

# High-performance Removal of Anti-inflammatory Using Activated Carbon from Water Treatment Plant Sludge: Fixed-bed and Batch Studies

**Alaor Valério Filho**

Federal University of Pampa - Bage Campus: Universidade Federal do Pampa

**Luana Vaz Tholozan**

Federal University of Pampa - Bage Campus: Universidade Federal do Pampa

**Aline Lemos Arim**

Federal University of Pampa - Bage Campus: Universidade Federal do Pampa

**André Ricardo Felkl de Almeida**

Federal University of Pampa - Bage Campus: Universidade Federal do Pampa

**GABRIELA SILVEIRA DA ROSA** (✉ [gabrielarosa@unipampa.edu.br](mailto:gabrielarosa@unipampa.edu.br))

Universidade Federal do Pampa <https://orcid.org/0000-0002-8831-448X>

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## Research Article

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1       **High-performance removal of anti-inflammatory using activated carbon from water treatment**  
2                               **plant sludge: fixed-bed and batch studies**

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4       Alaor Valério Filho<sup>a</sup>, Luana Vaz Tholozan<sup>b</sup>, Aline Lemos Arim<sup>b</sup>, André Ricardo Felkl de Almeida<sup>a,b</sup>,  
5       Gabriela Silveira da Rosa<sup>a,b</sup>.

6  
7       <sup>a</sup> Graduate Program in Science and Engineering of Materials, Federal University of Pampa, 1650 Maria  
8       Anunciação Gomes Godoy Avenue, Bagé, Rio Grande do Sul 96413-172, Brazil.

9  
10      <sup>b</sup> Chemical Engineering, Federal University of Pampa, 1650 Maria Anunciação Gomes Godoy Avenue,  
11      Bagé, Rio Grande do Sul 96413-172, Brazil

12  
13      Corresponding author:

14      Gabriela Silveira da Rosa

15      email: gabrielarosa@unipampa.edu.br

16      telephone: +55 53 32473664

17      fax: +55 53 32473679

18  
19      **Abstract**

20      Activated carbon from water treatment sludge (WASC) was employed as adsorbent material to remove the  
21      anti-inflammatory Nimesulide (NM) from aqueous solutions. NM adsorption was performed in batch and  
22      fixed-bed systems, evaluating pH, adsorbent dosage, adsorption kinetics, equilibrium isotherm, continuous  
23      adsorption, and simulated effluents. The kinetic data were best fitted to the Elovich model and Intraparticle  
24      diffusion reaching the equilibrium at 120 min. Langmuir model presented a better description of the  
25      equilibrium data with the maximum adsorption capacity ( $q_{max}$ ) of 274.99 mg g<sup>-1</sup> from NM adsorption by  
26      WASC. The adsorbent was tested in two simulated hospital effluents and proved to be an excellent  
27      adsorbent for removing NM from an aqueous solution with the presence of salts, sugars, and other  
28      inorganics. Finally, WASC was applied in fixed-bed NM adsorption obtaining the adsorption capacity of  
29      217.28 mg g<sup>-1</sup>.

30  
31      **Keywords:** nimesulide; adsorption; hospital effluent; adsorbent; water treatment plant sludge; factorial  
32      design

33      **1 Introduction**

34  
35      The increase of pollutants in the effluents has been considered a major problem for the  
36      environment and, consequently, for human life. This situation leads to the reduction of drinking water  
37      available (Politano et al. 2017), which is related to global climate change, population growth, industrial  
38      and agricultural activity, allied to the improper disposal of contaminants, such as pharmaceuticals in water  
39      bodies (Petrie et al. 2015).

40           Recent researches have indicated the presence of pharmaceutical compounds in effluents and even  
41 drinking water, which classify them as emerging contaminants (Sophia A. and Lima 2018). The main origin  
42 of contamination of the environment by pharmaceuticals is through domestic and hospital sewages (Seid-  
43 Mohammadi et al. 2020), since 30-90% of the ingested is eliminated in urine and feces (Miao et al. 2016).  
44 As a consequence of this contamination, the growth of resistant bacteria is causing the inefficiency of usual  
45 drugs in the treatment of several diseases (Braschi et al. 2010; Peña-Guzmán et al. 2019).

46           Regarding emerging pharmaceutical contaminants, the anti-inflammatory NM (nimesulide or 4-  
47 nitro-2-phenoxyphenyl) has stood out, due to its wide application in the treatment of pain and inflammations  
48 in medicine (Lima et al. 2013), which is a result of its great efficacy compared to similar drugs such as  
49 ibuprofen, diclofenac, and piroxicam (Singh et al. 2001). The presence of NM in high concentrations was  
50 reported by a study carried out in a sewage treatment plant in Greece (Papageorgiou et al. 2016). Seeking  
51 a solution to this problem, studies have investigated the removal of NM from effluents (Gonçalves et al.  
52 2016; Reis et al. 2016; Jauris et al. 2017; Wang et al. 2020).

53           The adsorption process has been widely applied in the removal of emerging contaminants from  
54 effluents due to its several advantages (Streit et al. 2020), such as efficiency, flexibility, low cost, simplicity  
55 in application, and low energy consumption (Ahmed 2017; Dotto and McKay 2020). Regarding the  
56 adsorption of NM in aqueous solutions, it is worth mentioning Reis et al. (2016), Jauris et al. (2017), Saucier  
57 et al. (2015), Pauletto et al. (2020) that used adsorbent materials from sewage sludge, graphene, cocoa shell,  
58 and commercial activated carbon, respectively.

59           The development of alternative adsorbents has been considered a great option for the high cost of  
60 conventional adsorbents (Puchana-Rosero et al. 2016; Rovani et al. 2016; Ribeiro et al. 2019; Silva et al.  
61 2020). In this sense, water treatment plant sludge (WTS) has been an excellent raw material (Xu et al. 2015;  
62 Valério Filho et al. 2020), as the reuse of this residue is a solution for problems related to the high cost of  
63 WTS transport, which causes it to be discarded, frequently, in nearby water bodies (Dassanayake et al.  
64 2015; Hidalgo et al. 2017). Moreover, the WTS has important characteristics such as alumina and silica in  
65 its composition that can assist in the formation of functional surface groups that have a good interaction  
66 with various contaminants present in effluents (Siswoyo et al. 2019).

67           Thus, the objective of this work was to apply activated carbon from water treatment plant sludge  
68 in the adsorption of anti-inflammatory NM. The batch analysis was done by evaluating initial pH, adsorbent  
69 dosage, adsorption kinetics, and isotherm. The study also emphasized the treatment of simulated hospital  
70 wastewater and the fixed-bed adsorption of NM by WASC, as a proposal for industrial application.

71

## 72 **2 Materials and Methods**

73

### 74 2.1 Materials and solutions

75           NM, with purity  $\geq 98\%$ , and all other reagents (analytical grade) were purchased from Sigma-  
76 Aldrich, Brazil. NM was used in this study without further purification. To improve the NM solubilization,  
77 the solution was prepared with a solution of ethanol (20% v/v).

78

### 79 2.2 Production and characterization of activated carbon

80 WTS was collected at the water treatment plant in the city of Bagé, Brazil (31°18'22.5"S  
81 54°07'20.0"W). The sample was activated with ZnCl<sub>2</sub> and CaOH<sub>2</sub> and then pyrolysis was performed at  
82 550°C for 30 min. Then acid leaching with HCl was applied to remove remaining inorganics. The activated  
83 carbon produced was named washed activated sludge carbon (WASC) and was characterized using BET,  
84 FTIR, DRX, and TGA techniques, the details can be found in a previous paper (Valério Filho et al.).

85 The reactive groups present on the surface of WASC before and after the NM adsorption were  
86 obtained by the Fourier Transform Infrared Spectroscopy (Shimadzu IR Prestige-21, Japan) technique. The  
87 spectrum was performed in the range of 500-4500 cm<sup>-1</sup> with a resolution of 4 cm<sup>-1</sup>.

88

### 89 2.3 Batch studies

90 NM solution of 25 mL (15-800 mg L<sup>-1</sup>) was added in contact with WASC (0.4-1.6 g L<sup>-1</sup>). The pH  
91 value was investigated in the range of 8 to 11 (adjusted with NaOH). A shaker (NOVA ÉTICA, 109-1,  
92 Brazil) was used to agitate the mixtures, between 5 and 240 min, at 150 rpm. The samples were centrifuged  
93 (QUÍMIS, Q222TM216, Brazil) to separate the activated carbon from the NM solution. The concentration  
94 of NM was evaluated using standard known concentrations, at the maximum wavelength of 392 nm, in a  
95 UV-VIS spectrophotometer (Kazuaki, II-226, China). Equations 1 and 2 were used to determine the  
96 adsorption capacity, ( $q_e$ , mg g<sup>-1</sup>) and removal efficiency ( $E$ , %), respectively.

$$q_e = \frac{(C_i - C_e)V}{m} \quad (1)$$

$$E = \frac{C_i - C_e}{C_i} \quad (2)$$

97 where  $C_i$  is the initial NM concentration (mg L<sup>-1</sup>);  $C_e$ , equilibrium NM concentration (mg L<sup>-1</sup>);  $M$ , the mass  
98 of WASC (g); and  $V$ , the volume of solution (L).

99

### 100 2.4 Statistical analysis

101 2<sup>2</sup> Factorial Design (FD) was applied at a 95% confidence level to understand which factor  
102 (adsorbent dosage ( $A_d$  (g L<sup>-1</sup>)) and initial pH) would have a major impact on adsorption processes and how  
103 these parameters would interact between them. This method was also used to develop a mathematical model  
104 to describe the adsorption process. Table 1 shows the independent variables and respective levels used in  
105 the experimental design.

106

107 **Table 1** Independent variables and levels of experimental design.

108

109 The FD was carried out with independent variables at 3 levels and it was arbitrated 3 repetitions  
110 of the central point to provide an estimate of pure error.

111

### 112 2.5 Kinetic and isotherm studies

113 Four kinetic models were tested to describe experimental data: the pseudo-first order, pseudo-  
114 second order, intraparticle diffusion, and Elovich kinetic models were adjusted to experimental data. These  
115 models are represented by Equations 3-6, respectively.

$$q_t = q_e(1 - e^{-k_1 t}) \quad (3)$$

$$q_t = \frac{q_e^2(k_2 t)}{(1 + q_e k_2 t)} \quad (4)$$

$$q_t = k_{int} t^{1/2} + C \quad (5)$$

$$q_e = \frac{1}{\alpha} \ln(1 + \alpha \beta t) \quad (6)$$

116 where  $t$  is the time of contact (min);  $q_t$  is the amount of NM adsorbed at time  $t$  ( $\text{mg g}^{-1}$ );  $k_1$  is the pseudo-  
 117 first order rate constant ( $\text{min}^{-1}$ );  $k_2$  is the pseudo-second order rate constant ( $\text{g mg}^{-1} \text{min}^{-1}$ );  $k_{id}$  is the rate  
 118 constant for intraparticle diffusion ( $\text{g mg}^{-1} \text{min}^{-1/2}$ );  $C$  is related to diffusion resistance ( $\text{mg g}^{-1}$ );  $\alpha$  is the  
 119 initial rate of Elovich model ( $\text{mg g}^{-1} \text{min}^{-1}$ ); and  $\beta$  is the Elovich model constants ( $\text{mg g}^{-1}$ ).

120 Langmuir and Freundlich isotherm models were applied to analyze the equilibrium experimental  
 121 data. These models are represented in Equations 7 and 8, respectively.

$$q_e = \frac{q_{max} K_L C_e}{1 + K_L C_e} \quad (7)$$

$$q_e = K_F C_e^{1/n_F} \quad (8)$$

122 where  $q_{max}$  is the maximum adsorption capacity of the adsorbent ( $\text{mg g}^{-1}$ ),  $K_L$  is the Langmuir equilibrium  
 123 constant ( $\text{L mg}^{-1}$ );  $K_F$  is the Freundlich equilibrium constant ( $\text{mg}^{1-(1/n)} \text{L}^{1/n} / \text{g}$ ) and  $1/n_F$  is the Freundlich  
 124 exponent.

125 All model parameters were defined by nonlinear regression, using the quasi-Newton method. The  
 126 adequacy of the models was analyzed by variance analysis (ANOVA) checked by  $F_{\text{value}} > F_{\text{tabled}}$ , where  $F_{\text{value}}$   
 127 is the regression coefficient. Furthermore, the models were checked by using the Chi-square ( $X^2$ ) and  
 128 average relative error (ARE) according to Equations 9 and 10, respectively.

129

$$ARE = \frac{100}{nn} \sum \frac{q_{exp} - q_{pred}}{q_{exp}} \quad (9)$$

$$X^2 = \sum \frac{(q_{exp} - q_{pred})^2}{nn - NN} \quad (10)$$

130

131 where  $q_{exp}$  are the experimental values;  $q_{pred}$  is the value of the model,  $nn$  is the experiment number observed,  
 132 and  $NN$  is the number of the parameters in the model.

## 133 2.6 Simulated hospital wastewater

134 In this study, two simulated hospital effluents were produced to evaluate NM adsorption by WASC  
 135 in the middle of sugars, high salt, urea, and other inorganics commonly found in hospital waste effluents  
 136 (Saucier et al. 2015). Table 2 shows the composition of the simulated effluents.

137

138 **Table 2** Chemical composition of simulated hospital effluents.

139

## 140 2.7 Continuous adsorption studies

141 The fixed-bed tests were performed on glass columns using 1 g of WASC. Two columns were  
 142 used, the internal diameter of column 1 is 5 mm and the bed height 50.4 mm, column 2 has an internal

143 diameter of 9 mm and 28 mm of bed height. The NM solution (200 mg L<sup>-1</sup>) was used to feed the bed with  
 144 a flow rate of 10 mL min<sup>-1</sup>. Thomas and Yoon-Nelson models were fitted to the experimental fixed-bed  
 145 data for an estimate of the kinetic parameters, they are represented in Equations 11 and 12, respectively.

$$C_t = \frac{C_e}{1 + \exp\left(\frac{K_{th} q_{th} m}{Q} - k_{th} C_e t\right)} \quad (11)$$

$$C_t = \frac{C_e}{1 + \exp(k_{yn} (\tau_h - t))} \quad (12)$$

146 were  $k_{th}$  is the Thomas rate constant (mL mg<sup>-1</sup> min<sup>-1</sup>);  $q_{max}$  is the maximum adsorption capacity of Thomas  
 147 model (mg g<sup>-1</sup>);  $Q$  is the flow rate (mL min<sup>-1</sup>);  $k_{yn}$  is the Yoon-Nelson rate constant (min<sup>-1</sup>); and  $\tau_h$  is the  
 148 time required for 50% solute breakthrough (min).

149

### 150 3 Results and Discussion

151

152 Table 3 presents the experimental design of the interaction between adsorbent dosage ( $A_d$ ) and pH,  
 153 and the results of adsorption capacity and efficiency of removal of NM by WASC.

154

155 **Table 3.** Experimental results for capacity and efficiency of NM adsorption. Conditions:  $C_i$ , 30 mg L<sup>-1</sup>;  
 156 contact time, 60 min; temperature, room temperature (25 ± 2°C).

157

158 The low standard deviation results (0.03-0.91 mg g<sup>-1</sup> and 0.10-1.96%) indicate the reproducibility  
 159 of the experiments. The highest value of  $q_e$  was 45.06 mg g<sup>-1</sup> (run 1), which corresponds to an efficiency  
 160 of 59.77%, and the highest value for  $E$  was 95.31%, which corresponds to an adsorption capacity of 17.83  
 161 mg g<sup>-1</sup>.

162 Fig. 1 presents the estimated effects in the adsorption process of NM by WASC for adsorption  
 163 capacity and efficiency. The reverse elimination process was applied in the statistical analysis of the model,  
 164 excluding non-significant dependent terms (da Rosa et al. 2019).

165

166 **Fig. 1** Pareto charts of the estimated effects on adsorption capacity (a) and efficiency (b)

167

168 Analyzing the results plotted in pareto charts it can be inferred that the pH is the most significant  
 169 effect on the adsorption capacity and efficiency of NM. Fig. 1(a) indicates that all parameters were  
 170 significant for adsorption capacity ( $p > 0.05$ ). The pH was the parameter with the most pronounced negative  
 171 effect. There is a linear dependence between the pH and the adsorbent performance, this is, the adsorption  
 172 capacity decreases with the increase of pH. The interaction between  $A_d$  and pH had a positive effect and  $A_d$   
 173 had a negative effect.

174 From the adsorption efficiency presenting in Fig. 1(b), the more pronounced effect was the pH  
 175 with the negative effect. The  $A_d$  parameters had a positive effect and the interaction between  $A_d$  and pH  
 176 was not significant ( $p \leq 0.05$ ). The  $A_d$  antagonist behavior from adsorption capacity and efficiency can be  
 177 explained by the high values of  $A_d$ , which promotes an increase in adsorption efficiency. Although it  
 178 increases the presence of free sites in WASC and, consequently, leads to the decreasing of adsorption  
 179 capacity. Due to this, the central point 1 g L<sup>-1</sup> for  $A_d$  was chosen to continue the batch tests.

180 The pH of the solution is an important factor to be observed during pharmaceutical adsorption  
 181 because affects the surface charge of the adsorbent (Arim et al. 2018). Studies have already reported that  
 182 in solutions at pH lower than 7 the NM precipitates (Saucier et al. 2015; Jauris et al. 2017). Fig. 1(a-b) and  
 183 Table 3 indicates that the best pH condition for a higher  $q_e$  was at initial pH 8. The higher the pH, the  
 184 lower the concentration of  $H^+$  ions. This indicates that the WASC surface must be negative and that  
 185 interaction between WASC-NM does not occur electrostatically (Saucier et al. 2015). The interaction  
 186 probably occurs through H bonding and van der Waals forces (Saucier et al. 2015; Jauris et al. 2017).

187 The kinetic behavior of NM adsorption by WASC and the adjustments of the pseudo-first order,  
 188 pseudo-second order, Elovich, and intraparticle diffusion mathematical models are presented in Fig. 2.

189

190 **Fig. 2** Kinetic curves and mathematical model adjustments of pseudo-first order, pseudo-second order, and  
 191 Elovich models (a) and intraparticle diffusion (b). Conditions:  $C_i$ , 30 mg L<sup>-1</sup>; pH, 8;  $A_d$ , 1 g L<sup>-1</sup>; temperature,  
 192 room temperature ( $25 \pm 2^\circ\text{C}$ ).

193

194 It can be observed in Fig. 2(a) that the sorption rate is higher at the beginning of the process because  
 195 of the greater number of active sites on the surface of the adsorbent (Arim et al. 2019). The experimental  
 196 data show that most NM was removed around 90 minutes and no significant changes in terms of removal  
 197 were observed after 120 min.

198 Fig. 2(b) presenting the limiting rate step for the adsorption process of NM onto WASC, using the  
 199 intraparticle diffusion model. Three steps can be identified in the kinetic plots. The first step is related to  
 200 the surface diffusion, with the mass transfer of the NM to the external surface of the WASC particles (Alves  
 201 et al. 2013). The second step is related to the intraparticle diffusion and the third step indicates the  
 202 equilibrium phase due to the NM occupation of all the active sites of WASC (Arim et al. 2018).

203 The kinetic parameter values obtained from the fitting of the kinetic models to experimental data  
 204 are presented in Table 4.

205

206 **Table 4** Kinetic parameters of NM anti-inflammatory adsorption in WASC.

207

208 All models were checked by the statistical significance through the regression F test and the values  
 209 obtained indicated which models presented a good fit. The Elovich and Intraparticle diffusion models  
 210 describe better the adsorption kinetic as indicated by the highest coefficient of determination,  $R^2$ , even  
 211 though the Intraparticle diffusion model shows the lowest values for  $X^2$  and ARE. The parameters values  
 212 of intraparticle diffusion obtained from NM adsorption onto WASC were  $k_{int} = 1.94 \text{ g mg}^{-1} \text{ min}^{-1/2}$  and  $C =$   
 213  $7.93 \text{ mg g}^{-1}$  which represents intraparticle rate constants and boundary layer thickness, respectively (Al-  
 214 Rashdi et al. 2012; Arim et al. 2018). The  $C$  values different from zero indicate that more mechanisms were  
 215 involved in NM adsorption (Arim et al. 2018).

216 The good fit for the Elovich model can indicate the presence of chemisorption in NM removal, not  
 217 a first-order reaction [30], such behavior is confirmed to the high adjustment for the pseudo-second order  
 218 model. This means that the NM molecule was dissociated into independent fragments creating radicals and  
 219 atoms attached to the adsorbent (Dotto and McKay 2020). The parameters  $\alpha$  ( $0.2142 \text{ mg g}^{-1} \text{ min}^{-1}$ ) and  $\beta$

220 (9.89 mg g<sup>-1</sup>) of this model represent the initial rate of chemisorption and the number of sites available for  
 221 NM adsorption, respectively. The Pseudo-first order model has also presented a good fit, which indicates  
 222 that van der Waals forces and H bonding can occur in the NM adsorption (Saucier et al. 2015; Jauris et al.  
 223 2017).

224 The equilibrium experimental data of NM adsorption onto WASC and the adjustment of the  
 225 isotherm models are presented in Fig. 3 and their parameters in Table 5.

226

227 **Fig. 3** Isotherm curve from adsorption of NM on WASC. Conditions:  $C_i$ , 15-800 mg L<sup>-1</sup>; pH, 8;  $A_d$ , 1 g L<sup>-1</sup>;  
 228  $t_c$ , 180 min; temperature, room temperature (25 ± 2°C).

229

230 **Table 5.** Isotherm parameters of NM anti-inflammatory adsorption in WASC

231

232 The isotherm curves (Fig. 3) indicate a favorable adsorption process from NM adsorption onto  
 233 WASC, it occurs when the increase of the adsorption capacity and the increase of adsorbate concentration  
 234 are proportional (Silva et al. 2020). The good results for NM adsorption can be related to the WASC surface  
 235 area of 582.0 m<sup>2</sup> g<sup>-1</sup>. Also, the predominant mesoporous size distribution (3.02 nm) for WASC (Valério  
 236 Filho et al.) and the extreme distances between the atoms of NM molecule of 0.993 nm (Saucier et al. 2015)  
 237 indicate that WASC is capable to adsorb NM anti-inflammatory.

238 The Langmuir isotherm is the best model for describing the experimental data, considering the  
 239 highest values of R<sup>2</sup> and F<sub>value</sub> and also the lowest values of X<sup>2</sup> and ARE. The maximum sorption capacity  
 240 of NM onto WASC was 274.99 mg g<sup>-1</sup>, the value is superior to studies that have already investigated the  
 241 adsorption of NM. The maximum sorption of NM previously reported in the literature was  $q_{max}$  of 14.18  
 242 mg.g<sup>-1</sup>, using a silica aerogel (Caputo et al. 2012);  $q_{max}$  of 26.12 mg.g<sup>-1</sup>, using a combination of  
 243 polysiloxanes and sewage sludge (Simões dos Reis et al. 2016);  $q_{max}$  of 66.45 mg.g<sup>-1</sup>, using activated carbon  
 244 from sewage sludge (Reis et al. 2016);  $q_{max}$  of 74.81 mg.g<sup>-1</sup>, using activated carbon from cocoa shell  
 245 (Saucier et al. 2015); and  $q_{max}$  of 82.4 mg.g<sup>-1</sup>, using a graphene material (Jauris et al. 2017). Due to the  
 246 excellent values for maximum adsorption capacity, in Fig. 4 the adsorption of NM by WASC was analyzed  
 247 in a competitive environment with other inorganics, sugars, and salts. The chemical composition of  
 248 simulated hospital effluents is showing in Table 2.

249

250 **Fig. 4** Adsorption efficiency of NM in hospital effluents treatment with WASC. Conditions: pH, 8;  $A_d$ , 1 g  
 251 L<sup>-1</sup>; contact time, 180 min; temperature, room temperature (25 ± 2°C).

252

253 The application of the adsorbent material in simulated effluent provides important information  
 254 regarding the efficiency of this adsorbent in competitive effluents (Wamba et al. 2019). The WASC  
 255 impressively adsorbed 98.57 % and 88.08 % of NM in the hospital effluent A and B, respectively. Using  
 256 activated carbon from cocoa shell, Saucier (Saucier et al. 2015) reported efficiency of 95.58 % in the  
 257 removal of NM from simulated hospital effluent using an adsorbent dosage of 2.5 g L<sup>-1</sup>. This result indicates  
 258 that WASC was a great and sustainable option for the utilization of WTS as an adsorbent for NM removal  
 259 from hospital wastewater.



260 Fig. 5 shows the continuous adsorption of NM by WASC. The influence of bed height and length  
261 was analyzed in two beds with different diameters and fixed adsorbent mass and flow rate.

262  
263 **Fig. 5.** Fixed-bed adsorption of NM onto WASC. Conditions:  $C_i$ , 200 mg L<sup>-1</sup>; pH, 8; WASC mass, 1 g;  
264 temperature, room temperature ( $25 \pm 2^\circ\text{C}$ ); flow rate, 10 ml min<sup>-1</sup>.

265  
266 Fig. 5 showed that the small internal diameters and, consequently, higher bed height provide better  
267 conditions from the NM adsorption by the WASC. This is related to the interaction time between NM-  
268 WASC in the column. The 52 mm bed height provides a longer interaction time than the 28 mm height.  
269 Such occurrence is in agreement with the kinetic curves presented in Fig. 2, where it was observed that the  
270 adsorption of NM does not occur in an instantaneous way, such behavior in fixed-bed confirms that the  
271 adsorption of NM is mainly controlled by chemisorption (Patel 2020). This means that greater bed heights  
272 will allow for better performance because the unused fraction of WASC is reduced. WASC saturation time  
273 was longer for column 1 than for column 2, this is also related to the greater use of the adsorbent bed and  
274 consequently greater adsorption capacity.

275 To describe the dynamic behavior of the column, the Thomas and Yoon-Nelson models (Equations  
276 11 and 12) were fitted to the experimental data. Table 6 summarizes the parameters found for each model  
277 and the respective error parameters ( $R^2$ ,  $X^2$  and  $ARE$ ).

278  
279 **Table 6** Model parameters of the fixed-bed NM adsorption onto WASC

280  
281 Thomas and Yoon-Nelson models showed a good fit for both columns with high values for  $R^2$ .  
282 Column 1 presents higher values from  $R^2$  and lower values from  $X^2$  and  $ARE$  in comparison with Column  
283 2. The explanation for this is that the adjustments can better predict the fixed bed curve when the adsorbent  
284 is saturated by NM molecules (Dotto and McKay 2020). The saturation of 1 g of WASC occurs for column  
285 1 obtaining  $q_{max}$  of 217.28 mg g<sup>-1</sup>.

286 Fig. 6 shows the intensity of the molecular groups present in WASC before and after the NM  
287 adsorption.

288  
289 **Fig. 6.** FT-IR spectra for WASC before and after the NM adsorption

290  
291 After the adsorption, WASC demonstrates a decrease in alcoholic and phenolic O-H groups (a)  
292 compared to before the NM adsorption, it is represented by the intense band between 3600-3400 cm<sup>-1</sup>  
293 (Calvete et al. 2010a, b; da Silva et al. 2011). The band range at 1700-1400 cm<sup>-1</sup> indicates the presence of  
294 C=O carboxylic acid stretching in WASC (b), the interference can be related to NH bend of NM (Caputo  
295 et al. 2012; Saucier et al. 2015). The 940-665 cm<sup>-1</sup> band in WASC before the adsorption, indicates the  
296 presence of bending O-H (c) (Puchana-Rosero et al. 2016). The decrease in the O-H groups may be related  
297 to the disruption of these groups due to the interaction with NM molecules through H bonding (Saucier et  
298 al. 2015; Jauris et al. 2017).

299 Based on the results of this work, it is possible to infer that the NM-WASC interaction is mainly  
300 controlled by intraparticle diffusion and chemisorption, but also presents attraction forces of H bonding.  
301 This great interaction of adsorbent-adsorbate might have positively influenced the high values obtained  
302 from  $q_{max}$  of isotherm studies and fixed-bed adsorption.

303

#### 304 **4. Conclusion**

305 The WASC showed excellent results for the removal of NM anti-inflammatory. FD was successful  
306 in predicting the optimal pH 8 and  $A_d$  values. The equilibration time was reached in 120 min and the models  
307 that better described the kinetics data were the Intraparticle diffusion and Elovich model. The maximum  
308 amount adsorbed ( $q_{max}$ ) of NM in batch tests was 274.99 mg g<sup>-1</sup> and the isotherm data were better described  
309 by the Langmuir model. WASC proved to be efficient in the treatment of hospital wastewater, obtaining an  
310 impressive adsorption efficiency of 98.57% in a competitive environment with sugars, salts, and other  
311 inorganics. Finally, WASC was used in a fixed-bed for adsorption of NM in a continuous system, obtaining  
312  $q_{max}$  values of 217.28 mg g<sup>-1</sup>, saturating in 250 min at a flow rate of 10 mL min<sup>-1</sup>. The results obtained in  
313 this work prove that WASC is an extremely promising adsorbent in the treatment of real pharmaceutical  
314 effluents.

#### 315 **Data availability**

316 Not applicable.

#### 317 **Consent for publication**

318 Not applicable.

#### 319 **Availability of data and materials**

320 All data generated or analyzed during this study are included in this published article and its supplementary  
321 information files.

#### 322 **Competing interests**

323 The authors declare that they have no competing interests.

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#### 329 **Ethics approval and consent to participate**

330 Not applicable.

331

#### 332 **Authors contributions**

333 Alaor Valério Filho: Conceptualization, methodology, investigation, formal analysis, visualization, and  
334 writing

335 Luana Vaz Tholozan: Writing and editing

336 Aline Lemos Arim: Investigation and paper review

337 André R. F. de Almeida: Formal analysis, methodology, and paper review

338 Gabriela S. da Rosa: Conceptualization, methodology, investigation, and writing of the review and editing.

339

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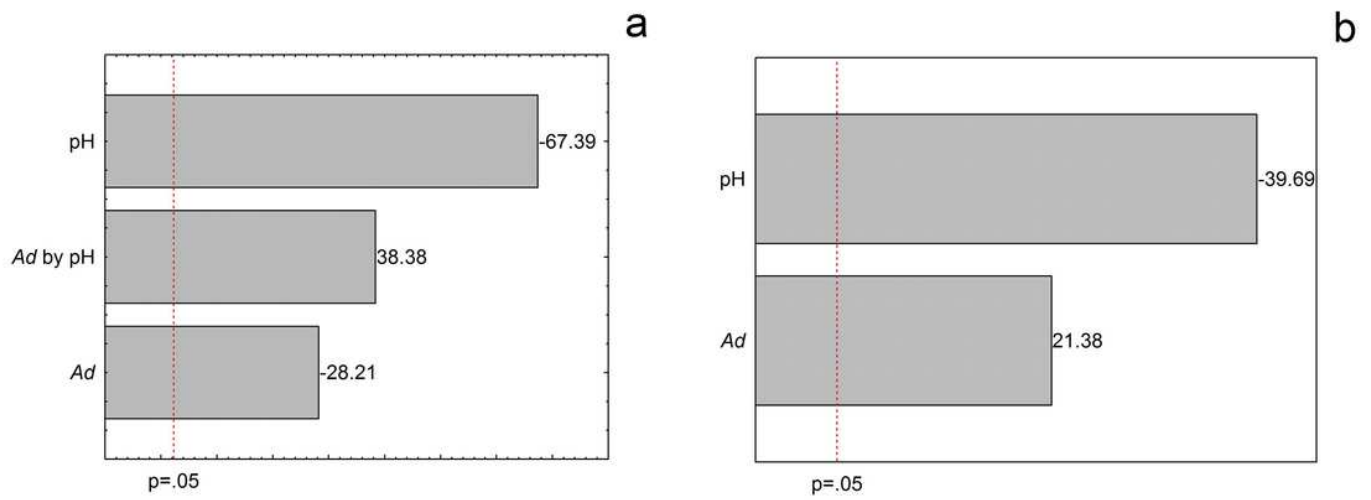
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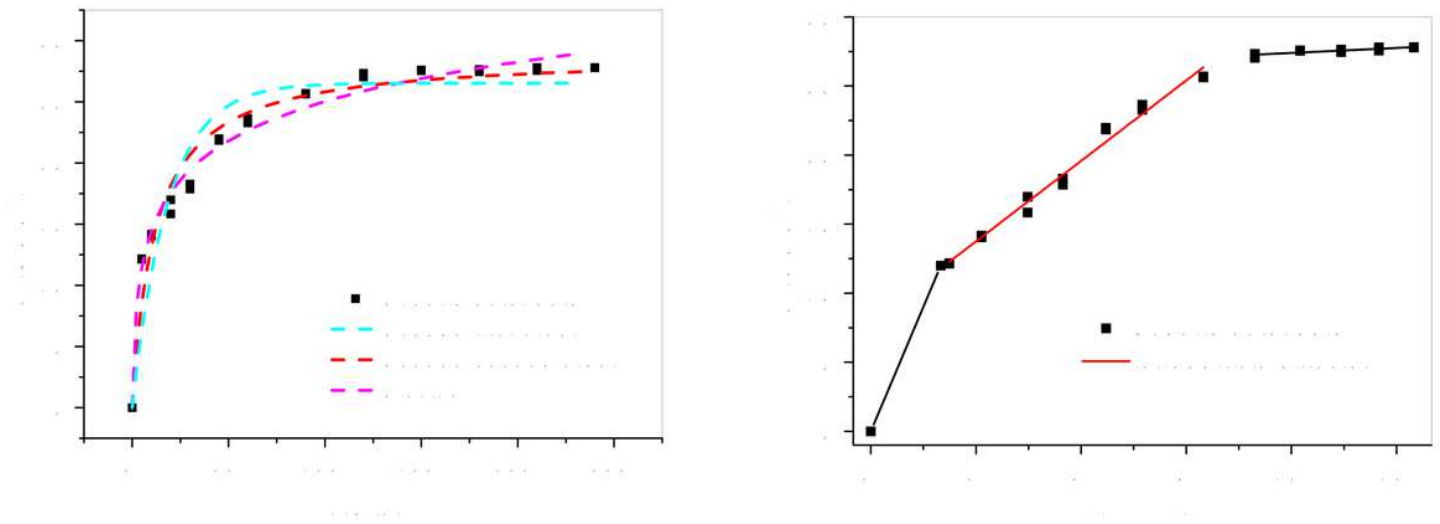
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# Figures



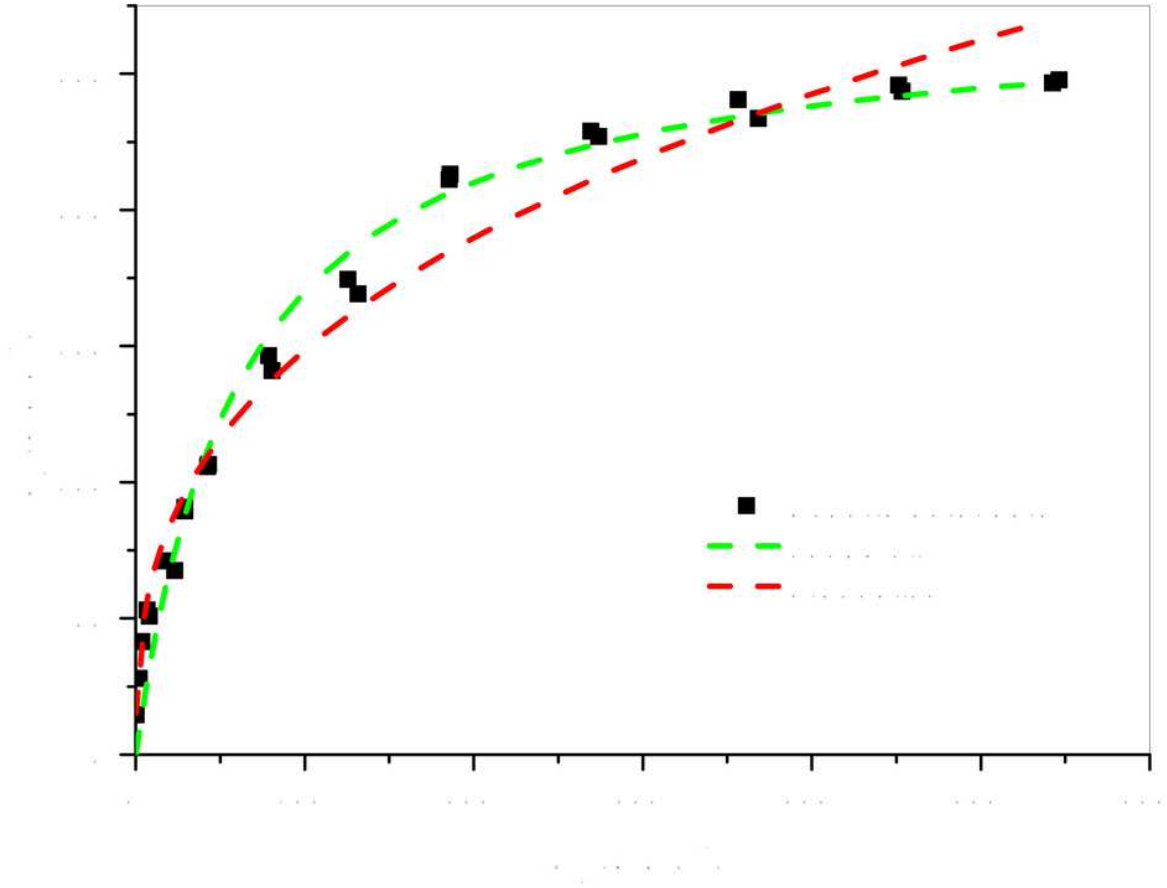
**Figure 1**

Pareto charts of the estimated effects on adsorption capacity (a) and efficiency (b)



**Figure 2**

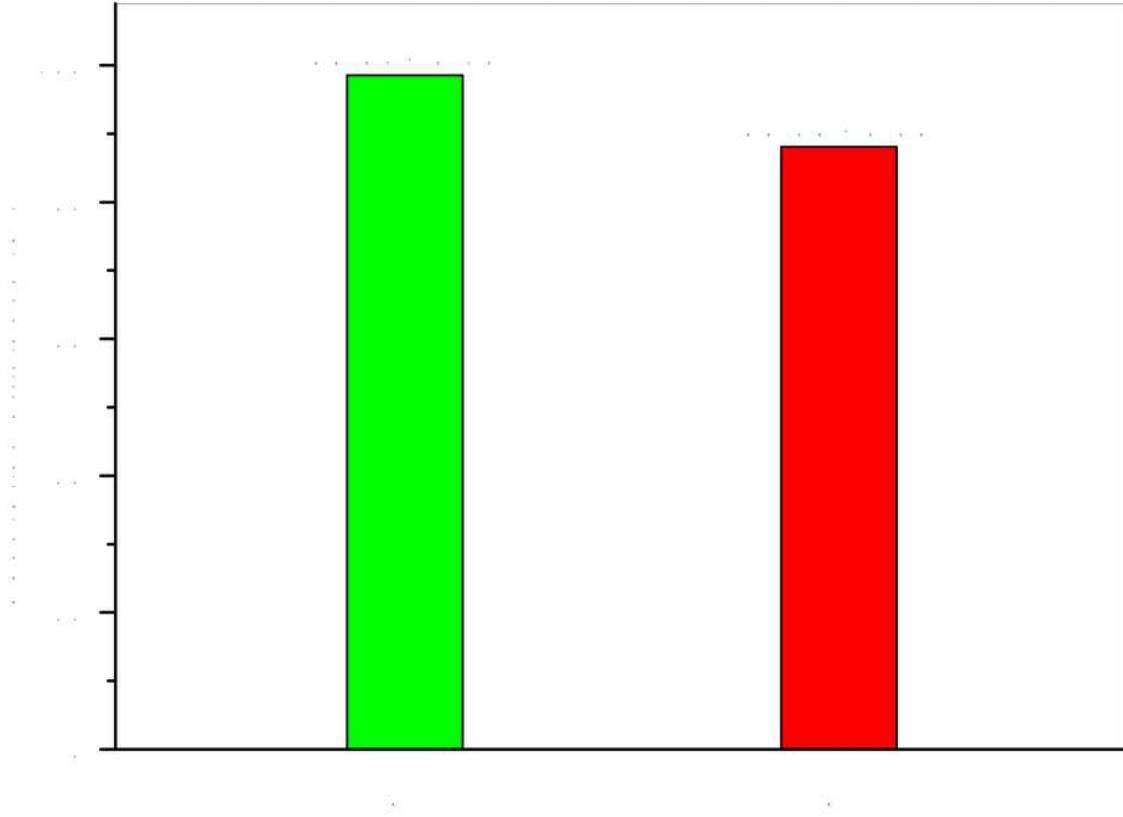
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**Figure 3**

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**Figure 4**

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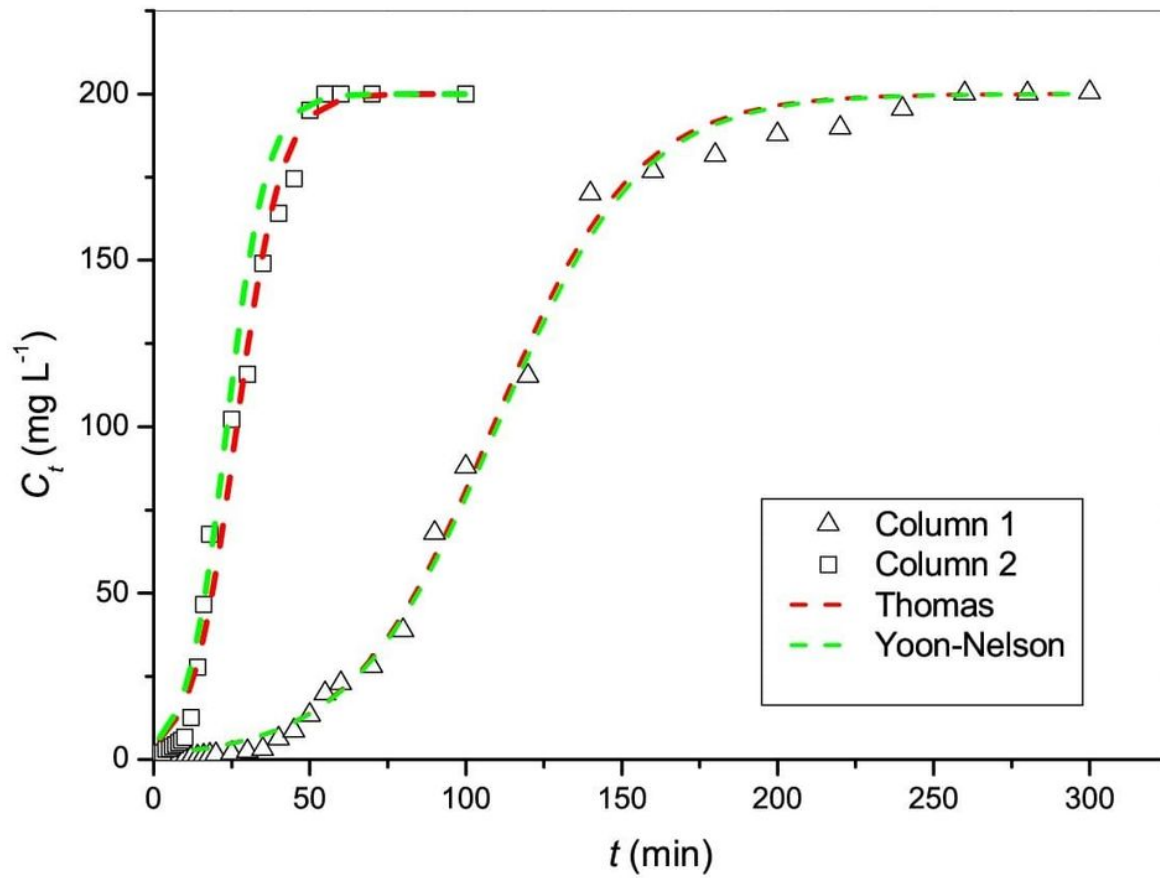


Figure 5

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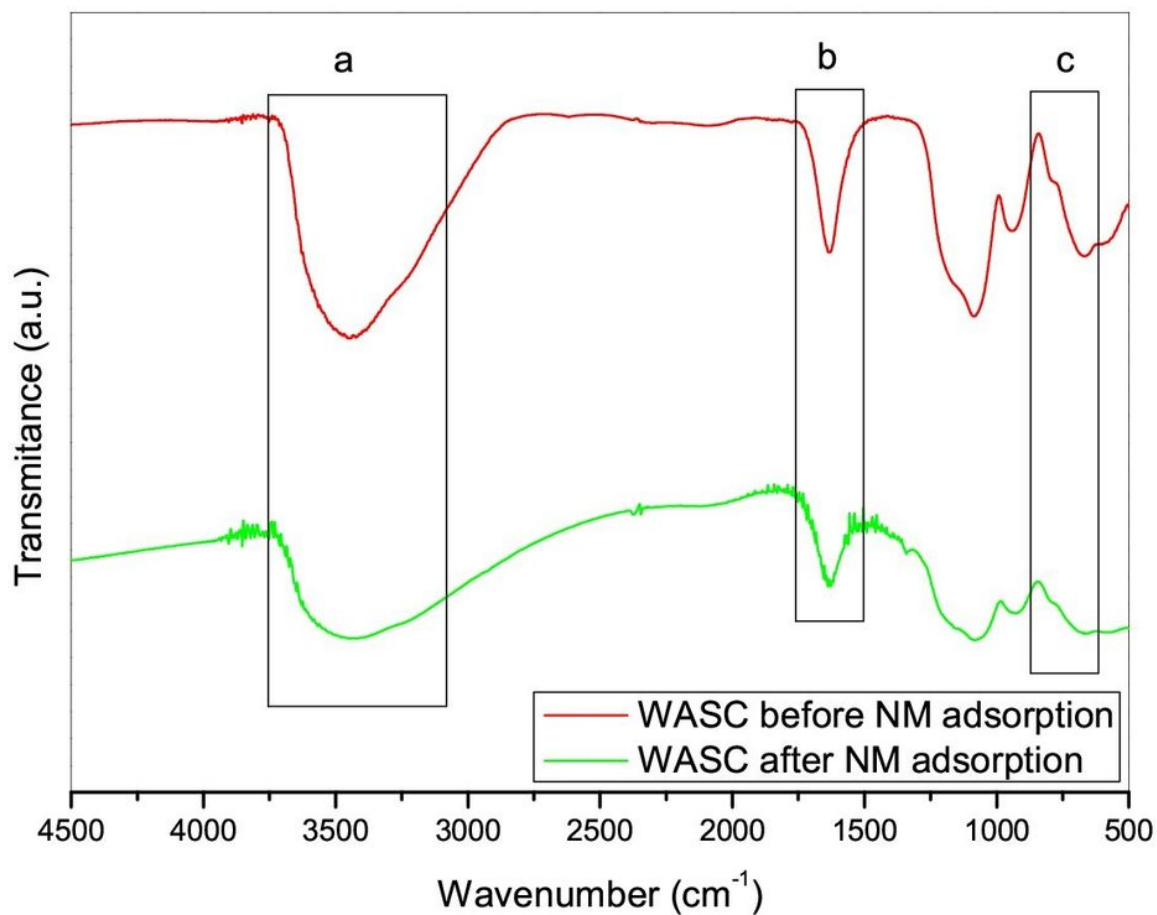


Figure 6

FT-IR spectra for WASC before and after the NM adsorption

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