text{tail}}
\end{bmatrix} = \int_0^L \begin{bmatrix}
R CR^T & -R CR^T S_t \\
S_t R CR^T & -S_t R CR^T S_t
\end{bmatrix} dl \begin{bmatrix}
V \\
\Omega
\end{bmatrix}
\]  

(6)

where \(V\) and \(\Omega\) are propulsion and rotation velocity matrices, \(D_h\) and \(N_h\) are resistance matrices for the head, and \(C\) represents the resistance coefficient matrix for the tail. Besides, \(R\) is the rotation matrix between the local Frenet-Serret coordinates and the nanorobot’s frame, \(S_h\) and \(S_t\) are the corresponding position transformation matrices for the head and the tail.

The above equations describe the elasto-hydrodynamics of the sperm-shaped nanorobot swimming in viscous fluids. In the experiments, the nanorobot was actuated to swim in the horizontal plane (XY) and was investigated from the top view. Apart from the elasto-hydrodynamics, a simplified undulatory propagation modelling could also be used. Swimming of the nanorobot in the X direction can be simplified into two orthogonal components in the XY and XZ planes. Motion of the nanorobot in each plane can be treated as a bending wave propagation across the two distal ends, and relative phase lag between the head and tail in two planes are noted as \(\phi_{xy}\) and \(\phi_{xz}\). Here, flagellar propulsion of the sperm-like nanorobot along X direction can be ascribed to the overall oscillation along the body induced by two separate oscillations in both XY and XZ planes as:
where $a_1$ and $a_3$ are amplitudes of magnetic oscillation that correspond to the head, $a_2$ and $a_4$ are amplitudes of fluidic oscillation that correspond to the tail. Besides, $f$ is the actuation frequency, and $m$ is the curvature of bending deformation.

The propulsive forces in two planes can be expressed as

$$ F_{xy}(x, y) = \int_0^L C_\parallel \left[ \left( \frac{C_\perp}{C_\parallel} - 1 \right) \frac{dy}{dt} \frac{dy}{dx} - V_{xy}(x, y) \right] dl $$

$$ F_{xz}(x, z) = \int_0^L C_\parallel \left[ \left( \frac{C_\perp}{C_\parallel} - 1 \right) \frac{dz}{dt} \frac{dz}{dx} - V_{xz}(x, z) \right] dl $$

where $dl$ is an infinitesimal section along the body, $C_\parallel$ and $C_\perp$ are the drag coefficients in the tangential and normal directions. Besides, $V_{xy}(x, y)$ and $V_{xz}(x, z)$ are two contributions of the X-direction velocity resulted from oscillations in XY and XZ planes, respectively. When the nanorobot reaches a steady swimming state, the total force equals zero, and the velocity components can be calculated to be

$$ V_{xy}(x, y) = \pi \left( \frac{C_\perp}{C_\parallel} - 1 \right) \left( \frac{m-1}{m+1} \right) \frac{a_1 a_2}{L} \sin\left( \phi_{xy} \right) $$

$$ V_{xz}(x, z) = \pi \left( \frac{C_\perp}{C_\parallel} - 1 \right) \left( \frac{m-1}{m+1} \right) \frac{a_3 a_4}{L} \sin\left( \phi_{xz} \right) $$

And the resultant velocity along X-direction can be expressed as

$$ V_x = V_{xy}(x, y) + V_{xz}(x, z) $$

Hence, we can deduce that a phase difference in oscillation is requisite to generate effective locomotion with a nonzero velocity. The oscillations in two perpendicular planes undergo different fluidic drag conditions due to the substrate-induced asymmetry, and diverse amplitudes as well as phase lags are stimulated. The resultant motion of the nanorobot is determined by combination of the decomposed oscillations, which can result in a balance between propulsion and retarding in the form of forward or
backward locomotion. In this case, dynamic magnetic field with a precessing angle is essential for swimming direction reversal since spatial oscillations become accessible to lead to bidirectional resultant.

**Propulsion performance of the sperm-like nanorobot.** To actuate the sperm-like nanorobot and test its propulsion performance, a precessing magnetic field or a so-called conical rotating magnetic field was applied using a custom-made triaxial Helmholtz coil system. The externally actuated magnetic field can be expressed as

\[
\vec{B} = B_{yz}[\cos(2\pi ft)\vec{e}_y + \sin(2\pi ft)\vec{e}_z] + B_x\vec{e}_x \tag{14}
\]

where \(B_{yz}\) and \(f\) are the amplitude and rotating frequency of the circular polarized component of the magnetic field. And \(B_x\) is the static component of the magnetic field. Besides, \(\vec{e}_x, \vec{e}_y, \vec{e}_z\) are the unit vectors along the corresponding coordinate axis.

The resultant field vector at the head of the nanorobot was rotating in a cone-like path, and the angle between the field vector and the cone axis was noted as the precessing angle (\(\theta\)) of the actuation field. For flagellar propulsion of sperm-like nanorobots, undulatory motion theory has been developed as described above, which is focused on the bending wave propagating process along the body. Actuated by the magnetic torque exerted on the head, continuous rotation is triggered to drive the body to fluctuate. The stimulated wave propagates along the flagellum yet different oscillating amplitudes are generated from the head to the tail. Flexibility of the artificial flagellum contributes to effective undulatory propagation and a constant phase lag exists compared to the magnetic head. Here, time-dependent deformation of the flexible flagellum was measured over one whole period and morphing changing process of the body was also illustrated. The nanorobot was actuated to oscillate by a 2 Hz precessing field (\(B = 100\) Gs, \(\theta = 30^\circ\)) (Movie 1). The results indicate the whole propagating process of the generated wave during helical flagellar propulsion, and a distinct oscillating angle can be observed from the superimposed image as shown in Fig. 2a. Such nanorobot could be actuated to precess synchronously with the low-frequency alternating magnetic field.

A planar coordinate system was defined to facilitate position recording and calculation. In this view, the upward tail tip of the nanorobot corresponds to a positive value of oscillating angle yet the downward tail tip corresponds to a negative one. As shown in Fig. 2b, we measured the oscillating angle change of the nanorobot in a given time period, which exhibited a sinusoidal pattern with time and kept consistent with the precessing field's oscillation. To investigate the relative position relations between the nanorobot's head and flagellum, we further recorded the displacements of the head and the tail tip along the Y axis, with respect to the original position (\(Y = 0\)) at \(t = 0\) s. As shown in Fig. 2c, the displacement waveforms near the distal end as well as the head were recorded. Both the head and the flagellum undergo a sinusoidal waving locomotion in the direction perpendicular to the cone axis, and a fixed phase diversity.
exists between them. The head and the flagellum exhibit diverse oscillation amplitudes during propulsion, in which the tail tip oscillates with a larger amplitude compared with the head. In this case, the nanosphere head dominates the magnetic response and acts as an oscillation source. It is actuated to precess around and drives the flagellum to rotate in the same pattern with a phase lag under the sinusoidal alternating magnetic field. It also proves that asymmetrical shape deformation occurs to cater the scallop theorem and achieve effective locomotion as a result. At the same time, a negative positional offset of the swimmer’s body can be observed, which is related to the minor lateral drift during swimming.

**Bidirectional locomotion property of the nanorobot.** For magnetic actuation of the sperm-like nanorobot, four types of spatially oriented precessing magnetic fields were defined according to the corresponding directions (Fig. 3a). When the field vector exhibited an acute angle with the flagellum-head direction, the field was defined as a “Head-pointing Field” (HF), and the rotating direction was further classified into counter-clockwise (CCW) or clockwise (CW) types on the basis of the right-hand rule. Schematics of the sperm-like nanorobot actuated by a HF type field with a precessing angle $\theta$ was shown in Fig. 3b. Similarly, when the field vector was pointing in the head-flagellum direction, it could be defined as a “Flagellum-pointing Field” (FF) with a CCW or CW rotating directions. In our experiments, the nanorobotic sperms would not easily turn around for coincident magnetic alignment when the precessing axis of the high-frequency field ($f > 5$ Hz) was abruptly turned in an opposite direction. This could be ascribed to the relatively low magnetic torque as well as the encountered fluidic drag of the slender nanorobot near the substrate surface, which induced the insensitive magnetic response under high-frequency dynamic fields. This was also confirmed using magnetic nanowires actuated under 3 Hz and 5 Hz precessing fields for comparison (Movie 5 and 6). Both HF and FF type fields could be used to actuate the nanorobot and the flexible flagellum could be driven to oscillate around with the precessing magnetic head. Effective locomotion can be observed near the substrate due to periodic nonreciprocation that breaks the time symmetry, which is depended on integrated effects of elastic flagellum, hydrodynamic resistance as well as fluidic flows generated by the moving head. Due to continuous interactions with the viscous fluids, helical flagellar propulsion was generated for the nanorobot.

To study the motion directionality, diverse precessing angles and directions were adopted for experimental comparison (Movie 2). As shown in Fig. 3c, the field strength and frequency were set to be constant at 100 Gs, 40 Hz, yet the spatial directions were different. In Fig. 3c-1, when a field of HF-CCW at $\theta = 10^\circ$ was applied, backward locomotion in the flagellum-pointing direction could be observed, which corresponded to a negative velocity ($V < 0$). However, when the field was set to be precessing in the CW direction, the nanorobot changed to swim forward on the contrary. In this case, the nanorobot was capable to move in an opposite direction without a U-turn trajectory, which was different from other one-tail magnetic microswimmers. This property could be attributed to the chirality of the sperm-like nanorobot, which was a combined effect of the nonideal self-assembled structural configuration as well as the time-dependent undulatory dynamics. Thus magnetic fields of diverse precessing directions were capable to drive the nanorobot to rotate and achieve bidirectional locomotion. In Fig. 3c-2, the magnetic field ($\theta = 10^\circ$) was tuned to be a FF type, the nanorobot kept the original pointing direction without turning...
turning the precessing axis 180°, yet the nanorobot could be driven to oscillate and move in an opposite
direction as a result. Therefore, a FF-CW and FF-CCW type of precessing magnetic field could actuate the
nanorobot to move in the same direction with the results of HF-CCW and HF-CW cases, respectively.

In addition, the influence of the actuation field’s precession angle was also investigated as shown in
Fig. <link rid="fig3">3</link>-c-3. Under a HF type field at θ = 30°, the nanorobot could be effectively
actuated forward in both CCW and CW directions, which was quite different with the results demonstrated
in Fig. 3c-1. It could be explained that actuation field of a large precessing angle induced relatively violent
precession with higher oscillation frequency, and the chirality was no longer valid in this case. The results
confirmed that flexible switching between swimming forward and backward could be achieved via tuning
the actuation field parameters, including precessing direction and angle as well as field frequency. In the
future, such bidirectional propulsion property can be applied to control multiple sperm-like nanorobots
with distinguished strategies and complete cooperative tasks.

Based on the preliminary actuation study above, actuation experiments under fields of various
parameters were conducted, and locomotion directions as well as resultant velocities were systematically
measured. As shown in Fig. 4a-1 to 3, the field strength was set to be constant at 50 Gs, yet the
precessing angles were 10°, 30°, 60°, respectively. Four types of fields (HF-CCW, HF-CW, FF-CCW, FF-CW)
at a given frequency ranging from 5 Hz to 40 Hz were applied to actuate the nanorobot. The positive
velocity corresponded to swimming forward yet the negative velocity represented backward propulsion.
At a lower value of precession angle (θ = 10°), the nanorobot was actuated to swim backward over the
frequency range regardless of spatial directions of the fields. However, the results at higher precession
angles (θ = 30° and 60°) were completely different since both forward and backward locomotion could be
observed. Specifically, the nanorobot was actuated forward under HF-CW or FF-CCW fields, yet backward
under HF-CCW or FF-CW fields. A highly effective forward velocity of 2.11 µm/s and backward velocity of
2.77 µm/s could be easily obtained at θ = 30° via tuning the precession directions of the field, indicating
distinct bidirectional propulsion property which was different from previously reported sperm-shaped
microswimmers.

As shown in Fig. 4b-1 to 3, under precessing magnetic fields of 70 Gs, the propulsion results were similar
with the cases in 50 Gs when other parameters kept the same. The nanorobots still kept swimming
backward at θ = 10°, yet locomotion differentiation occurred when θ = 30° or 60°. However, when the field
strength was large enough (100 Gs), it turned to be much easier for the nanorobots to move forward.
Specifically, both HF-CW and FF-CCW fields could successfully drive the nanorobots forward at θ = 10°,
despite backward locomotion was still destined under HF-CCW or FF-CW fields. A large forward velocity
of 2.96 µm/s and backward velocity of 4.26 µm/s could both be achieved at 40 Hz using the opposite
precessing directions (HF-CW and FF-CW fields, respectively). As increasing precessing angle of the 100
Gs fields (θ = 30°, 60°), robust forward propulsion turned to be dominated regardless of the spatial
directions of the actuation fields. In this case, a significantly high forward velocity could be obtained over
a wide frequency range.

\[
\text{Loading [MathJax]/jax/output/CommonHTML/fonts/TeX/fontdata.js}
\]
Thereon, we measured and summarized locomotion directions of the nanorobot actuated by precession magnetic fields of diverse parameters, and the results were listed in Table 1. From the observations in our experiments, it can be deduced that locomotion direction of the sperm-like nanorobot is determined by multiple actuation parameters including field strength, frequency, precessing angle as well as direction. In the experiments, the sperm-like nanorobots generally tended to move forward under precessing magnetic fields of HF-CW or FF-CCW types. To propel the nanorobots forward, precessing magnetic fields of an intensified strength as well as a large precessing angle were desired for actuation, which was also consistent with the velocity measurement results in Fig. 4.

<table>
<thead>
<tr>
<th>θ</th>
<th>B (Gs)</th>
<th>HF-CW/HF-CCW</th>
<th>FF-CW/FF-CCW</th>
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<tbody>
<tr>
<td>10°</td>
<td>50</td>
<td>+/-</td>
<td>+/-</td>
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<tr>
<td></td>
<td>70</td>
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<td>100</td>
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<td>30°</td>
<td>50</td>
<td>+/-</td>
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<td>70</td>
<td>+/-</td>
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Moreover, we also fabricated nanorobots with shorter flagella, which were synthesized via controlling the electrochemical deposition time. In Figure S2, SEM image of the short-tailed nanorobot (tail length about 8 µm) was demonstrated. Actuation experiments of such nanorobot under precessing magnetic fields of 100 Gs were carried out (Movie 3 and 4) and locomotion velocities were calculated as shown in Fig. 5. Similarly, four directional types of fields and precessing angles of 10°, 30°, 60° were applied successively for flagellar propulsion. Bidirectional locomotion could be distinctly observed under fields of any precession angles, which was quite different compared with the long-tailed nanorobots that tended to move forward under the same actuation condition. Under the 100 Gs magnetic field of a moderate precessing angle (θ = 30°), typical bidirectional property could be observed and relatively high locomotion velocity exceeded 2 µm/s could be achieved both in forward and backward directions. The nanorobot could be actuated to move forward under precessing magnetic fields of HF-CW or FF-CCW types, and move backward under HF-CCW or FF-CW fields, which were still similar with the experimental results of
long-tailed ones actuated under 70 Gs fields. With diversity in body length, the sperm-like nanorobots exhibited different sensitivity to the dynamic fields yet the locomotion directions kept basically consistent. It can also be predicted that short-tailed nanorobots tend to move forward under precessing fields of an enhanced intensity.

**Conclusion**

In summary, we presented novel flexible sperm-like nanorobots based on a simple and facile preparation method. Based on tunable electrochemical deposition of flexible flagella and self-assembled bonding with magnetic nanobeads, the mass produced sperm-like nanorobots were endowed with flexible head-to-tail structures. The integrated nanorobot was actuated in glycerin solution and exhibited effective bidirectional locomotion properties with respect to the dynamic magnetic fields. Motion velocities under diverse magnetic fields were measured, showing the directions were mainly determined by the actuation parameters including field intensity, frequency as well as spatial directions. Under a precessing magnetic field of 70 Gs at $\theta = 40^\circ$, the nanorobot could be actuated forward to reach a high velocity at 4.86 $\mu$m/s (about 0.37 body length/s), and backward velocity of 3.17 $\mu$m/s (about 0.24 body length/s) could also be achieved when turning the field direction. Based on tuning the actuation fields, swimming forward and backward could be switched without turning around, which was useful for flexible motion control in viscous fluids. This work demonstrated ultrasmall flexible sperm-like nanorobot with effective bidirectional propulsion under magnetic actuation, which provided significant exploration of reliable nanorobotic models at low Reynolds numbers. In future work, it is necessary to explore group manipulation and further biomedical applications of such nanorobots.

**Declarations**

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**Author contributions statement**

N.C. and D.G. contributed equally to this work. N.C. performed the fabrication and characterization. D.G. conceived the ideas and performed the magnetic actuation experiment. N.C. and D.G. participated in discussions, wrote and reviewed the manuscript. J.C. supervised the project and reviewed the manuscript.

**Competing interests**

The authors declare no competing interests.

**Additional information**
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References


**Figures**
Figure 1

(a) Schematics of the fabrication process of the sperm-like nanorobots. (b-c) SEM image and EDS results of the as-prepared Au/PPy nanowire. (d-e) Structural schematics and SEM image of the self-assembled sperm-like nanorobot.
Figure 2

(a) Time-lapse images of a sperm-like nanorobot's flagellar oscillation over one propulsion period ($T=0.5$ s) actuated under externally applied precessing magnetic field ($B=100$ Gs, $f=2$ Hz, $\theta=30^\circ$). The insets were morphing postures of the nanorobot at corresponding stages, and the stack image was also shown to demonstrate the whole oscillation process under magnetic actuation. (b) The plot describes the nanorobot's oscillation angles observed in the two-dimensional view under continuous magnetic actuation. The dashed blue line is the real-time oscillation angle of the applied precessing magnetic field. (c) The position displacement of the nanorobot’s head and tail tip in the oscillation process under
Figure 3

(a) Definition of various spatially oriented precessing magnetic fields with respect to the sperm-like nanorobot. (b) Schematics of a sperm-like nanorobot actuated by a precessing magnetic field in triaxial Helmholtz coils. (c) Time-lapse images of a nanorobot's motion under magnetic fields of diverse precessing directions and angles, which were set at a constant strength (100 Gs) and frequency (40 Hz). The position of the nanorobot is marked with an enclosing dashed rectangle box. Scale bars: 15 μm.
Figure 4

Locomotion velocity of the sperm-like nanorobots actuated under various types of precessing magnetic fields (HF-CCW, HF-CW, FF-CCW, FF-CW) with given parameters (field strength $B$, precession angle $\theta$) over a frequency range (5-40 Hz). (a1-a3) $B=50$ Gs, $\theta=10^\circ$, 30°, 60°. (b1-b3) $B=70$ Gs, $\theta=10^\circ$, 30°, 60°. (c1-c3) $B=100$ Gs, $\theta=10^\circ$, 30°, 60°.
Figure 5

Locomotion velocity of the short-tailed nanorobot actuated under a 100 Gs precessing magnetic fields (HF-CCW, HF-CW, FF-CCW, FF-CW) over a frequency range (5-40 Hz) at given precession angles $\theta$. (a1-a3) $\theta=10^\circ, 30^\circ, 60^\circ$.

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