

# The challenge of designing accelerated indoor tests to predict the outdoor lifetime of perovskite solar cells

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## Article

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2   **of perovskite solar cells**

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21 **Abstract**

22 Over the past decade, perovskite solar cells have travelled an amazing way towards high  
23 efficiency. However, a major roadblock remaining is the operational stability, while achieving  
24 technological maturity and proving real-world stability is crucial to gain trust among investors.

25 In that sense, it is of high interest to be able to predict the operational lifetime, which needs to be in  
26 the range of years or decades, within an experimentally reasonable timeframe. Yet, peculiarities of  
27 perovskite solar cells' ageing behaviour lead to severe difficulties in translating the results of indoor  
28 tests to their outdoor counterpart. In particular, transient processes cause diverse results among  
29 different ageing tests.

30 Here, for the first time, we show a complete set of constant illumination indoor testing, cycled  
31 illumination indoor testing and real-world outdoor testing on equal in-house devices. Exemplarily,  
32 we compare two different types of perovskite solar cells, in which only the hole-transport layer is  
33 varied. Despite this small change, the devices show distinctly different transient behaviour. In either  
34 case, the commonly used constant illumination experiments fail to predict the outdoor behaviour of  
35 the cell. Yet, we observe a good correlation between the cycled illumination test and the outdoor  
36 behaviour of one of the two solar cells, while this is not the case for the other system. This result  
37 highlights the urge for further research on how to perform meaningful accelerated indoor tests to  
38 predict the outdoor lifetime of perovskite solar cells.

39

## 40 **Introduction**

41 Perovskite solar cells (PSCs) are a rapidly developing photovoltaic technology<sup>1</sup>. The next step  
42 on the path towards commercialisation is to surmount the challenge of stability under outdoor  
43 operation conditions. Despite significant improvement of PSC stability with respect to light, heat, and  
44 humidity achieved over recent years<sup>2,3</sup>, this class of solar cells' stability under outdoor operation  
45 remains almost unexplored. This is one of the first studies reporting on maximum-power-point-  
46 tracked outdoor installed PSCs samples<sup>4</sup>. Obviously, understanding real-world device operation and  
47 stability is an essential element in technology maturing and fosters trust in the new technology among  
48 investors. That trust in the reliability of a technology is especially important in photovoltaics, as  
49 expected service time is in the range of 25-30 years. The required investment is almost completely  
50 required initially and commercial viability depends crucially on minimal and predictable technical  
51 degradation of the photovoltaic installation. In order to guide the development of accelerated ageing  
52 tests in the lab, we present first insights into the challenges of translating the results of indoor tests to  
53 the real-world performance of perovskite solar cells.

54 Over the past years, it took significant efforts to develop reliable and reproducible laboratory  
55 measurements for testing PSCs' efficiency. This difficulty was mainly due to ionic movements<sup>5,6</sup> and  
56 other slow transient processes<sup>7</sup> affecting perovskite solar cells. Thus, PSCs are not compatible with  
57 the classical methods used to estimate current-voltage characteristics (JV). Broad discussion in the  
58 research community has resulted in widely recognised common practices for efficiency estimation  
59 under standard test conditions (STC)<sup>8,9</sup>. The most obvious conclusion was introducing maximum  
60 power point tracking (MPPT) to validate the value extracted from JV scans.

61 More recently, the influence of transient behaviour in PSCs was found relevant in studying the  
62 long-term stability of devices<sup>10,11</sup>. The origin of that behaviour is the coexistence of several dynamics  
63 with characteristic times spanning from timescales of seconds to hours<sup>12</sup>. Such slow dynamics are  
64 relevant in the day-night cycling of devices in operational condition and need to be considered to  
65 estimate PSCs' energy yield over the device's lifespan. Although a consensus on the particular ageing  
66 tests to assess PSCs' stability has been agreed on<sup>13</sup>, there is no clear strategy to predict the PSCs'  
67 *outdoor* lifetime from accelerated indoor ageing. Despite the scarce experience in this area, available  
68 data already suggests that innovative ideas are needed to overcome the challenges<sup>11,14</sup>. The main  
69 challenges include a diverse diurnal behaviour of perovskite cells caused by slow transient processes  
70 that affect the performance over the day-night or degradation-recovery cycle. Those transients, whose  
71 nature depends on the type of solar cell investigated, make the extraction of cell parameters (*e.g.*

72 temperature coefficients) from outdoor data unreliable and complicate the investigation on the  
73 relation between outdoor and standard indoor tests.

74 This work analyses available literature and in-house data on PSCs' outdoor and indoor ageing  
75 behaviour, outlines challenges in predicting operational lifetime through accelerated ageing tests and  
76 suggests strategies to overcome those.

77

78 **Outdoor Testing**

79 To achieve the prediction of a realistic outdoor lifetime of PSCs with an accelerated indoor test,  
80 it is essential to understand the temporary changes in device power output due to weather conditions  
81 and the state of the device. This section will discuss the shortcomings of existing PSCs' outdoor data  
82 thus far, showcase the difficulty to extract valid device parameters from outdoor tests, and provide  
83 examples of different transient processes in PSCs that affect their energy yield and lifetime.

84 Despite the extensive research activity in the field of perovskite solar cells, only few papers so  
85 far reported the cells' behaviour under outdoor conditions, amongst those only one under MPP-  
86 tracking. Table S1 provides a summary of the publications known to the authors. The majority of  
87 these papers focuses on PSCs' stability and utilises outdoor conditions as a realistic combination of  
88 stress factors. According to the ISOS-protocols<sup>13,15</sup>, outdoor-related ageing experiments are classified  
89 into three groups. While ageing occurs under outdoor conditions in all protocols, the characterising  
90 measurements and the electronic load during ageing are varied. According to ISOS-O-1 periodic JV-  
91 measurements are performed under a solar simulator indoor, while ISOS-O-2 requires the periodic  
92 acquisition of JV-curves under the natural solar light outdoors. Whereas in those protocols, the  
93 electronic load during ageing outdoors can be MPP *or* open circuit, ISOS-O-3 demands for  
94 continuous maximum power point tracking and periodic JV-scans in STC. Almost all reports so far  
95 rely on the two former protocols, and mostly the devices were at open circuit during the ageing.  
96 However, although not specific to PSCs<sup>16</sup>, the electric load condition is critical particularly in  
97 perovskite-based devices, mainly due to their sensitivity to ion redistribution<sup>17</sup>. The operational load  
98 has significant implications on the degradation mechanisms and measured device lifetime<sup>18</sup>. PSCs'  
99 degradation is often (but not always<sup>19</sup>) fastest at open circuit<sup>18</sup>. Also, in any real application, the solar  
100 cell will be operated at MPP. The strong dependence of PSCs' ageing behaviour on the electronic  
101 load and MPPT being the only realistic load condition highlights the importance of conducting ageing  
102 experiments under MPPT.

103

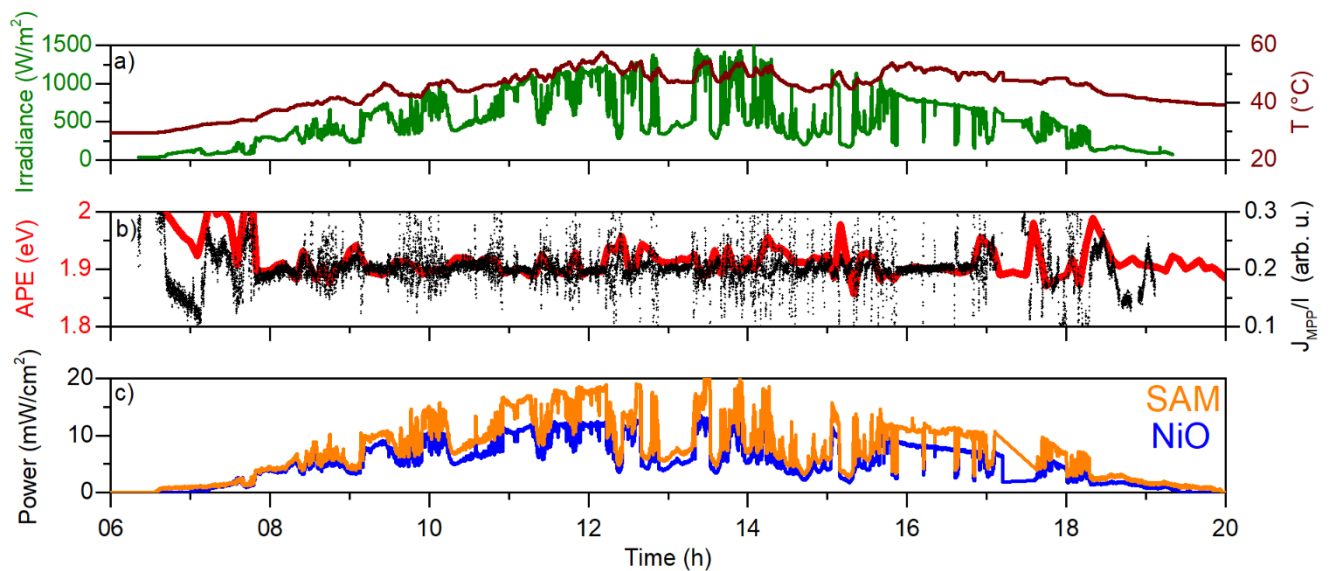


Figure 1: Impact of real-world stresses on the PSC's power output: One day of outdoor exposure of PSCs with organic self-assembled monolayers (SAM) and NiO hole transport layers. The respective power output c) measured via MPP tracking closely follows the measured irradiance a). The average photon energy (APE) in b), is calculated from spectral data measured in the plane of samples and plotted next to the ratio of  $J_{mpp}$  to irradiance (black dots in b)) to highlight the effect of the sun spectrum.

104 Figure 1 shows an example of MPP output from two different p-i-n PSCs during one day of  
 105 outdoor testing together with measured irradiance and temperature during that day. The examined  
 106 cells are comprised of the following layer stack: ITO/HTL/Cs<sub>5</sub>(MA<sub>15</sub>FA<sub>85</sub>)<sub>95</sub>Pb(I<sub>85</sub>Br<sub>15</sub>)<sub>3</sub>/C<sub>60</sub>/SnO<sub>2</sub>/Cu;  
 107 the hole-transport-layer (HTL) was varied. As one option for the HTL, NiO was used, which is the  
 108 "standard" for stable p-i-n devices<sup>20</sup>, while as other HTL the newly developed self-assembled-  
 109 monolayer (SAM) "MeO-2PACz"<sup>21</sup> ([2-(3,6-dimethoxy-9H-carbazol-9-yl)ethyl]phosphonic acid)  
 110 was used. A variant of this molecule, the "MeO-4PACz", recently gained attention since it enabled a  
 111 record perovskite-silicon monolithic tandem solar cell<sup>1,22</sup>.

112 As with other PV technologies, PSCs' power output depends on irradiance, temperature, solar  
 113 light spectrum, and incidence angle. As can be seen from Figure 1 a) and c), the power output of the  
 114 solar cells resembles the measured irradiance, which is due to the linear dependence between  
 115 irradiance and MPP current density ( $J_{MPP}$ ), see Figure S3. Yet, the  $J_{MPP}$ -to-irradiance ratio is not a  
 116 straight line as shown in Figure 1b. Some deviations from this linearity are caused by changes in the  
 117 incident sunlight spectrum. They coincide with changes in the average photon energy (APE) of the  
 118 incident spectrum, which is a technology-agnostic figure of merit of the spectrum (see Eq. S1 for the  
 119 definition)<sup>23,24</sup>. In essence, a blueshift (higher average photon energy) in the incident spectrum leads  
 120 to a marginally improved device current, while a redshift (lower energy) leads to a marginal decrease.



121 With outdoor data available, a logical next step to take -also for investors- would be energy  
122 yield predictions and analyses <sup>25-27</sup>. However, we advise caution here, since the extraction of  
123 parameters from outdoor data might lead to a misinterpretation in case of PSCs. For example, E.  
124 Velilla *et al.* found temperature coefficients insignificant for PSCs <sup>26</sup>. Stoichkov *et al.* even observed  
125 PSCs' temperature coefficients being positive in some cases when derived from outdoor data<sup>25</sup>,  
126 meaning that device efficiency improves with temperature. While a positive temperature coefficient  
127 may correlate to annealing effects or ion redistribution, it might also be entirely misleading due to  
128 unaccounted transient behaviour overlapping with temperature effects in real-world conditions. Table  
129 S3 summarises reported temperature coefficients obtained from either indoor or outdoor data. When  
130 measured indoor, temperature coefficients of PSCs are negative like in all other PV technologies,  
131 lying in the range of approximately -0.1 to -0.3 %/K. An exception poses devices with Spiro-  
132 OMeTAD, which show a non-linear dependence due to a peculiarity of this hole transporting  
133 material <sup>28,29</sup>.

134 Since reports of PSC temperature coefficients are scarce at the moment, in Figure 2, we compare  
135 the temperature coefficients at different light intensities derived from indoor and outdoor  
136 measurements on the same set of samples. The two different hole-transport layers are used in an  
137 otherwise identical stack. The devices show temperature coefficients from app. -0.1 to -0.3 %/K when  
138 measured in a controlled indoor environment after saturating the light-soaking effect (see SI for  
139 details), which is in the expected range. However, we observe significantly different values from  
140 outdoor data on the same type of devices, including some positive coefficients (see SI for details of  
141 calculation). Positive correlation in outdoor power with temperature was also reported to GaAs solar  
142 cells and explained by temperature-correlated spectral changes<sup>30</sup>, which we believe cannot explain  
143 results reported here. Instead, we believe that the discrepancy shown in Fig. 2 arises due to the  
144 presence of reversible processes that affect the PSC's daily behaviour and hence prohibit  
145 straightforward data interpretation. Indeed, the hottest part of the day is typically midday, meaning  
146 that the natural periodic increase in device temperature overlaps with reversible periodic transient

147 processes in PSCs, affecting calculated values. This example showcases that caution must be taken  
148 when extracting PSC parameters from outdoor data.

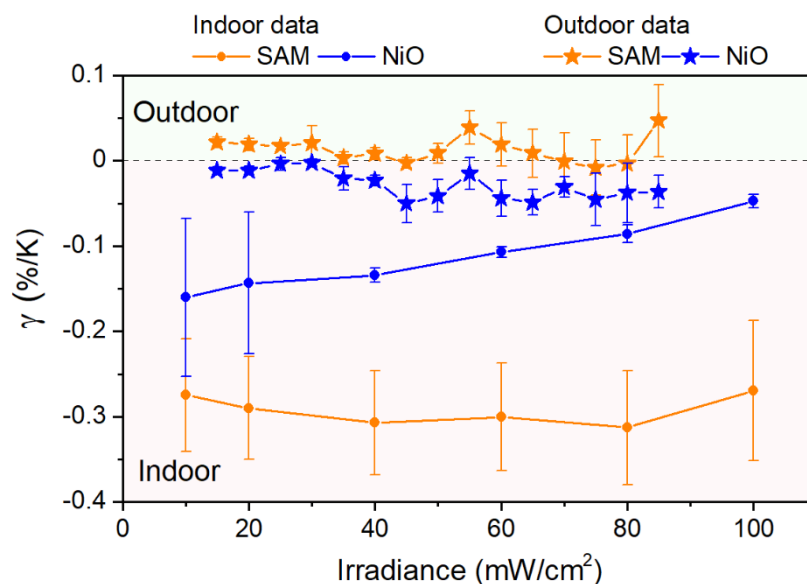


Figure 2: Care needs to be taken when extracting device parameters from outdoor measurements: Temperature coefficients of two types of PSCs with different HTMs at different light intensities, calculated from indoor and outdoor measurements.

149 Transient effects not only complicate the extraction of device parameters, but also influence the  
150 diurnal behaviour in outdoor conditions. Two different reversible transient patterns have been  
151 reported for PSCs<sup>10</sup>. In one case, cells are losing efficiency upon operation and recover during the  
152 following dark period. The opposite is also known: some perovskite cells improve upon light soaking  
153 and lose efficiency when put into the dark. It was also observed that the time under illumination  
154 required to reach peak performance might increase with consecutive cycles. This effect is called  
155 fatigue. In this paper, we refer to *fatigue* as any change in shape or absolute height of MPP-efficiency  
156 over time curves with increasing number of cycles.<sup>31,32</sup> Transient processes in PSCs can occur on a  
157 timescale of hours (sometimes even hundreds of hours<sup>33</sup>) under illumination<sup>34</sup> or in the dark<sup>35</sup>. The  
158 exact type of PCE evolution varies depending on the device stack and degradation stage<sup>12</sup>.

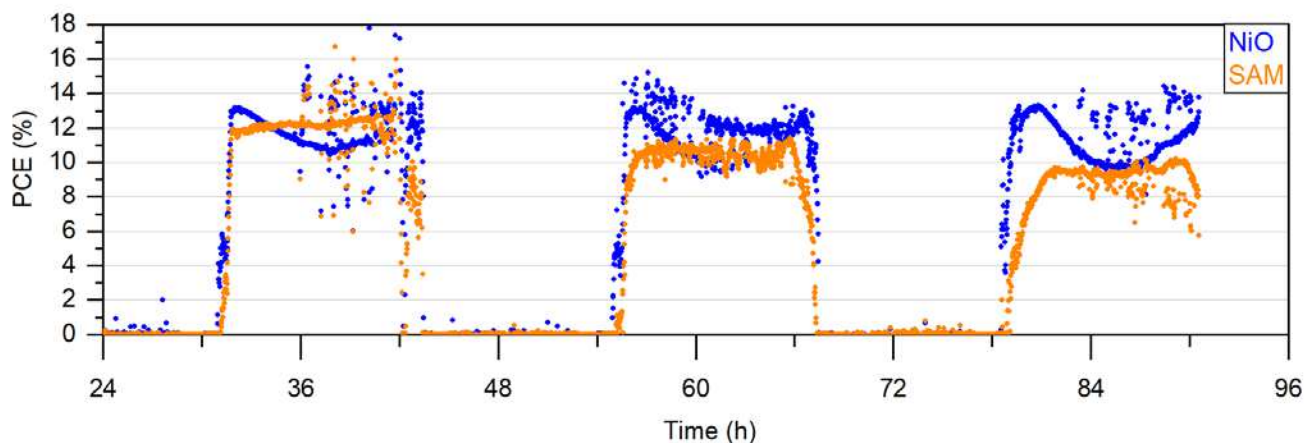


Figure 3: Exemplary PCE of two types of PSCs with different HTMs during three consecutive days of outdoor MPP-tracking

159 As an example, Figure 3 shows the power conversion efficiency of two different stacks of p-i-n  
 160 PSCs under MPPT in outdoor conditions during three consecutive days. While the only difference  
 161 between stacks is the hole transport layer, these two types of cells show dramatically different day-  
 162 night behaviour patterns. PSCs with NiO perform best in the morning, slowly degrade over the day  
 163 and recover to almost initial values overnight, while already starting to recover in the evening hours.  
 164 Relatively high series resistances contribute to this behaviour, possibly explaining a better  
 165 performance at low irradiance in the evening (see Figure S4). However, since evening values are still  
 166 noticeably below morning ones, we assume the impact of reversible degradation. On the contrary,  
 167 PSCs with SAM require several hours (strongly depending on the day of observation) to reach their  
 168 peak efficiency.

169 It is not always easy to judge such transient behaviour from indoor experiments, partly due to  
 170 frequent practice of removing the initial "stabilisation" phase from the reported PSC ageing curves.  
 171 We strongly recommend providing full datasets, because under the natural day-night cycle in outdoor  
 172 conditions, initial transient processes might have a significant contribution to the observed behaviour.  
 173 Although not necessarily detrimental for the long-term device stability in a constant light experiment,  
 174 such transients might significantly contribute to PSCs energy yield in outdoor tests. These transients  
 175 have to be considered for optimising the devices for outdoor applications. We encourage the  
 176 community to report more information on the devices' light-soaking behaviour and recovery even for  
 177 standard constant illumination experiments, like the time-to-maximum, time-to-saturation of  
 178 recovery and the extent of recovery (see Figure S5 for schematics).

179           The presence of reversible processes makes the commonly used constant illumination tests a  
180 suboptimal proxy for device stability and complicate the comparison between indoor and outdoor  
181 ageing tests in PSCs. Transients changing with each cycle obviously cannot be present in a constant  
182 illumination test. This challenge will be discussed in detail in the next section.

## 183 Comparing Indoor and Outdoor

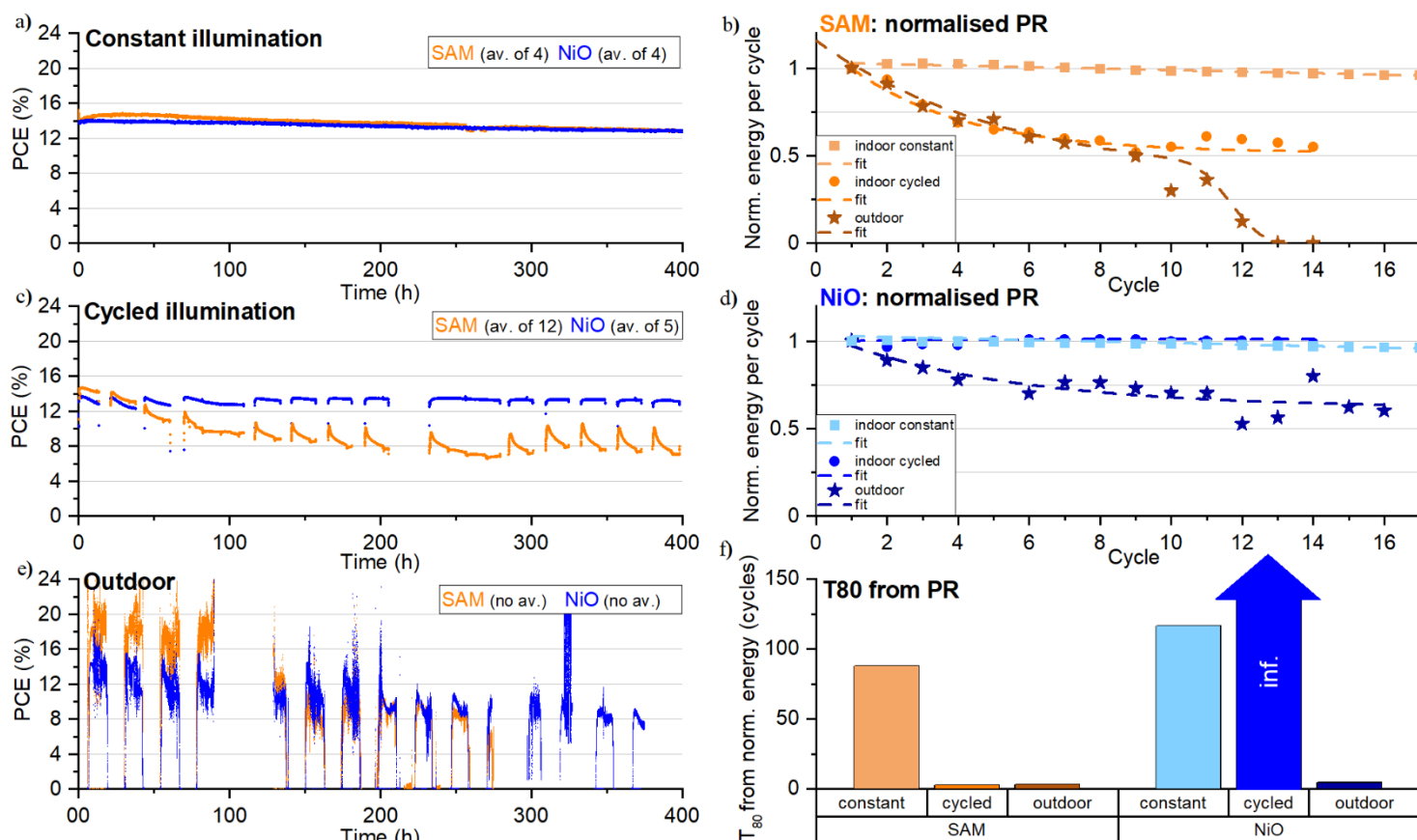


Figure 4: Comparison of indoor and outdoor stability for two solar cells using a different HTL. a) Indoor experiment with constant illumination. c) Indoor experiment with cycled illumination. Both indoor experiments are conducted at 25 °C and in nitrogen. e) Outdoor experiment, conducted in Berlin, July-August 2020. Values not averaged for better display; averaged performance ratio over 5 and 6 cells as well as another outdoor run in Figure S6. All experiments a) c) e) are performed under continuous MPP-tracking. b),d): Integrated power output divided by integrated irradiance (performance ratio), integrated over 12 h, one cycle or one day, then normalised to the first day. f) T<sub>80</sub> calculated from b) and d).

184 As a first step towards predicting outdoor lifetime with indoor testing, we present a comparative  
 185 study with indoor and outdoor data. Three different ageing tests, indoor and outdoor, have been  
 186 performed (see Table 1).

187 In our study, both types of solar cells were tested at first under constant ageing conditions  
 188 indoors. These were in brief: 100 mW/cm<sup>2</sup> continuous illumination by a solar simulator (Figure S1  
 189 displays the spectrum), MPP-tracking, 25 °C actively controlled sample temperature, measurements  
 190 under nitrogen atmosphere. The test corresponds to the protocol ISOS-L1-I, and the results are shown  
 191 in Figure 4a (averages of 4 cells each). Secondly, a cycled indoor experiment was performed on  
 192 another set of samples. It was conducted under the same conditions, but the illumination was switched

193 on for periods between 13 h and 38 h. Then, cells were put into the dark and disconnected for periods  
 194 between 8 h and 25 h (see Figure 4c, averages of 5 and 12 cells). The test corresponds to ISOS-LC-  
 195 1-I. Finally, another set of samples were encapsulated between two glasses using acrylic glue and  
 196 exposed outdoors with continuous MPP tracking (Berlin, July-August 2020) according to the ageing  
 197 protocol ISOS-O-2 (see Figure 4e, averages of 5 and 6 cells). Note that there is a data gap from 4<sup>th</sup>  
 198 day evening to 6<sup>th</sup> day morning. Weather conditions (irradiance, ambient and cell temperature,  
 199 relative humidity) were simultaneously recorded and are shown in Figure S7.

200

201 Table 1: Conditions of the performed ageing tests.

	<b>Test 1</b> "Constant illumination"	<b>Test 2</b> "Cycled illumination"	<b>Test 3</b> "Outdoor"
<i>light source</i>	simulated light, 100 mW/cm <sup>2</sup>	simulated light, 100 mW/cm <sup>2</sup>	solar light
<i>illumination</i>	constant	cycled	varying
<i>temperature</i>	25 °C actively controlled	25 °C actively controlled	varying
<i>electronic load</i>	MPP-tracking	MPP-tracking	MPP-tracking
<i>test atmosphere</i>	N <sub>2</sub> flow	N <sub>2</sub> flow	air (encapsulated)
<i>encapsulation</i>	none	none	glass to glass, acrylic glue, N <sub>2</sub>
<i>system</i>	open	open	closed
<i>ISOS protocol</i>	ISOS-L1I	ISOS-LC-1I	ISOS-O-2
<i>Figure</i>	4a	4c	4e

202

203 When analysing the constant indoor test (Figure 4a), it seems that the overall stability is very  
 204 similar. However, the tracks' slope is different, and the curves are crossing each other after ~420 hours  
 205 of testing (see the full test in Figure S8). Consequently, NiO could be considered more stable in this  
 206 test with a T<sub>80</sub> (i.e. the time it takes for PCE to decrease 80% of initial value) of 835 h, while SAM's  
 207 T<sub>80</sub> equals 580 h.

208 The behaviour changes significantly when the illumination is cycled (Figure 4c). Within each  
 209 illumination period, for both stacks, the efficiency rises very fast at first and appears almost like a  
 210 vertical line at the beginning of each cycle; compare to Figure S9, where one cycle is displayed in  
 211 detail. This rise takes around 1 h and does not originate from the algorithm finding the MPP since  
 212 that happens within a timescale of minutes. For NiO, this initial rise in efficiency is faster and less  
 213 pronounced than for SAM. After reaching the maximum value, PCE starts to drop over time until the  
 214 illumination phase is over in both stacks. For SAM, this decay phase is of exponential shape, while  
 215 for NiO it is less pronounced and appears to be linear. With an increasing number of cycles, the shape  
 216 of the curves changes for both systems. As discussed before, this change in transient behaviour with

217 a growing number of ageing cycles is called fatigue<sup>31</sup>. For cells utilising SAM, the decay becomes  
218 steeper with increasing number of cycles.

219 Additionally, the maximum value reached drops dramatically during the first 5 days and then  
220 saturates until day 10 for SAM. For NiO, however, the curves decay only during the first 5 days and  
221 recover to nearly the initial value during the dark phase. After 5 days, the efficiency stays mainly  
222 constant after the initial rise of each cycle. The tracks of the outdoor experiment (Figure 4e) have  
223 been discussed before. It can be highlighted here that the two stacks' transient behaviour is  
224 substantially different and seems to interplay with the changing outdoor conditions.

225  
226 To compare the data, we computed the so-called performance ratio (PR) for all three ageing  
227 experiments with equation (1).

$$228 \quad \text{performance ratio} = \frac{\int_{t_1}^{t_2} P_{mpp} dt}{PCE \cdot \int_{t_1}^{t_2} \text{irradiance} dt} \quad \text{Equation (1)}$$

229 Here, the power output is integrated over a given time interval and divided by the integrated  
230 irradiance multiplied with the initial PCE measured at standard test conditions.<sup>36</sup> The PR therefore  
231 reflects the efficiency over the course of a full day. We then normalised the PR to the energy output  
232 of the first day.

233  
234 In real operation and outdoor experiments, energy can naturally be harvested only during the  
235 daytime, and the effective illumination time depends on the location and the time of the year.  
236 Consequently, the integration was performed over 24 h for the outdoor experiment. The cycled indoor  
237 illumination period was varied between 13 and 38h; here, the performance ratio was integrated over  
238 a full illumination cycle. For the ageing experiment with constant illumination, there is no cycle. We  
239 artificially introduced integration over equal periods of 12 h in order to have a comparable figure of  
240 merit. Figure 4b shows the normalised PR per cycle of SAM-cells for all three experimental  
241 conditions; Figure 4d shows the same for NiO. The plot enables us to compare the different datasets  
242 elegantly.

243 Solar cells utilising SAM that are tested under constant conditions behave quite differently  
244 when light-cycled in the same conditions. In the continuous light experiment, the normalised energy  
245 per cycle shows a linear decay, while in the light-cycled experiment the decay somewhat resembles  
246 an exponential shape (compare Figure S10). Since the only difference between those two indoor  
247 experiments is cycling the light, the different behaviour likely originates in recovery effects<sup>5,7,12</sup>. It  
248 seems that pausing the illumination and putting the cells to open-circuit condition harms the device

249 more than constant illumination and MPPT conditions. It appears counterintuitive that giving the cells  
250 "a rest" hurts them more than applying constant stress.

251 Interestingly, the indoor cycled PR for SAM-cells does match quite well with the outdoor  
252 experiment's ones until day 10. Then the performance drops rapidly over the next days until total  
253 failure on day 13. We assume that this is due to the breakdown of the encapsulation: As soon as water  
254 or oxygen have passed the encapsulation, the degradation rate is strongly enhanced and also leads to  
255 visual changes (see Figure S11) in the device due to perovskite decomposition<sup>37</sup>. Since passing the  
256 encapsulation is likely a diffusion process (see Figure S12), an error function can be used to model  
257 the behaviour. Hence, it instantly boosts the degradation rate, explaining the rapid drop of PR after  
258 day 10<sup>38</sup>. Despite this deviation, we were successful in reproducing the outdoor behaviour in a  
259 controlled indoor experiment in terms of trend and behaviour in this case. Still, it is evident that the  
260 two decay curves' exponential constants are different, and a lifetime prediction from the cycled indoor  
261 experiment would be erroneous. Also, it should be noted that the cycled indoor experiment is not yet  
262 accelerated since the actual test time was the same in both cases.

263 Despite these promising results for solar cells utilising SAM, the indoor cycled experiment's  
264 PR curves and the outdoor experiment's ones significantly deviate from each other for NiO. The  
265 outdoor curve again shows exponential decay, but the indoor cycled curve shows a linear behaviour  
266 without noticeable decay. The indoor cycled curve matches much better with the constant indoor one,  
267 which also shows linear behaviour but with a negative slope. This means that for NiO, the cycled  
268 cells show higher stability than in the experiment with constant illumination, which is the exact  
269 opposite behaviour to SAM.

270 The transient and fatigue behaviour appears to be fundamentally different for the two systems:  
271 It appears that with NiO, switching the light on-off is helping the devices to stay stable, while for  
272 SAM, the light switching is diminishing the cells' lifetime. The constant light experiment does not  
273 match the outdoor behaviour in either system. These main findings are also represented in Figure 4f,  
274 which displays  $T_{80}$  calculated from the normalised PR. For SAM, the outdoor behaviour was at least  
275 depicted properly by the indoor cycled experiment. However, an outdoor lifetime prediction from the  
276 indoor cycled experiment would be wrong for NiO. For this stack, we could not depict the outdoor  
277 behaviour with the indoor tests.

278 Without further experiments, it is difficult to tell why the stacks' behaviour is diverse, even if  
279 the only difference is the HTL. Possible reasons might comprise ion migration and possibly  
280 passivation effects, chemical reactions at the interface or the degradation of the HTL itself.



281           In conclusion, we found that outdoor behaviour could be reproduced with an indoor cycled  
282 experiment for cells utilising SAM. In contrast, for cells with NiO, outdoor behaviour could not be  
283 reproduced indoors. The difference is due to the diverse fatigue behaviour of the two systems.  
284

## 285 **Strategies for accelerated indoor testing**

286 Our endeavour is to conclude from an accelerated indoor test to perovskite solar cells' outdoor  
287 behaviour. The transient and fatigue behaviour of perovskite solar cells represent the main challenge.  
288 To tackle that challenge, there are three strategies: (1) to develop devices with minimal transient and  
289 fatigue behaviour, (2) to establish advanced indoor tests that are able to closely emulate outdoor  
290 degradation patterns and (3) to perform several indoor tests that deconvolve the degradation  
291 mechanisms present under the real-world combination of stresses.

292 Minimizing the transient behaviour as in (1) is one target of current PSCs research. Yet, so far,  
293 this has not been reached and consequently the community needs to treat these transients as part of  
294 device characteristics, report them, and understand the underlying mechanisms. It might still be  
295 possible to predict outdoor behaviour even from a constant load test. However, a prerequisite for this  
296 would be that the initial transient carries all the information needed.

297 The second strategy (2) is to develop suitable indoor tests to emulate real operational conditions  
298 better and eventually accelerate the ageing process in a multi-stress approach. Tress et al. follow that  
299 approach and developed a testing machine that is fed with weather data (temperature and irradiance)  
300 and reproduces these in a nitrogen atmosphere<sup>28</sup>. Recently, also Song et al. highlighted the need for  
301 advanced indoor testing procedures<sup>11</sup>. Yet, such machines are costly, complex, and require a high  
302 degree of development and will not be available in many labs. Additionally, the technical complexity  
303 will make it challenging to build testing machines with sufficient capacity in order to achieve high-  
304 throughput testing and collect significant statistics. However, it might be an option if these machines  
305 become available commercially.

306 In the third approach (3), researchers would perform different ageing tests that focus on one  
307 specific stress factor at a time. Consequently, the real-world degradation is split into a set of  
308 degradation mechanisms, each of which can be reproduced in the lab with a different ageing test.  
309 Then it might be possible to increase each stress to accelerate the test and obtain individual  
310 acceleration factors. By collecting these individual acceleration factors, it could be possible to deduce  
311 a global acceleration factor that predicts the cells' real outdoor lifetime. This approach appears  
312 appealing, even if many tests need to be conducted carefully. One major drawback of this approach  
313 is unavoidable: If stresses trigger specific degradation paths only when combined, the tests won't  
314 depict real operation anymore.

315 In any case, it must be strictly avoided that the acceleration triggers additional or unnatural  
316 degradation mechanisms. Additionally, we urge researchers to report significant statistics on any  
317 ageing test performed. The common practice of reporting single-pixel ageing tracks must be seen as

318 a starting point to tackle stability. Still, it can lead to misinterpretation and over-or underestimation  
319 of lifetimes of particular stacks.

320

## 321 **Conclusion**

322 Being able to predict the outdoor lifetime is crucial to speeding up the commercialisation of  
323 PSCs. Accelerated indoor tests, as standard (and standardized) as for other solar cell technologies,  
324 are obviously needed. Yet, those standards are not applicable to PSCs due to their transient behaviour  
325 that is not accounted for in constant illumination testing. We were able to show in this contribution,  
326 that indoor cycled illumination tests do represent outdoor behaviour well over a range of time for a  
327 SAM hole transporting layer PSC. However, the same test does not have predictive power for PSCs  
328 with a NiO hole transporting layer instead, indicating that simple cycling of the light is only a part of  
329 the solution in bridging indoor and outdoor ageing experiments.

330 Developing devices with minimal transient and fatigue behaviour is one goal of current PSCs  
331 research and would enable researchers to use existing lifetime tests. However, the pace of  
332 development may slow down commercialization. Finding indoor tests that emulate outdoor  
333 degradation patterns is necessary to come up with an adequately accurate lifetime estimate. This goes  
334 hand in hand with attempting to unravel the degradation mechanisms present under the real-world  
335 combination of stresses.

336 We point out the urge in finding appropriate and accelerating tests with immense care. Those  
337 tests need to be validated for their applicability to each specific PSC composition. More ageing data  
338 have to be reported fully and with statistical relevance, more outdoor data acquisition is needed.

339

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344

345

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347

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