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Mace-like carbon fibers/ZnO nanorods composites derived from *Typha orientalis* as ultralight and high-performance electromagnetic wave absorber

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ABSTRACT

Inspired by the nature, biomass-derived carbon attracts many attentions as the electromagnetic wave absorption (EMA) material owing to its advantages including abundant, low cost, renewable and environmentally friendly. However, it is difficult to make further breakthrough in effective absorption bandwidth (EAB) due to the impedance mismatch. In this work, mace-like carbon fibers/ZnO nanorods composites (BDCFs@ZnO) derived from *Typha orientalis* were prepared via a carbonization process and a subsequent hydrothermal process for the first time. The unique hollow structure of BDCFs and the construction of 3D interconnected conductive network led to the strong conduction loss and multiple reflection. The BDCFs sample possesses an excellent EMA performance with an ultralow filling ratio of only 5wt%. After directionally growing of the ZnO nanorods, an exceptional RL of -62.35 dB at 14.12

GHz and the EAB achieves 6.8 GHz at the thickness of 2.29 mm at a filling ratio of 15wt% were revealed. Mace-like ZnO with suitable permittivity effectively avoid the reflection result from direct contraction between EMW and carbon fiber, further improving impedance match. Simultaneously, a dielectric sum-quotient model was proposed to analyze the EMA performance of the samples. This work not only offers an inspiration for the development of dielectric loss-type EMA materials with lightweight and strong EMA performance by a sustainable, low-cost and easily available approach, but also provides an important strategy toward biomass-derived carbon-fiber-based composites in other fields.

Keywords: biomass derived-carbon fiber, ZnO nanorods, low filling ratio, EMA performance.

1. Introduction

With the rapid development of modern science and technology, the appearance of diversified kinds of electronic and electrical equipment has brought benefits and conveniences to people's life. Meanwhile, it also brings serious electromagnetic (EM) radiation and interference problems, which not only affect the normal operation of electronic equipment, but also endanger human's health and natural environment [1-4]. In order to solve these problems, the electromagnetic wave absorption (EMA) materials have become a research hotspot [5-7]. Generally speaking, EMA materials can be divided into two main groups: dielectric loss materials (TiO₂, SiC, ZnO and carbonaceous materials) and magnetic loss materials (Fe, Co, Ni and alloys) [8-10]. Although traditional magnetic EMA materials have been widely used, some

unavoidable shortcomings restrict their applications, including high density, narrow effective absorption bandwidth (EAB) and poor chemical stability [11, 12]. In contrast, carbonaceous materials such as graphene [13], carbon fiber [14], carbon black [15] and carbon nanotube [16], stand out among dielectric loss materials due to their low density, high conductivity and excellent stability [17-19].

As a traditional carbon material, carbon fiber contains more than 90% carbon. It exhibits a series of advantages including low density, high aspect ratio, outstanding physical and chemical stability, wide availability and remarkable electrical conductivity, leading it to be extensively applied in EMA materials [20-22]. The common preparation methods for carbon fibers are complex, expensive and not environmental-friendly, which is not suitable for large-scale production [23, 24]. Therefore, it is in urgent need to develop an economical, simple and green route to prepare carbon fiber absorber.

Recently, biomass-derived carbon has become a promising candidate due to their low-cost, abundant, environmental-friendly and renewable properties, which are in line with the characteristics required for new generation EMA materials [25, 26]. In addition, biomass itself has the unique morphology, which can be maintained after carbonization [27-29]. Therefore, it is widely used in various application fields, such as batteries [30, 31], supercapacitors [32, 33], catalysts [34, 35], adsorbents [36], and electromagnetic interference shielding [37]. To date, there have been some applications in the field of EMA based on the fiber morphology of natural plant. For instance, Li et al. used cotton as carbon source to fabricate the Co/C fibers which shows moderate microwave absorption performance [38]. Zhao et al. employed cotton as carbonaceous precursors

to achieve superior microwave absorption property, the lowest reflection loss is -60.0dB and the bandwidth is 4.4GHz [39]. Singh and his partners introduced a method for preparing heteroatom-doped carbon from chicken feather fiber, in which the optimized microwave absorption property with RL_{min} of -44.6dB was achieved [40]. Nevertheless, the filling ratio of these composites in the paraffin is between 25%~50%, which is not low enough. It is known that the lightweight of EMA has obvious advantages in the military field. Herein, the development of low filling ratio materials is currently one of the most important goals in the related fields. In nature, many plants, such as sisal and cotton, are rich in more than 60% cellulose. *Typha orientalis*, a perennial aquatic or marsh wetland plant, which can be found in lakes, ponds, ditches, swamps and rivers, and it can absorb large amounts of nutrients to produce large quantities of biomass [41-43]. It's worth noting that the fluffs of *Typha orientalis* are fibrous and light.

However, pure carbon fiber is more likely to reflect EM wave rather than absorb them because crystal structures dominate electronic structures in carbon materials. So a reasonable design of structure is crucial to improve this impedance matching situation [44]. Among these strategies, metal-free has assumed an increasing proportion for the last few years. As a significant polarization semiconductor with a wide band gap, Zinc oxide (ZnO) can be synthesized as special structure, such as nanoparticles, nanorods, nanowires, nanosheets and so on. It has been widely used in regulating EMA performance and get innumerable great achievements [22, 45, 46]. For example, Luo and partners synthesized ZnO nanostructures with different morphologies on the surface of carbon fiber and investigated the difference of EMA performance between

them [22]. Wang et al. prepared highly uniform polar ZnO arrays on carbon cloth substrate, proved that the CC@ZnO had promising potential in EMA field [45]. Wang and partners constructed the hierarchical $\text{Ti}_3\text{C}_2\text{T}_x$ MXene/Ni chain/ZnO array hybrid nanostructures on cotton fabric and improved the EMA performance [47]. Li investigated the EMA performance of CNT tightly and uniformly embedded with ultra-fine ZnO nanocrystals [48]. Yang et al. reported a nanosheet-like ZnO/Zn/carbon fiber composite with strong absorption and wide-frequency EMA properties [49].

Herein, we synthesized ZnO nanorods on the surface of the biomass-derived carbon fibers (BDCFs@ZnO) via a simple carbonization process at different temperatures and subsequent hydrothermal process, using *Typha orientalis* as the raw material. The EMA performance and absorption mechanism of BDCFs@ZnO are investigated. By adjusting the carbonization temperatures, BDCFs7 has an appropriate permittivity and excellent EMA performance with the filling ratio of only 5wt%. Moreover, the ZnO nanorods were grown on the BDCFs7 sample so that the EMA performance could be further improved. When the filling ratio is only 15wt%, the minimum RL value of BDCFs7@ZnO can reach -62.35dB at 14.12GHz with a thickness of 2.29 mm and the corresponding EAB can reach 6.8GHz. Therefore, this work offers an inspiration to the development of dielectric loss-type EMA materials with lightweight and strong EMA performance by a sustainable, low-cost and easily available approach, and provides a guideline to fabricate biomass-derived carbon fiber matrix composites.

2. Materials and method

2.1 Materials

Typha orientalis was obtained from the field. Zinc nitrate hexahydrate ($\text{Zn}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$), hexamethylenetetramine (HMTA), ammonia ($\text{NH}_3 \cdot \text{H}_2\text{O}$, 25%-28%), ethanol and deionized water were purchased from Shanghai Titan Technology Co., Ltd. The chemicals were of analytical grade and used without further purification.

2.2 Preparation of BDCFs

BDCFs were prepared by a simple carbonization process. First, *Typha orientalis* fluff were cut, washed with distilled water and alcohol for three times, respectively. Obtained fluff were dried at 60 °C for one day. Then, the obtained dry fluffs were put into the ceramic crucible and heated at 700 °C for 2h in the tube furnace under the atmosphere of argon with a heating rate of 5 °C/min, then cooled to the room temperature naturally in the tube furnace. The resulting samples were washed with distilled water until the filtrate was neutral. Finally, the samples were dried at 60 °C in vacuum until the water evaporated. The obtained sample was marked as BDCFs7. To compare the effects of BDCFs at different carbonization temperatures, the samples were also heated at 600 °C, 800 °C and denoted as BDCFs6, BDCFs8, respectively.

2.3 Preparation of BDCFs@ZnO

ZnO nanorods were decorated on the surface of BDCFs through a hydrothermal reaction to obtain BDCFs@ZnO. In detail, 0.38 g of $\text{Zn}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$ and 0.182 g of HMTA together with 2mL of ammonia were dissolved in 40 mL distilled water under the constant magnetic stirring for 10 min. Then, 10mg BDCFs were added to the reaction solution and continue stirring for another 10 min. Later, the obtained reaction

solution was transferred into a 50 mL Teflon-lined stainless-steel autoclave and maintained at 105 °C for 20 h. After cooling to the room temperature, the obtained gray fibers were washed three times with DI water and ethanol by means of filtration, respectively, and finally dry at 60 °C overnight. The composites were labeled as BDCFs6@ZnO, BDCFs7@ZnO and BDCFs8@ZnO respectively. For comparison, pure ZnO without BDCFs were prepared by the same process.

2.4 Characterization

The phase composition and chemical state of samples were characterized by X-ray diffractometer with Cu-K α as the irradiation source ($\lambda=1.54$ Å) from 10° to 90° (a step scan of 0.02° and 1 s per step). Raman spectra was obtained by a cryogenic matrix isolated Raman spectroscopic system using laser excitation at 532 nm to analyze the composition and state of carbon. Thermogravimetric analysis (TGA) of sample in air was used to determine the carbon content. X-ray photoelectron spectras (XPS) were performed on X-ray photoelectron spectrometer (Thermo Kalpha) to analyze element composition and state. The micromorphology of BDCFs and BDCFs@ZnO was observed by scanning electron microscope (SEM) and transmission electron microscope (TEM). The EM parameters were measured by the vector network analyzer (Ceyear 3672B-S) based on the coaxial cable method to attain the EMA performance. The frequency range of test is from 2 GHz to 18 GHz. The test samples were prepared by the following steps: First, mixing sample and the paraffin in a suit ratio, then the mixtures were pressed in a mould to form a ring, the outer diameter is 7.00 mm and the inner diameter is 3.04 mm.

3. Results and discussion

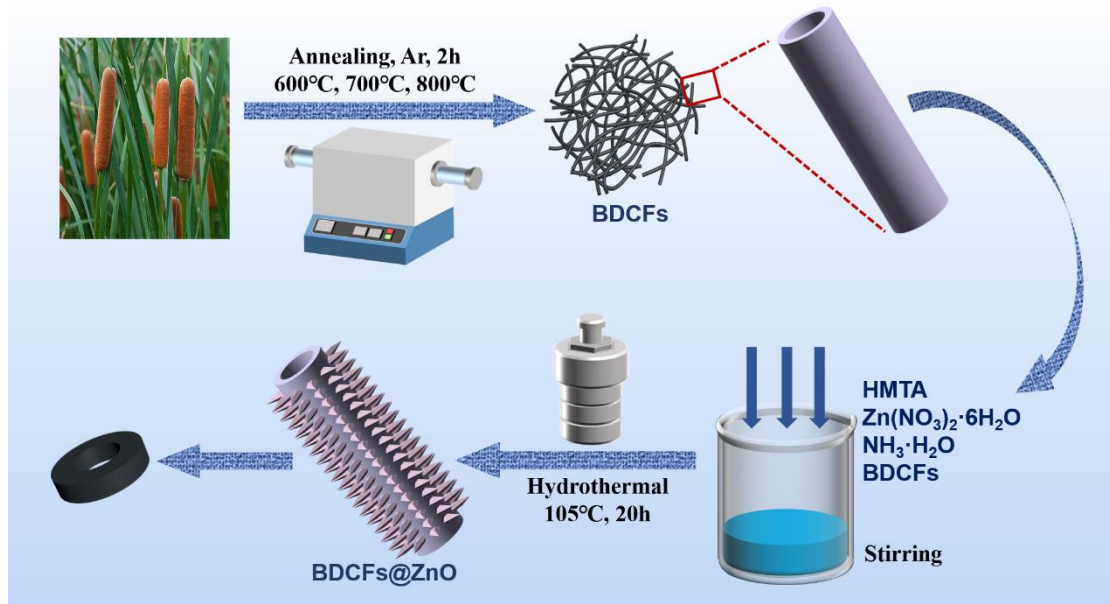
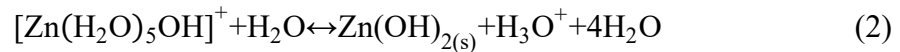
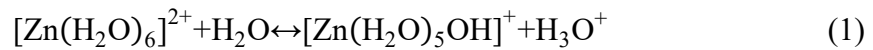


Fig. 1 Schematic of the formation of BDCFs@ZnO

The fabrication process of mace-like carbon fibers/ZnO composites (BDCFs@ZnO) is schematically illustrated in Fig. 1. Firstly, the cleaned *Typha orientalis* fluffs were carbonized at high temperature in argon atmosphere to produce BDCFs. Secondly, BDCFs were immersed in precursor solution to grow ZnO by a hydrothermal process, then the products were washed to attain BDCFs@ZnO composites. The synthesis process of ZnO is illustrated as follows [50]:



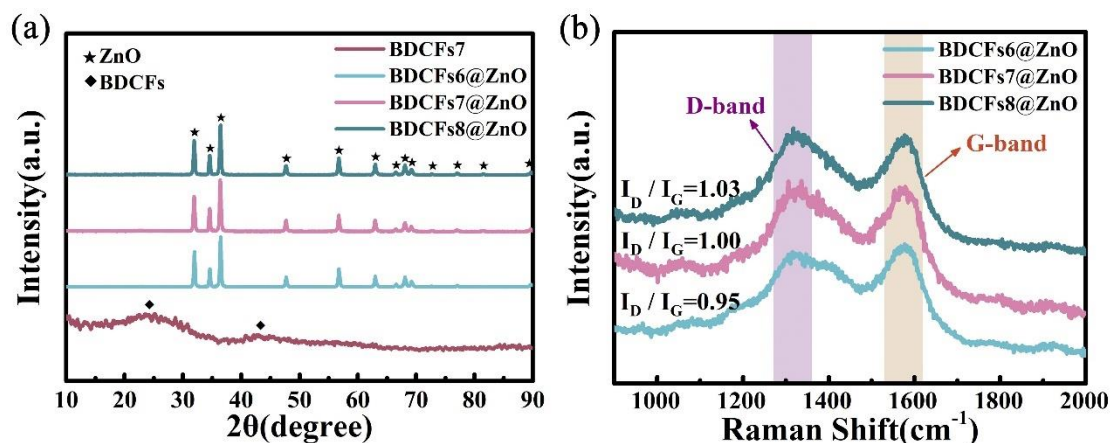


Fig. 2 XRD pattern (a) and Raman spectra (b) of different samples

Fig. 2a shows the XRD pattern of all the samples. Two broad diffraction peaks at 24° and 43° in BDCFs7 represent the formation of disordered graphite carbon in carbonization process. There are distinct diffraction peaks at 31.7°, 34.3°, 36.1°, 47.4°, 56.3°, 62.6°, 66.0°, 67.6°, 68.7°, 72.4°, 76.6°, 81.1° and 89.2° in BDCFs6@ZnO, BDCFs7@ZnO and BDCFs8@ZnO, which are corresponding to the (100), (002), (101), (102), (110), (103), (200), (112), (201), (004), (202), (104) and (203) planes of ZnO, respectively (JCPDS No. 79-0208), indicating the successful synthesis of ZnO nanorods on the BDCFs during the hydrothermal process. Correspondingly, there is almost no difference in the peak intensity of ZnO in different samples. The broad diffraction peaks of carbon are unobvious owing to the strong diffraction peaks of ZnO crystal. The grain size of ZnO was calculated to be about 29.9 nm based on the Scherrer equation.

The Raman spectra of BDCFs@ZnO obtained at various carbonization temperatures are shown in Fig. 2b. All the samples show two peaks at around 1350 cm⁻¹ and 1590 cm⁻¹, corresponding to the D band and G band, respectively. The D band is a breathing mode of A_{1g} symmetry involving phonons near the K zone boundary. It

becomes active in the disordered state or in the presence of nanocrystalline graphite. The G band involves the in-plane bond-stretching motion of pairs of carbon sp^2 atoms in graphite [51, 52]. Generally speaking, the graphitization degree is usually expressed by the ratio of the intensity of D band to G band (I_D/I_G), and a higher ratio represents a lower graphitization degree and more defects [6]. The I_D/I_G value of BDCFs6@ZnO, BDCFs7@ZnO and BDCFs8@ZnO is 0.95, 1.00 and 1.03, respectively. According to the three-stage model proposed by Ferrari and Robertson, this is because the carbon materials is in the stage of transformation of amorphous carbon to nanocrystalline graphite [51, 52]. The mean distance between defects (L_D) can be calculated by using the formula (4) and the defect density (n_D) can be approximatively estimated by the empirical equation (5) [53]:

$$L_D^2(\text{nm}^2) = (1.8 \pm 0.5) \times 10^{-9} \times \lambda_L^4 (I_D/I_G)^{-1} \quad (4)$$

$$n_D(\text{nm}^{-2}) = (1.8 \pm 0.5) \times 10^{22} \times \lambda_L^{-4} \times (I_D/I_G) \quad (5)$$

where λ_L is the excitation laser wavelength. The values of L_D are calculated to be 12.32 nm, 12.01 nm and 11.83 nm for sample BDCFs6@ZnO, BDCFs7@ZnO and BDCFs8@ZnO, respectively. The values of n_D are $2.01 \times 10^{11} \text{ cm}^{-2}$, $2.25 \times 10^{11} \text{ cm}^{-2}$ and $2.31 \times 10^{11} \text{ cm}^{-2}$ for them. All three samples have a large number of defects, and the defect density increases slightly with the increase of carbonization temperature.

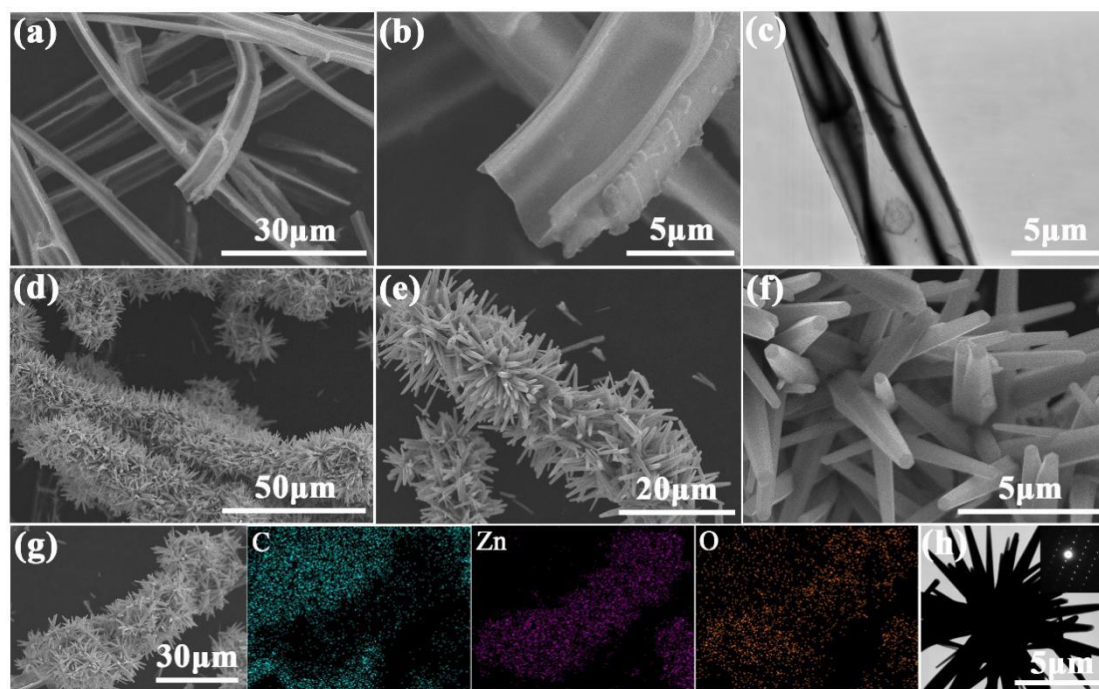


Fig. 3 SEM images (a-b) and TEM image (c) of BDCFs7. SEM images of BDCFs7@ZnO (d-f), SEM-EDX mapping images of BDCFs7@ZnO (g) and TEM of ZnO (h).

The microstructure of samples is obtained by SEM and TEM. Fig. 3a-c are SEM images and TEM image of the BDCFs7. The SEM images of BDCFs6 and BDCFs8 are shown in Fig. S1. It was observed that the carbonization temperature almost had no influence on the morphology of BDCFs. The carbon fibers are uniformly and continuously distributed, with the diameter of about 6-7 μm and the average length of several hundred of micrometers. There are two ways of parallel and staggered arrangement between carbon fibers. Besides, the morphology of individual carbon fiber is also very unique comparing with traditional cotton carbon fiber. Every carbon fiber is twisted to a certain instead of completely flat and straight. There are some bamboo-like nodes existing on the BDCFs, making the surface to be roughness. From the Fig. 3b-c, we can clearly observe the hollow structure of BDCFs, which allows the EM

waves to reflect internally and increases the specific surface area of the material. Fig. 3d-f clearly showed the morphology of BDCFs7@ZnO and ZnO. ZnO are present in the form of nanorods which are pyramidal crystals, and each rod is randomly distributed and appears like flowers, covering the surface of the BDCFs7 uniformly. The hexagonal ZnO rods are about 500 nm in diameter and 5 μ m in length. Fig. 3g is the SEM-EDX mapping of BDCFs@ZnO for determining the element composition and distribution. It clearly shows the presence of carbon, oxygen, and zinc elements. The weaker intensity of carbon is due to the covering of ZnO layer on the surface of carbon fibers. And the distribution of carbon and oxygen outside the sample comes from the conductive adhesive. As shown in the Fig. S1c-d, the carbon fibers' morphology of BDCFs6 and BDCFs8 are similar to BDCFs7. The BDCFs6@ZnO and BDCFs8@ZnO are also covered with ZnO with the same morphology like BDCFs7@ZnO. Fig. 3h is the TEM image with the selected area electron diffraction (SAED) pattern of ZnO, which further exhibits the crystal structure of ZnO nanorods.

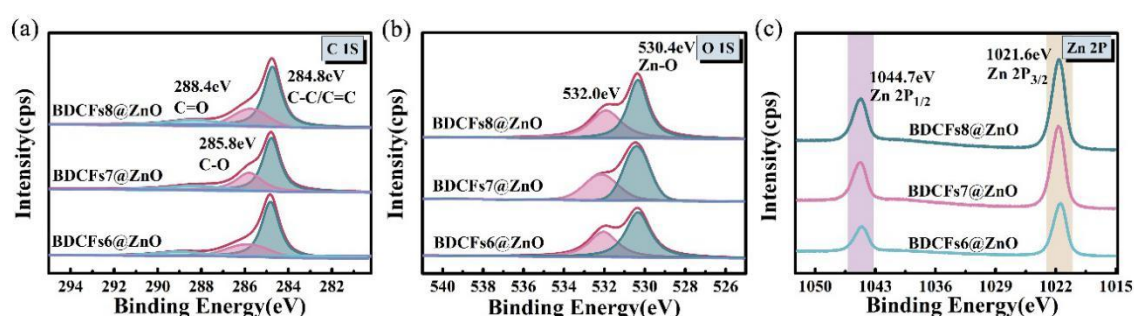


Fig. 4 XPS spectra of elements of different samples: C 1S (a), O 1S (b), Zn 2P (c), respectively.

The chemical composition and state of BDCFs@ZnO were detected by XPS. As shown in Fig. S2a, BDCFs7@ZnO was composited of three elements (C, Zn and O),

proving the successful preparation of ZnO on BDCFs7. Fig. 4 is the XPS spectra of three elements of BDCFs6@ZnO, BDCFs7@ZnO and BDCFs8@ZnO. In Fig. 4a, the C 1S energy spectrum is decomposed into three peaks. The peak at 248.8eV is belonging to the C-C or C=C, while the two peaks at 285.8eV and 288.4eV represent the C-O and C=O, respectively. In the O 1S spectrum (Fig. 4b), two obvious peaks detected at 532.0 and 530.4 eV can be attributed to the oxygen vacancies and ZnO bonds. Fig. 4c exhibits the spectrum of Zn 2P, and the peaks at 1044.7 and 1021.6 eV corresponds to the Zn 2P_{3/2} and Zn 2P_{1/2}, respectively. Fig. S2b is the thermogravimetric (TG) curve of BDCFs7@ZnO in the air. A minor weight loss occurred below 200°C is due to the evaporation of the physical absorbed water, and a major weight loss occurred between 200°C and 600°C is attributed to the pyrolysis of carbon in high temperature air.

On the basis of the transmission line theory, the EMA properties of the samples are corresponded to the relative complex permittivity ($\epsilon_r = \epsilon' - j\epsilon''$) and the relative complex permeability ($\mu_r = \mu' - j\mu''$). Among them, the real part of permittivity(ϵ') and the real part of permeability(μ') represent the storage capability of the electrical and magnetic energy, the imaginary parts(ϵ'' and μ'') are relevant to the loss capability of the electrical and magnetic energy [54].

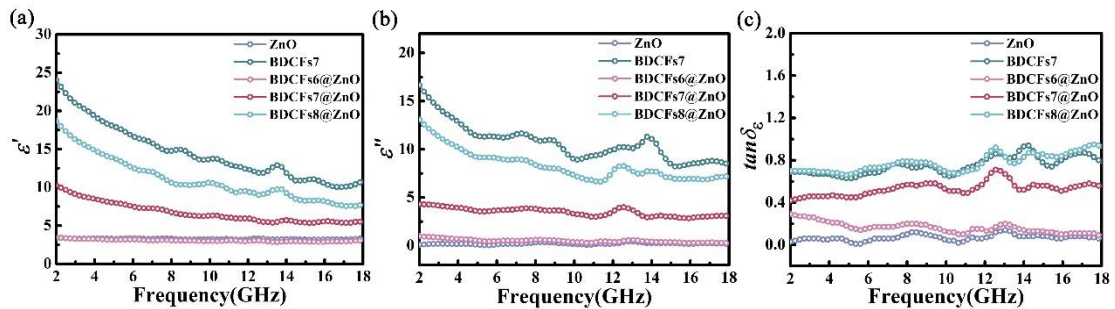


Fig. 5 Electromagnetic parameters of different samples at a filling ratio of 15wt%: real part of permittivity (a), imaginary part of permittivity (b) and dielectric loss tangent (c).

The variation of EM parameters with frequency is plotted in Fig. 5. The ϵ' of BDCFs7, BDCFs7@ZnO and BDCFs8@ZnO exhibits a distinct downward tendency, which is called frequency dispersion characteristic [28, 55]. From the Fig. 5a, we can observe that the BDCFs7 shows the highest ϵ' , ranging from 24.1 to 10.9, while the ϵ' of pure ZnO is very low and around 3. BDCFs6@ZnO also has a low ϵ' . As the frequency increases, it declines from 3.5 to 3.1. When the carbonization temperature rose to 700 °C, the ϵ' of BDCFs7@ZnO varies from 10.3 to 5.6. With the carbonization temperature continued to increase, the ϵ' of BDCFs8@ZnO falls from 18.7 to 7.7. As for the ϵ'' (Fig. 5b), the whole variant trend is identical. The values of BDCFs7, BDCFs6@ZnO, BDCFs7@ZnO and BDCFs8@ZnO varies from 16.7 to 8.4, 1.0 to 0.3, 4.3 to 3.0 and 13.1 to 7.1, respectively. The ϵ'' of ZnO fluctuates around 0.3. With the enhancement of carbonization temperature, the complex permittivity will increase. Therefore, the complex permittivity can be effectively tuned by adjusting the carbonization temperature. The complex permeability (μ_r) of the samples is shown in Fig. S3a-b. It is obvious that the μ' and μ'' maintain a really low level, which is own to the absence of magnetic components in the samples. The μ'' of the samples are negative in some frequency regions. This is mainly due to the fact that the sample will generate induced eddy currents under the action of electromagnetic waves, and the alternating electric field will cause the induced magnetic field and radiate the magnetic energy based on the Maxwell equation [56, 57]. Besides, the higher the conductivity, the more

significant the negative imaginary permeability [58, 59]. To further study the dissipation ability, Fig. 5c and Fig. S3c show the relationships between the loss tangent and the frequency. The dielectric loss tangent ($\tan\delta\epsilon = \epsilon''/\epsilon'$) and the magnetic loss tangent ($\tan\delta\mu = \mu''/\mu'$) represent the ability of attenuating electric and magnetic energy, respectively. The magnetic loss tangent of all the samples is at a very low level, indicating a poor magnetic loss ability because of the absence of magnetic components. The low dielectric loss tangent values of ZnO and BDCFs6@ZnO suggest the weak dielectric loss ability. The dielectric loss tangent values of BDCFs7, BDCFs7@ZnO and BDCFs8@ZnO are higher than the other samples, revealing the contribution of carbonization temperature on dielectric loss ability. Thus, it is concluded that the dielectric loss plays a dominant role in the EMA performance.

According to the Debye theory, the ϵ'' can be considered as the contribution of polarization relaxation(ϵ_p'') and conduction loss(ϵ_c''), described as the following equation [11, 60]:

$$\epsilon'' = \epsilon_p'' + \epsilon_c'' = \frac{\epsilon_s - \epsilon_\infty}{1 + \omega^2 \tau^2} \omega \tau + \frac{\sigma}{\omega \epsilon_0} \quad (6)$$

where σ is the electrical conductivity, ω is the angular frequency, τ is the relaxation time, ϵ_0 is the dielectric constant in vacuum, ϵ_s is the static permittivity and ϵ_∞ represent the relative permittivity at the high frequency limit. The first term represents the polarization relaxation, the second term is correlated with conduction loss. It can be seen from the equation that the high conductivity contributes to the increase of ϵ'' . Thus, conduction loss plays a major role at low frequencies and polarization relaxation plays a major role at high frequencies. Furthermore, the resonance peaks in ϵ'' plot are mostly

attributed to the polarization relaxation loss [61]. In general, the polarization loss can be divided into four categories, including ion polarization, electron polarization, dipole polarization and interface polarization. Among them, ion and electron polarization occur at 10^3 - 10^6 GHz. Therefore, dipole polarization and interface polarization play the dominant role in polarization relaxation processes [61].

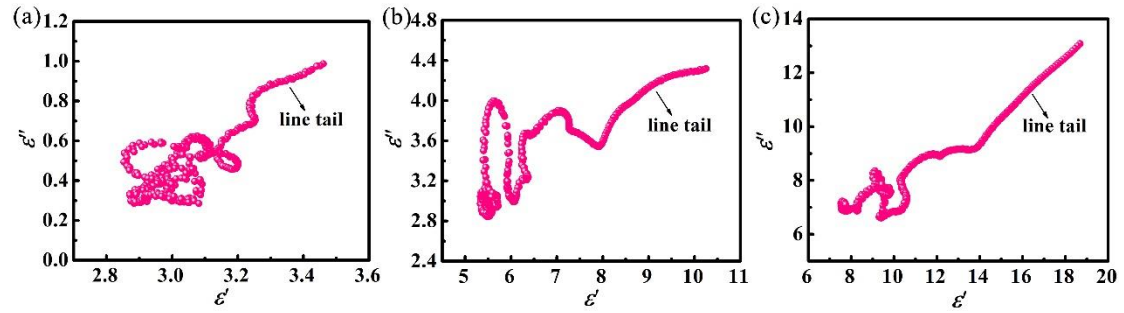


Fig. 6 Cole-Cole plots of BDCFs6@ZnO (a), BDCFs7@ZnO (b) and BDCFs8@ZnO (c) at a filling ratio of 15wt%.

According to the Debye theory, the relationship between ϵ' and ϵ'' can be described as following:

$$\left(\epsilon' - \frac{\epsilon_s + \epsilon_\infty}{2}\right)^2 + (\epsilon'')^2 = \left(\frac{\epsilon_s - \epsilon_\infty}{2}\right)^2 \quad (7)$$

The curve of ϵ' versus ϵ'' should be a semicircle, which is called the Cole-Cole plot. Each semicircle corresponds to one Debye polarization relaxation process, and the EM attenuation is closely related to the number of Cole-Cole semicircle [62]. Fig. 6 and Fig. S4 show the Cole-Cole plots of each sample. It can be noted that the ZnO sample has no semicircle with obvious contour and data plots are crowded together. The BDCFs7 and BDCFs6@ZnO samples only have a few clear semicircles in the limited range, suggesting the few polarization relaxation processes. The Cole-Cole curves of BDCFs7@ZnO and BDCFs8@ZnO both display multiple semicircles with distinct

outlines belonging to many polarization relaxations processes. Raman spectra shows that BDCFs are disordered and they have a lot of carbon defects that can trap free electrons. The charge around the defect continuously accumulates and is distributed asymmetrically, resulting in a defective dipole and polarization relaxation. In addition, the addition of ZnO will bring the interfacial polarization. There are many interfaces between BDCFs and ZnO. Due to the different conductivity and dielectric characteristics between the BDCFs and the ZnO, the extra charge will gather at the interface under the external electric field, then the interfacial polarization will occur [63]. In previous work, Yan et al. has used COMSOL software to simulate and verify that the interface polarization of the hierarchical structure of composite materials contributed a great deal to the enhancement of the EMA performance [64]. There are line tails in BDCFs7, BDCFs6@ZnO, BDCFs7@ZnO and BDCFs8@ZnO, suggesting the existence of conduction loss. And the length of line tail extended as the temperature increased, indicating that the conduction loss was gradually strengthened [3]. From the SEM images, we know that BDCFs with large aspect ratio can construct a three-dimensional (3D) interconnected network, which facilitates the electron hopping and migration. Under the alternating EM field, the 3D interconnected conductivity network could provide long channels to transport electron and generate a microcurrent, and ultimately convert EM energy into heat energy.

Based on the transmission line theory, the reflection loss (RL) value is used to represent the absorption performance, which is obtained by the following equation [65]:

$$RL(dB)=20 \log |(Z_{in}-Z_0)/(Z_{in}+Z_0)| \quad (8)$$

$$Z_{in}=Z_0(\mu_r/\epsilon_r)^{1/2} \tanh [j(2\pi fd/c)(\mu_r/\epsilon_r)^{1/2}] \quad (9)$$

where Z_0 is the air impedance, Z_{in} is the input impedance, f is frequency, d is the thickness of the samples, c is the velocity of light, ϵ_r and μ_r are the relative complex permittivity and permeability, respectively. The lower RL value and the wider EAB (the frequency range of $RL < -10\text{dB}$) indicate the better EMA performance. Generally, when RL value is lower than -10 dB , 90% of the EM can be attenuated [66].

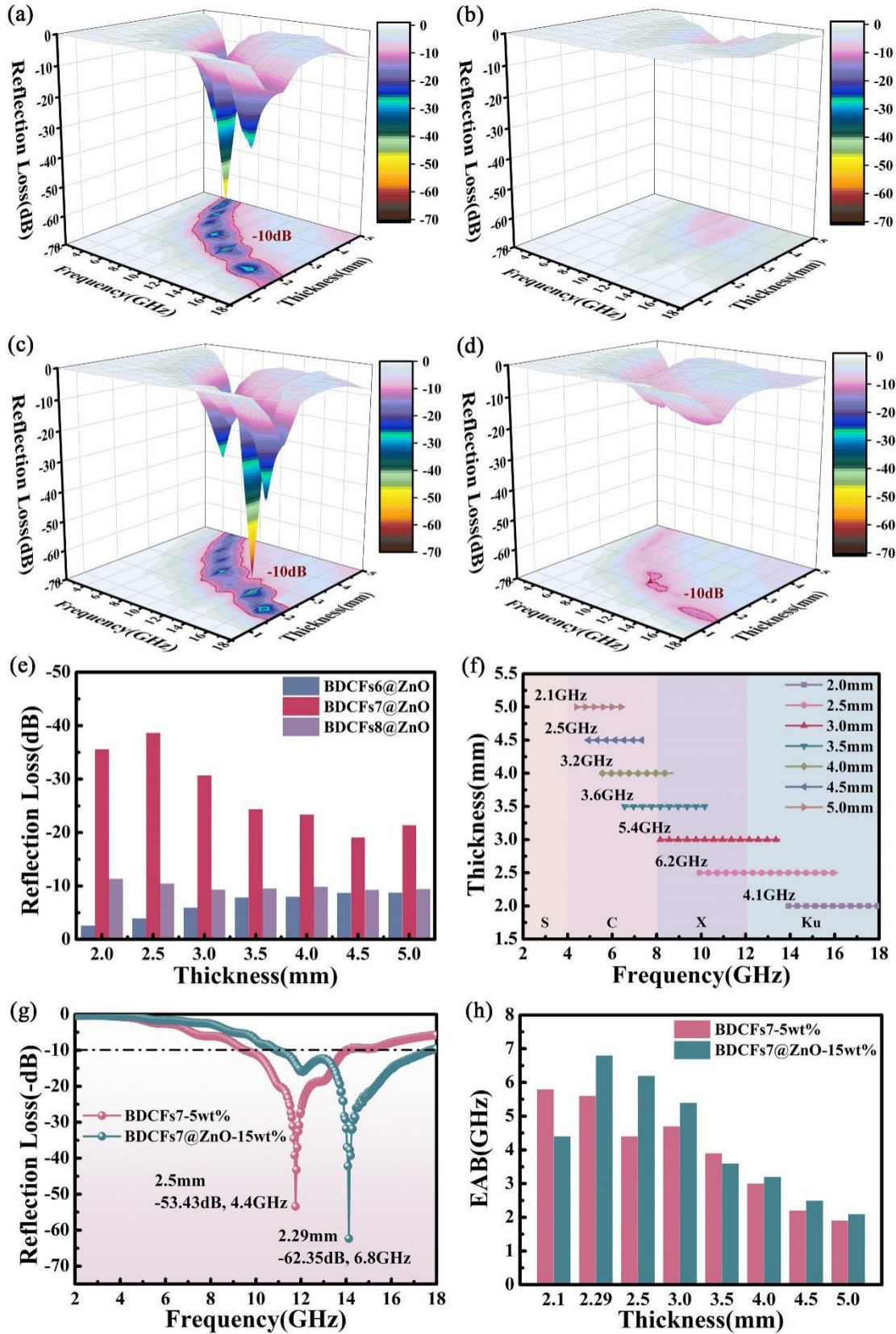


Fig. 7 3D RL plots of BDCFs7 at a filling ratio of 5wt%, BDCFs6@ZnO (b), BDCFs7@ZnO (c) and BDCFs8@ZnO (d) at a filling ratio of 15wt%. A comparison of

RL between different samples (e) and EAB of BDCFs7@ZnO at different thicknesses (f). A comparison of RL (h) and the EAB (i) between BDCFs7 and BDCFs7@ZnO.

Fig. 7 and Fig. S5 show the EMA performance of all the samples. The permittivity and EMA performance of BDCFs@ZnO could be successfully adjusted by changing the carbonization temperature. A remarkable EMA performance of pure BDCFs7 is obtained when the filling ratio is only 5wt% (Fig. 7a). It's RL is -53.43dB at 11.76GHz with a thickness of 2.5mm while the EAB can reach 5.8GHz at 2.1mm. While after introducing the ZnO, the EMA performance of BDCFs7@ZnO is significantly improved, including a stronger absorption, a broader bandwidth and a thinner thickness (Fig. 7g-h). The RL values of BDCFs6@ZnO, BDCFs7@ZnO and BDCFs8@ZnO are shown in Fig. 7b-d. At a filling ratio of 15wt%, BDCFs7@ZnO possesses an optimal EMA performance. The lowest RL is -62.35dB at 14.12GHz with a thickness of 2.29mm, and the EAB is 6.8GHz. For BDCFs7@ZnO, the full-band EMA almost covers the C (4-8.2 GHz), X (8.2-12.4 GHz), and Ku (12.4-18 GHz) bands by adjusting the thickness. Furthermore, it displays an effective absorption band at X band at the thickness of 3.0 mm. In a word, by adjusting the carbonization temperatures and introducing the ZnO nanorods, we can successfully tune the EMA performance of the materials.

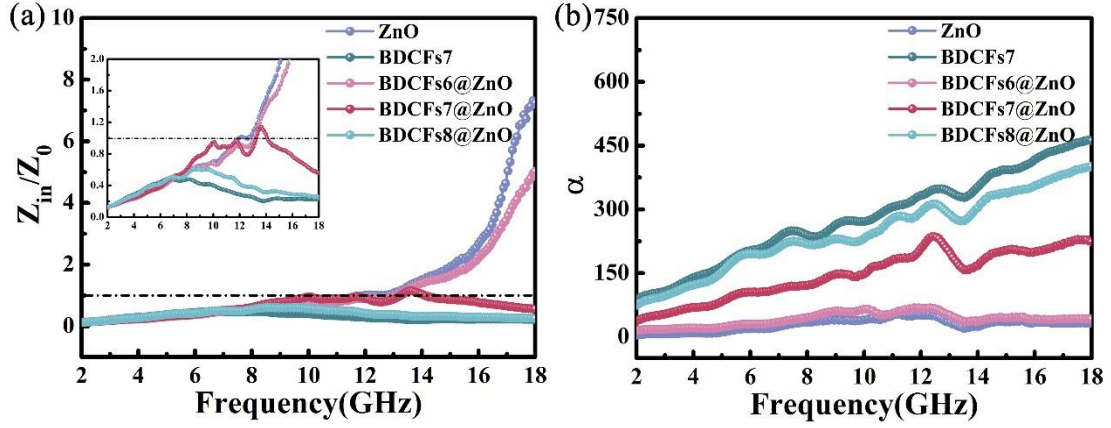


Fig. 8 The impedance matching (Z_{in}/Z_0) of BDCFs7@ZnO in the thickness of 2.29 mm (a) and attenuation constant (α) of all samples (b) at a filling ratio of 15wt%.

An excellent absorber must satisfy two principles: the incident EMW is able to enter the absorber to the maximum extent possible, and then be entirely attenuated in the absorber [67]. Good impedance matching means that the reflectivity of EMW on the surface of the material is minimized through special boundary conditions, which reduces the reflection of electromagnetic waves on the surface of the absorbing material and allows as much electromagnetic waves as possible to enter the inside of the absorbing material. The value of Z_{in}/Z_0 is used to evaluate the impedance matching characteristics. The value of Z_{in}/Z_0 closing to 1 represents a matched characteristic impedance [68]. Here we calculated the value of Z_{in}/Z_0 at a constant thickness of different samples. From the Fig. S6e, BDCFs7 shows a good impedance matching from 8GHz to 14GHz with a filling ratio of 5wt%. When the filling ratio increases to 15wt%, the mismatch of impedance in BDCFs7 was apparent since the values are far away from 1, as shown in Fig. 8a. The mismatch of impedance is due to the high complex permittivity, which will result in a strong reflection of EM wave and could hardly enter the absorber. It can be observed from Fig. 8 that the impedance matching characteristics

of BDCFs7@ZnO shows a great improvement in the range of about 10-15GHz where the values of Z_{in}/Z_0 are closer to 1. The ratio of the BDCFs6@ZnO and BDCFs8@ZnO samples are only close to 1 in a small range, which indicates poor impedance matching characteristics. Another crucial factor, the attenuation constant, can be expressed by the following formula [69]:

$$\alpha = \frac{\sqrt{2}\pi f}{c} \sqrt{(\mu_r''\epsilon_r'' - \mu_r'\epsilon_r') + \sqrt{(\mu_r''\epsilon_r'' - \mu_r'\epsilon_r')^2 + (\mu_r'\epsilon_r'' + \mu_r''\epsilon_r')^2}} \quad (10)$$

The constant represents the ability of the absorbing material to dissipate the EM energy that enters it. Fig. 8b depicts the attenuation constants of different samples with a filling ratio of 15wt% as a function of frequency, it follows the same trend as the dielectric loss tangent (Fig. 5c). As can be clearly observed, the attenuation constant of pure ZnO is very low and the attenuation ability is very poor. The attenuation constant of BDCFs7 is the highest, indicating the strongest attenuation ability which mainly due to the conduction loss. As the carbonization temperature increases, the BDCFs7@ZnO and BDCFs8@ZnO possess much larger α value than that of BDCFs6@ZnO, implying them outstanding attenuation capacity for the incident EM waves. However, the impedance mismatch of BDCFs7 and BDCFs8@ZnO limits its absorbing performance. Based on the above discussion, it can be concluded that the BDCFs7@ZnO sample possesses the optimal electromagnetic wave absorption performance, this is consistent with the obtained RL diagram.

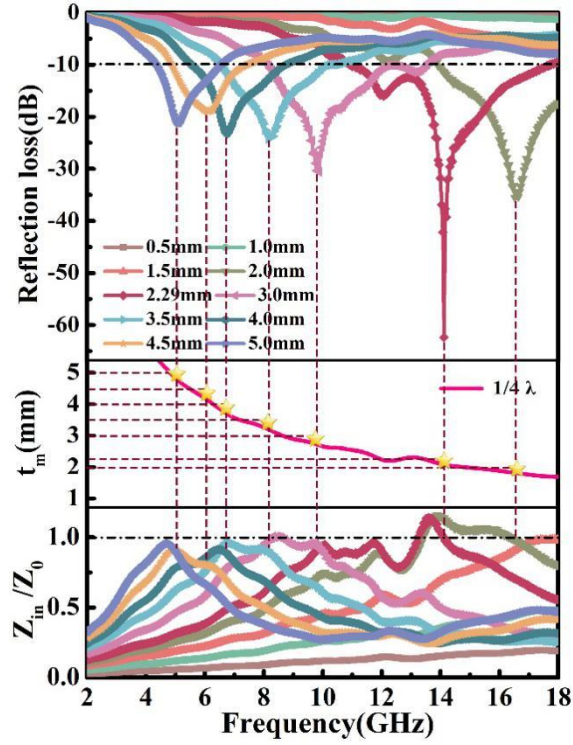


Fig. 9 Frequency dependence of reflection loss, matching thickness, and impedance matching (Z_{in}/Z_0) of BDCFs7@ZnO at a filling ratio of 15%.

As is demonstrated in Fig. 9, it reveals the relationships of the RL peak, thickness and impedance matching as a function of frequency, respectively. Remarkably, the RL peak gradually shifts to a lower frequency as the absorber's thickness increases from 2mm to 5mm. This phenomenon can be described by the quarter-wavelength cancellation model [70]:

$$t_m = \frac{nc}{4f_m \sqrt{|\epsilon_r \mu_r|}} \quad (n=1,3,5,\dots) \quad (11)$$

where t_m stands for the thickness, f_m stands for the frequency corresponding to RL peak. If the relationship between thickness and the frequency matches the above equation, incident and reflected waves are out of phase by 180° , resulting in the extinction of each other at the air-absorber interfaces. The yellow stars which stand for experimental consequence are located at around the $1/4\lambda$ curve, demonstrating that the relationship

between t_m and f_m for the EMA of BDCFs7@ZnO obeys the quarter-wavelength cancellation model. In addition, the RL peak occurs near the Z_{in}/Z_0 value of 1, which is consistent with the impedance matching theory.

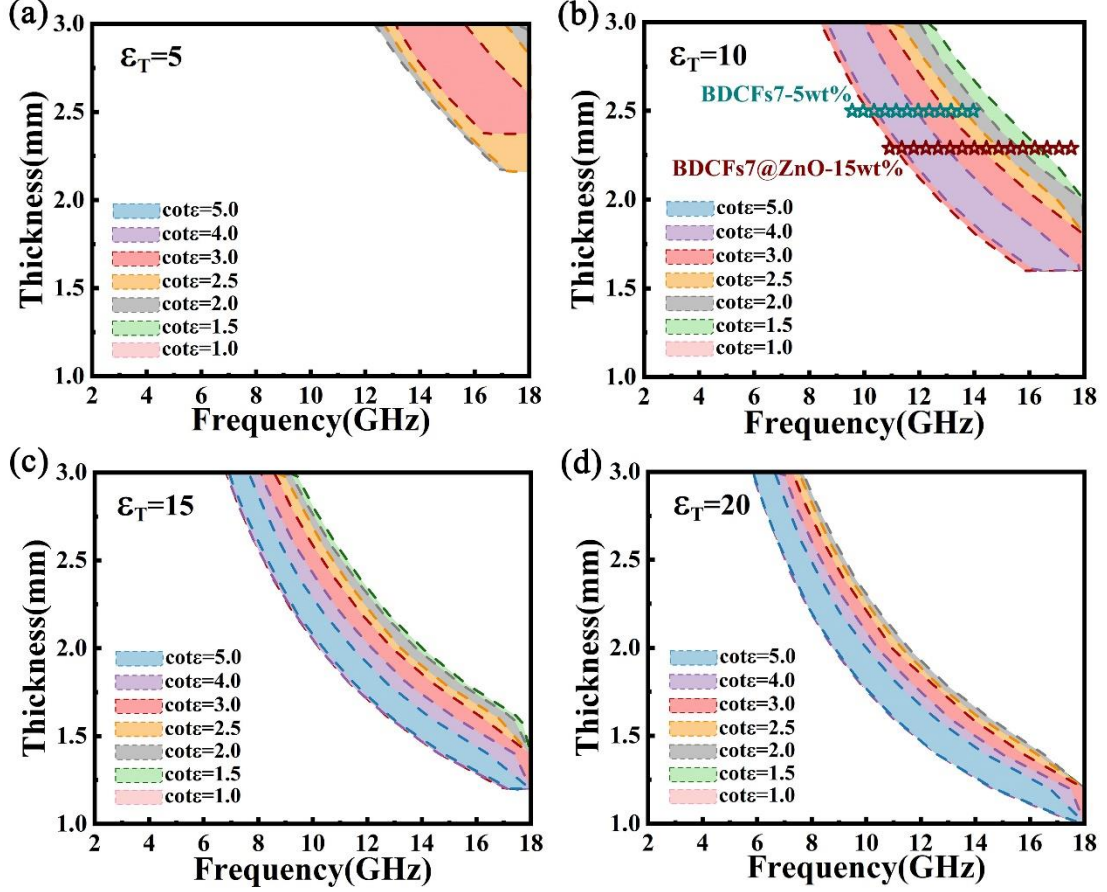


Fig. 10 Dielectric sum-quotient model with $\cot\epsilon$ from 1.0 to 5.0: (a) $\epsilon_T=5$, (b) $\epsilon_T=10$, (c) $\epsilon_T=15$ and (d) $\epsilon_T=20$.

In order to further analyze the wide EAB and low matching thickness of the samples, the dielectric sum-quotient model was applied from a computational point of view. In a non-magnetic material system, we suppose that the values of μ' and μ'' are 1 and 0, respectively. By adjusting the values of ϵ'' and ϵ' , it can be seen that the effective RL values ($RL < -10\text{dB}$) are influenced by the sum and quotient of them. In this model, ϵ_T is defined as the sum of the real and imaginary parts and $\cot\epsilon$ is the quotient of the

real and imaginary parts. Fig. 10a-d shows the relationship between ϵ_T , $\cot\epsilon$, thickness, frequency and effective RL values. The relevant data calculated according to the dielectric sum-quotient model are shown in Tab. S1-4. From the Fig. 10a-d, we can observe that the effective RL value moves towards low frequencies and starts to appear at thinner thickness with the increase of ϵ_T . But it is clear that the frequency range of the effective RL values is also gradually narrowing, meaning that the EAB is reduced. Combined with the permittivity of BDCFs7 and BDCFs7@ZnO, when the RL values are less than -10dB, the sum and quotient of their dielectric constant is close to 10 and 2, respectively. In Fig. 10b, the EAB of them are basically matched with the calculated results. Therefore, we can design the dielectric values of the non-magnetic absorbing material to obtain the desired bandwidth and thickness according to the calculation results obtained by this model.

Tab. 1 EMA performances of some reported biomass-derived carbon-based absorbers

Samples	RL (dB)	EAB (GHz)	t (mm)	Filling ratio (wt%)	R _F	E _F	Ref
BDCFs7	-53.43	5.8	2.5	5	10.7	1.2	This work
BDCF7@ZnO	-62.35	6.8	2.29	15	4.2	0.45	This work
PCFF	-44.6	2.2	1.68	30	1.5	0.07	[40]
Co/C fiber	-50.1	5.6	2	20	2.5	0.28	[38]
HPCs	-62.2	7.3	2.71	30	2.1	0.24	[71]
Ni(OH) ₂ /AC	-23.6	2	6	50	0.5	0.04	[72]
HPMC-1.0	-52	5	1.7	15	3.5	0.33	[73]
RHPC/Co	-40.1	2.7	1.8	25	1.6	0.11	[74]
CFs-650	-52.6	8.6	2.6	30	1.8	0.29	[75]
MPC600	-49.6	5	2	30	1.7	0.17	[76]
PC-600	-42.4	2.24	2	30	1.4	0.07	[24]

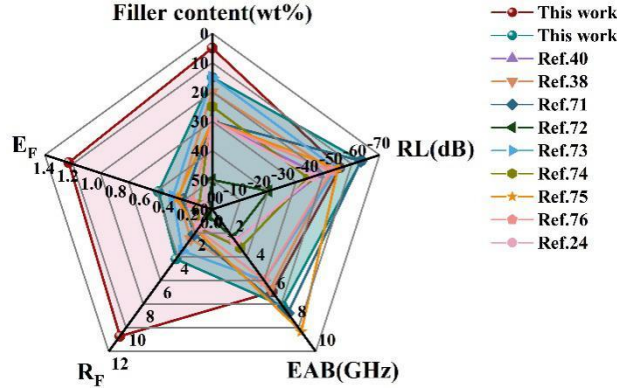


Fig. 11 The comparison of EMA performance between this work and other studies.

Tab. 1 listed the EMA performance of biomass-derived carbon-based absorbers reported in the literatures in recent years. Here, we define two parameters R_F and E_F as the evaluation index to evaluate absorption performance absorbing materials, respectively:

$$R_F = \frac{|RL|}{100F} \quad (12)$$

$$E_F = \frac{|EAB|}{100F} \quad (13)$$

where F represent the filling ratio. The comparison of EMA performance between this work and other biomass-derived carbon-based materials is visually demonstrated by radar map in Fig. 11. Compared with others, BDCFs7 presents the advantage of lightweight. At the low filling ratio of 5%, it exhibits an excellent EMA performance, including strong RL values, broad EAB and thin thickness. The values of R_F and E_F can reach 10.7 and 1.2, which are much higher than other materials. After compounding BDCFs7 with ZnO, the filling ratio of BDCFs@ZnO at 15wt% can obtain an outstanding EMA performance. RL reduced from -53.43dB to -62.35dB, EAB increased from 5.8GHz to 6.8GHz and the thickness decreased from 2.5mm to 2.29mm.

Although the filling ratio of BDCFs7@ZnO has increased, it still remains at a low level. The values of R_F and E_F of BDCFs7@ZnO are 4.2 and 0.45, which are still higher than that of absorbing materials in other works. Remarkably, the R_F and E_F values of BDCFs7@ZnO reach new records, suggesting the bright prospect for it as an ultralight, broadband and high-efficient EM wave absorber.

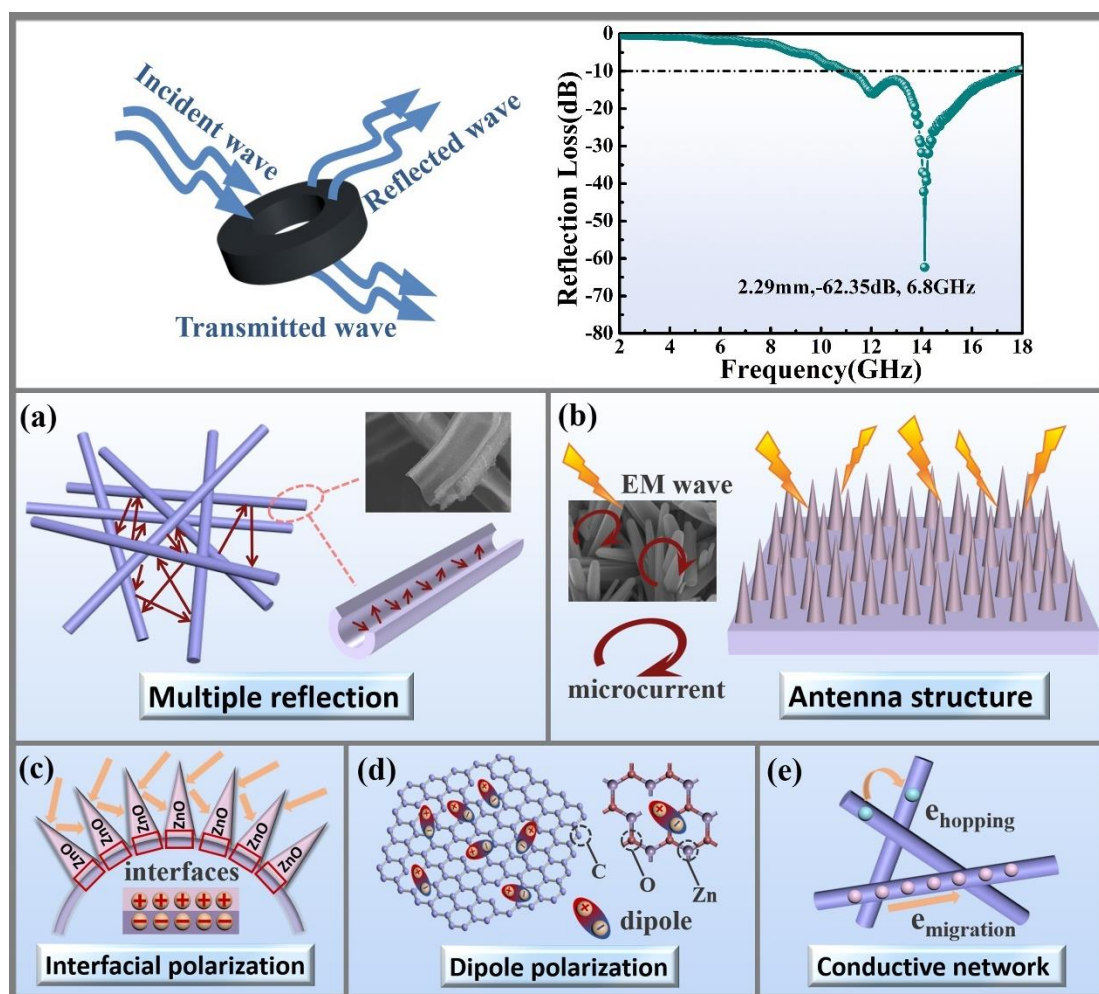


Fig. 12 The schematic illustration of the electromagnetic microwave absorption of the BDCFs samples: multiple reflection (a), antenna structure (b), interfacial polarization (c), dipole polarization (d) and conductive network (e).

In summary, the excellent EMA performance are explained by the following facts (Fig. 12). Firstly, the staggered hollow tube structure with low density is beneficial for

dissipate of EM energy. Multiple reflections of incident EM waves occur in the hollow tube and 3D connected network, greatly increasing the propagation routes and dissipation of the EM waves. Secondly, the permittivity and the dielectric loss ability of the BDCFs@ZnO samples is sensitive to the carbonization temperature. 3D interconnected conductive network with high aspect ratio increases the transmission path of electrons, so that more EM energy is converted to heat energy. By adjusting the carbonization temperature, BDCFs7@ZnO has a strong conduction loss. Next, in spite of conduction loss, dipole polarization and interfacial polarization also play a crucial role in determining the attenuation capacity. What's more, BDCFs7@ZnO possesses a good impedance matching by optimizing the fabricating process. The carbon defects of BDCFs7 and the oxygen vacancy of ZnO act as the dipole centers which lead to dipole polarization. At the interfaces between BDCFs7 and ZnO, many capacitor structures are formed due to the accumulation of positive and negative charges, which are beneficial to the interfacial polarization. Due to the thermal vibration of the molecules under an alternating EM field, the polarization movement and charges interact with electromagnetic waves and lead to the dielectric fluctuations, which is also confirmed in the peaks shown in Fig. 5b. Further, the BDCFs7@ZnO exhibit a clear Cole-Cole semicircle and line tail (Fig. 6), revealing the strong polarization relaxation, conduction loss and attenuation ability. Besides, there are many void spaces forming among the ZnO nanorods, it could generate multiple reflections and extend the EM wave propagation routes. Finally, the ZnO nanorods can be thought of a receiving antenna. When the incident EMW are propagated to the ZnO nanorods, they will be transformed

into the microcurrent and be attenuated [77-79].

4. Conclusion

In summary, mace-like carbon fibers/ZnO composites derived from *Typha orientalis* were successfully synthesized by a simple carbonization process and subsequent hydrothermal process. With a filling ratio of only 5wt%, pure BDCFs7 can achieved a RL of -53.43dB at 2.5mm and a EAB of 5.8GHz at 2.1mm. After compounding with ZnO, the BDCFs7@ZnO sample possessed better impedance matching characteristics and stronger attenuation capability, resulted in a remarkable EMA performance. The multiple reflection, conduction loss, dipole polarization and interfacial polarization in BDCFs7@ZnO cause the enhance of dielectric loss. When the filling ratio was 15wt%, it had the minimum RL value of -62.35dB at 14.12GHz with the thickness of 2.29mm and exhibited an EAB of 6.8GHz (from 10.9GHz to 17.7GHz). The strong conduction loss and multiple reflection are owing to the unique hollow structure of BDCFs and the construction of 3D interconnected conductive network. The abundant carbon defects and interfaces in BDCFs@ZnO composites bring the strong dipole polarization and interfacial polarization. In addition, a dielectric sum-quotient model was applied to further verify the experimental results and to inspire the design of electromagnetic wave absorbing materials. As a result, this work not only offers inspiration to the development of dielectric loss-type EMA materials with low filling ratio and strong EMA performance, but also provides a guideline to fabricate biomass-derived carbon fiber matrix composites in other fields.

Acknowledgments

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Figures

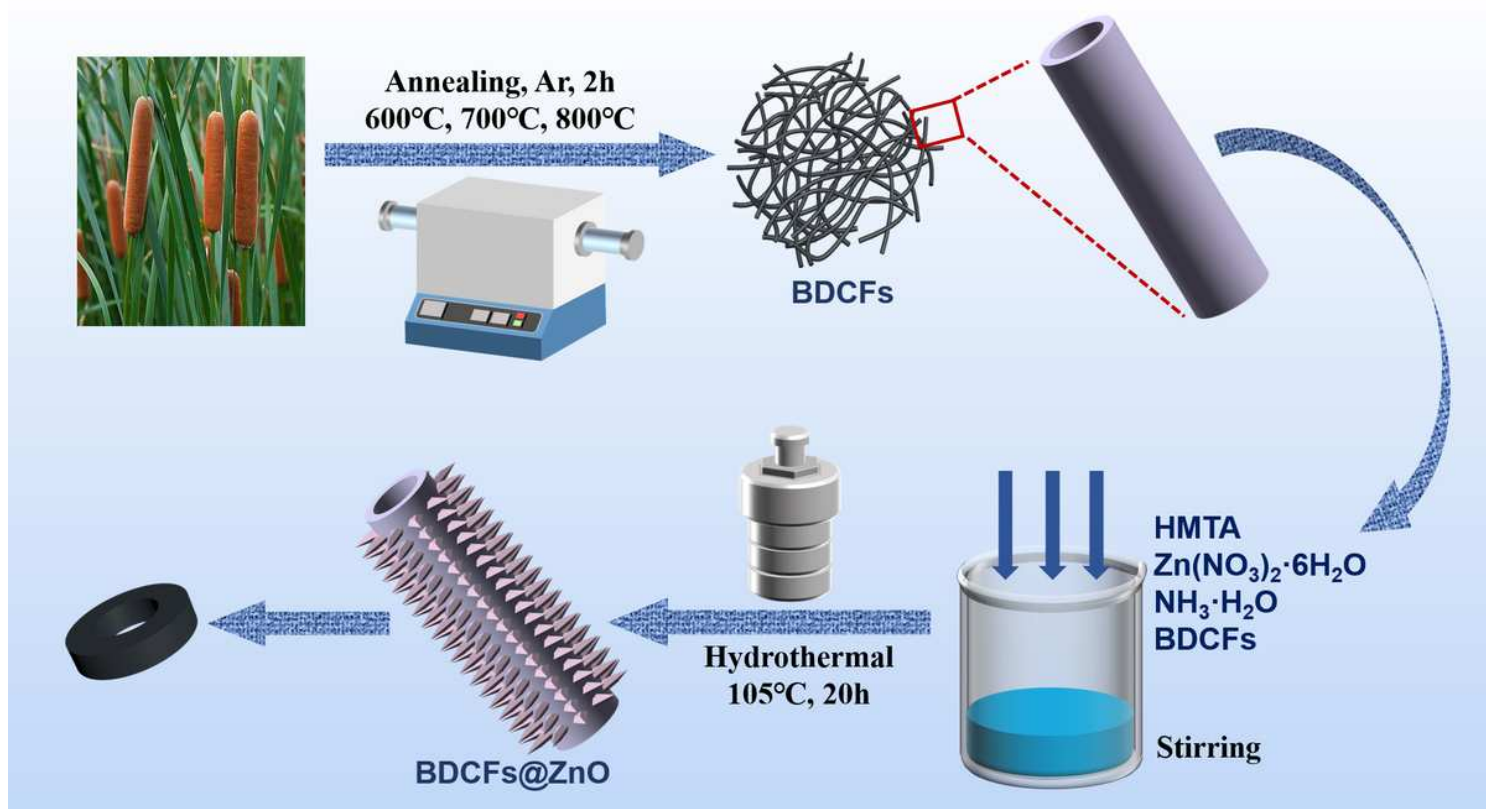


Figure 1

Schematic of the formation of BDCFs@ZnO

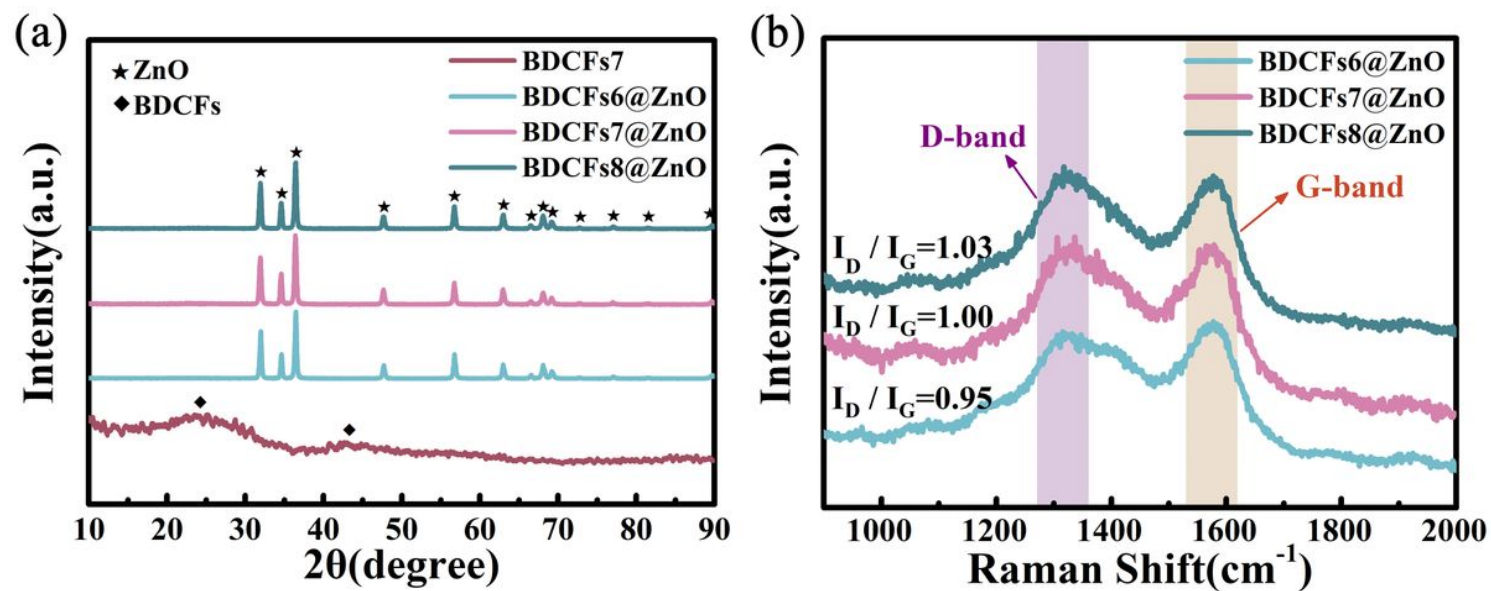


Figure 2

XRD pattern (a) and Raman spectra (b) of different samples

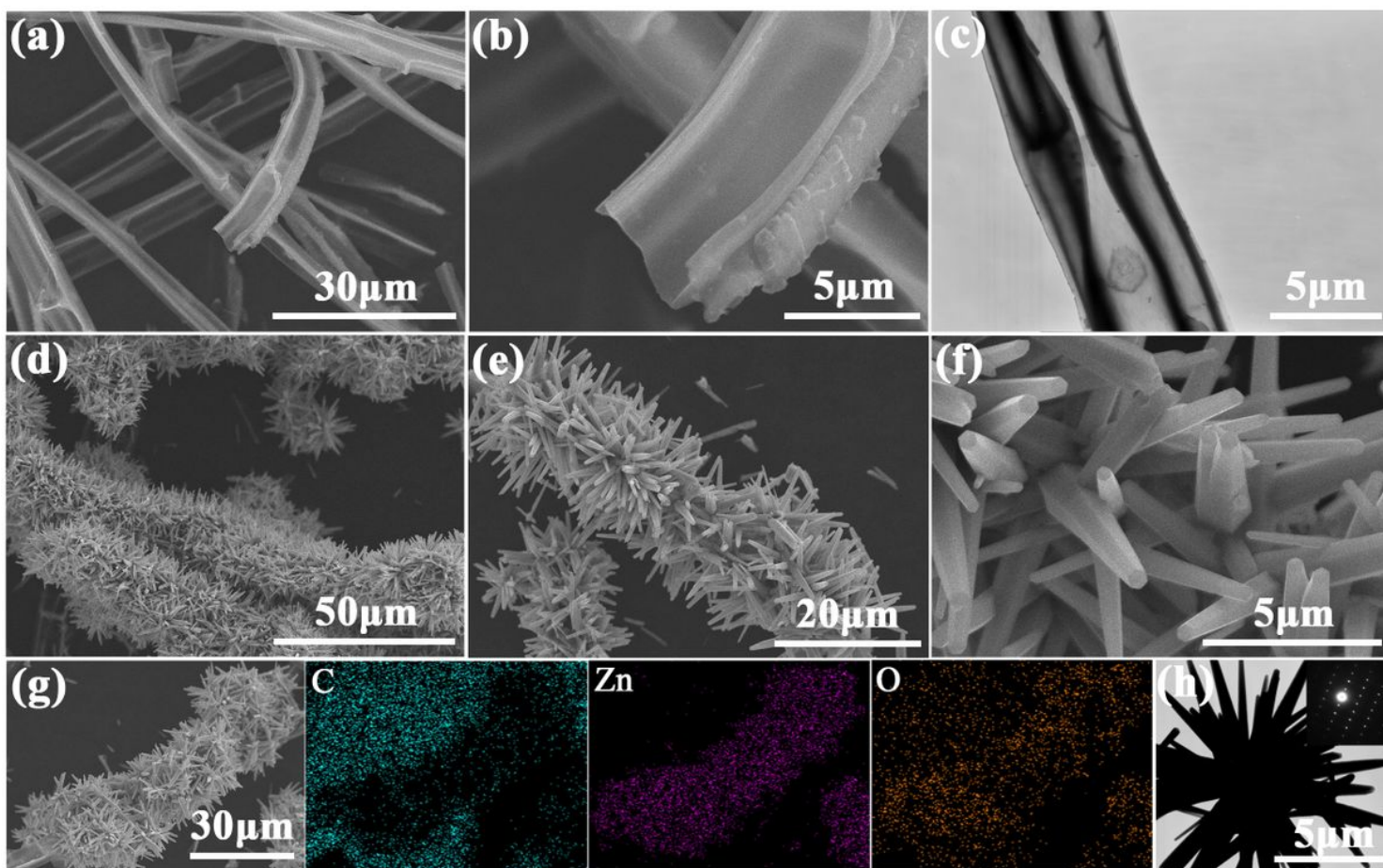


Figure 3

SEM images (a-b) and TEM image (c) of BDCFs7. SEM images of BDCFs7@ZnO (d-f), SEM-EDX mapping images of BDCFs7@ZnO (g) and TEM of ZnO (h).

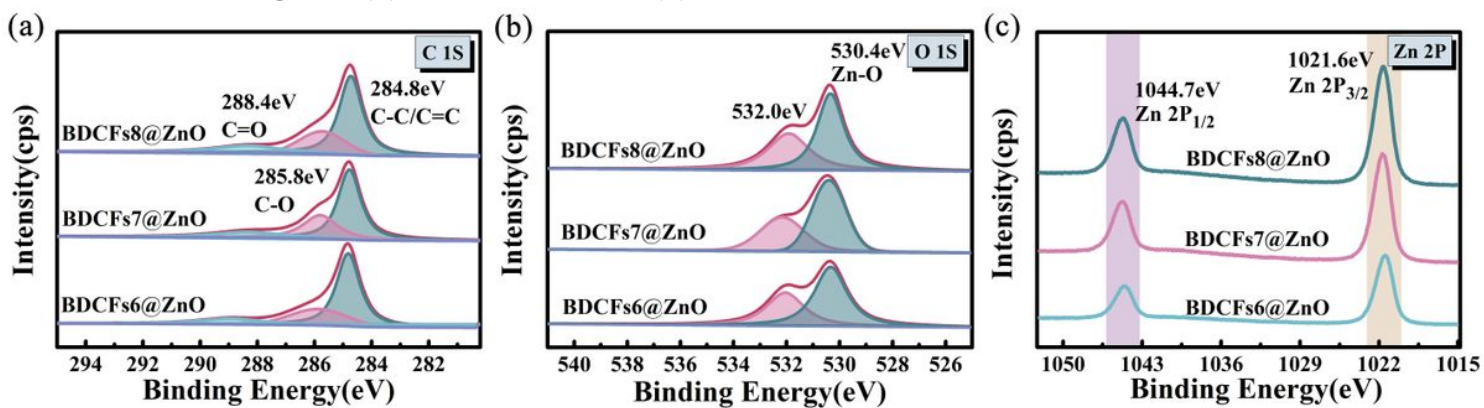


Figure 4

XPS spectra of elements of different samples: C 1S (a), O 1S (b), Zn 2P (c), respectively.

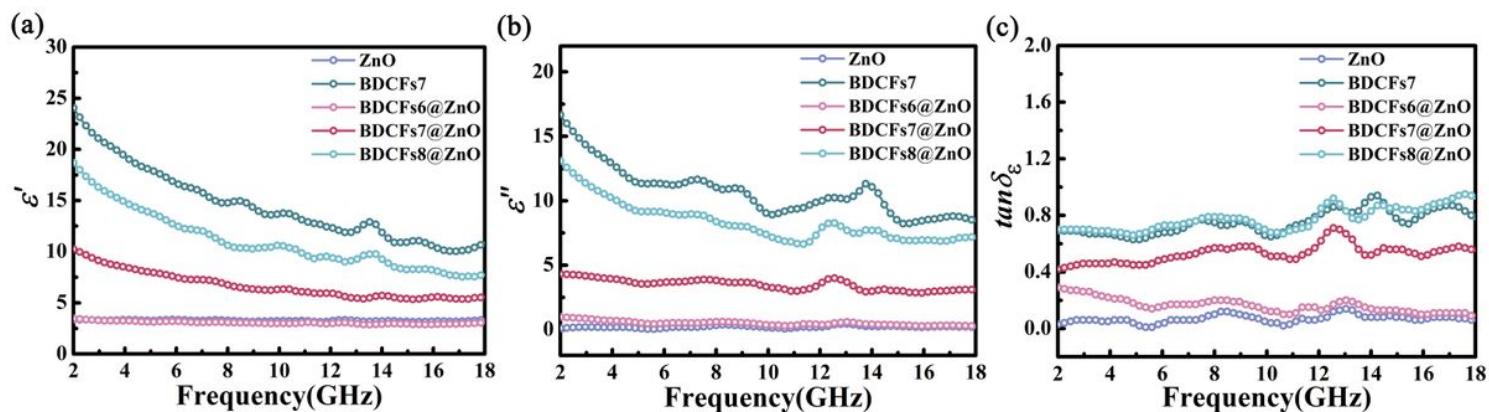


Figure 5

Electromagnetic parameters of different samples at a filling ratio of 15wt%: real part of permittivity (a), imaginary part of permittivity (b) and dielectric loss tangent (c).

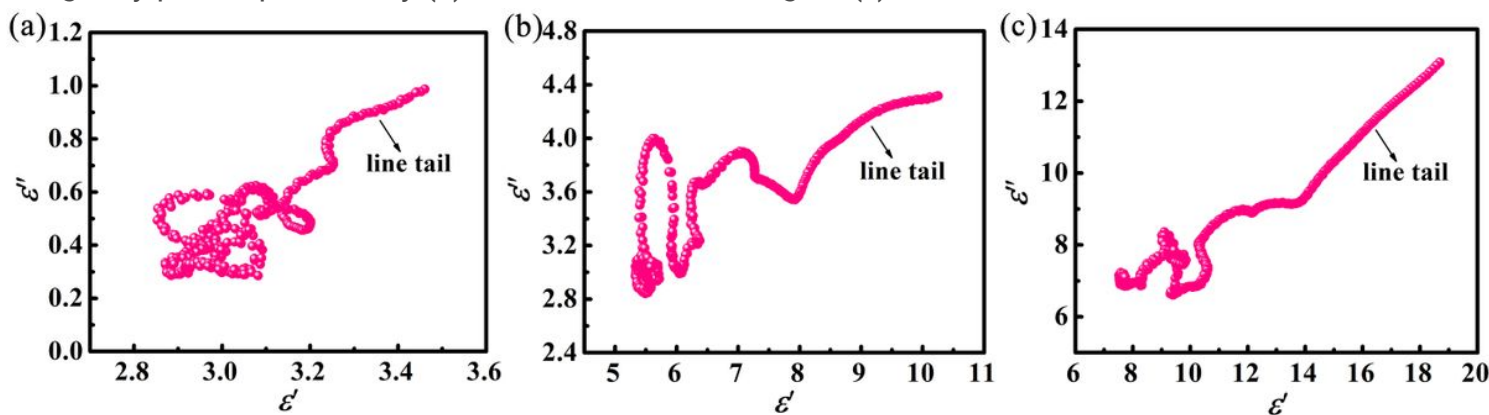


Figure 6

Cole-Cole plots of BDCFs6@ZnO (a), BDCFs7@ZnO (b) and BDCFs8@ZnO (c) at a filling ratio of 15wt%.

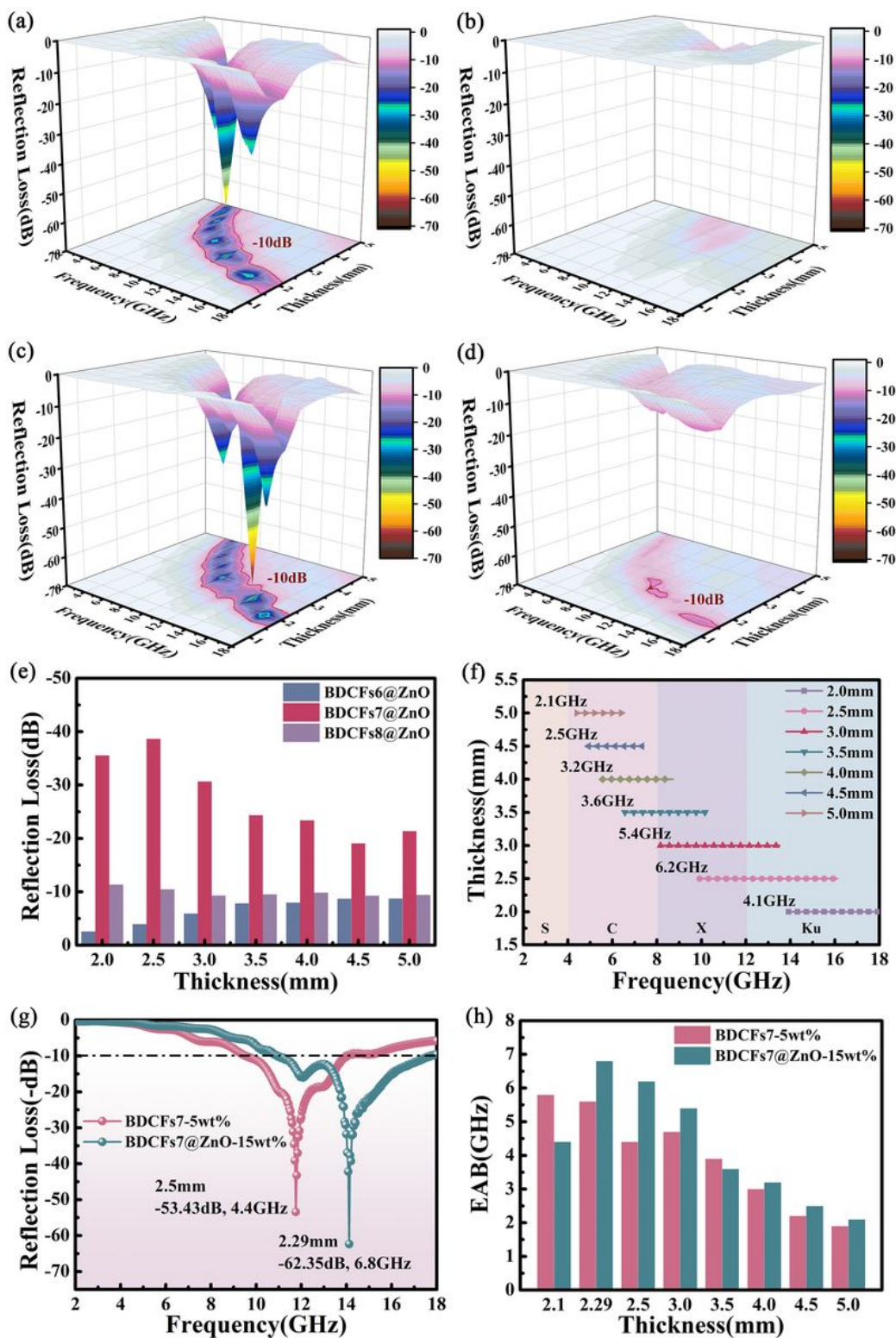


Figure 7

3D RL plots of BDCFs7 at a filling ratio of 5wt%, BDCFs6@ZnO (b), BDCFs7@ZnO (c) and BDCFs8@ZnO (d) at a filling ratio of 15wt%. A comparison of RL between different samples (e) and EAB of BDCFs7@ZnO at different thicknesses (f). A comparison of RL (h) and the EAB (i) between BDCFs7 and BDCFs7@ZnO.

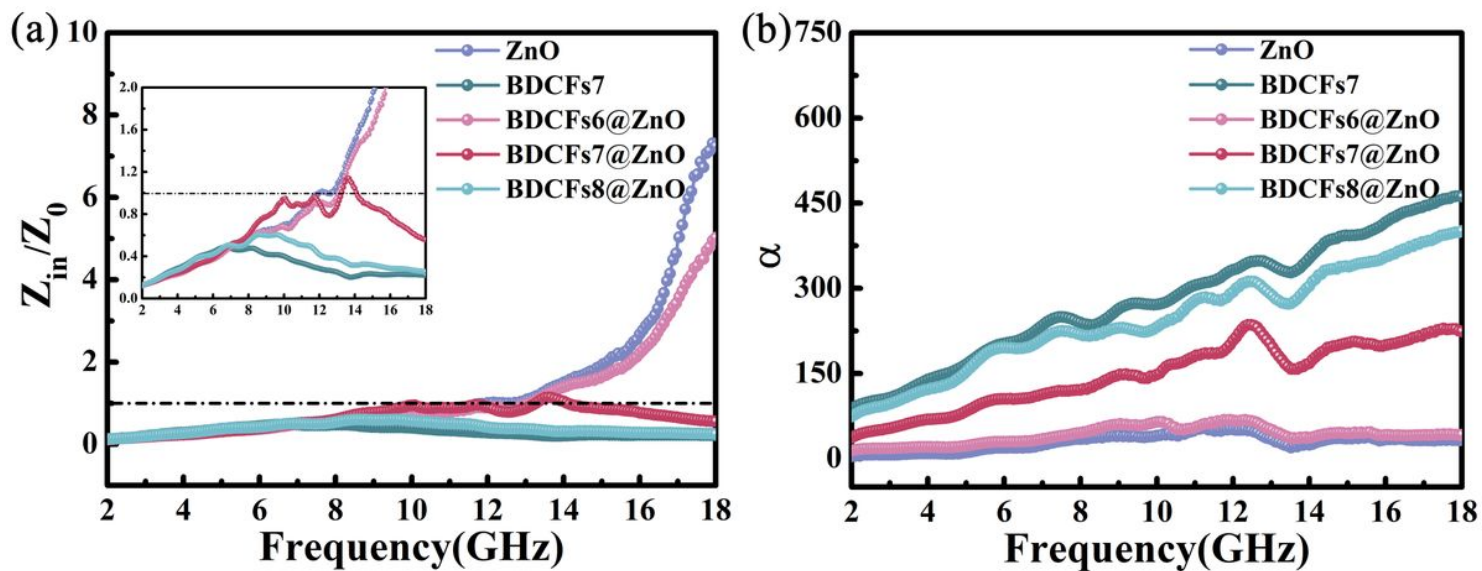


Figure 8

The impedance matching (Z_{in}/Z_0) of BDCFs7@ZnO in the thickness of 2.29 mm (a) and attenuation constant (α) of all samples (b) at a filling ratio of 15wt%.

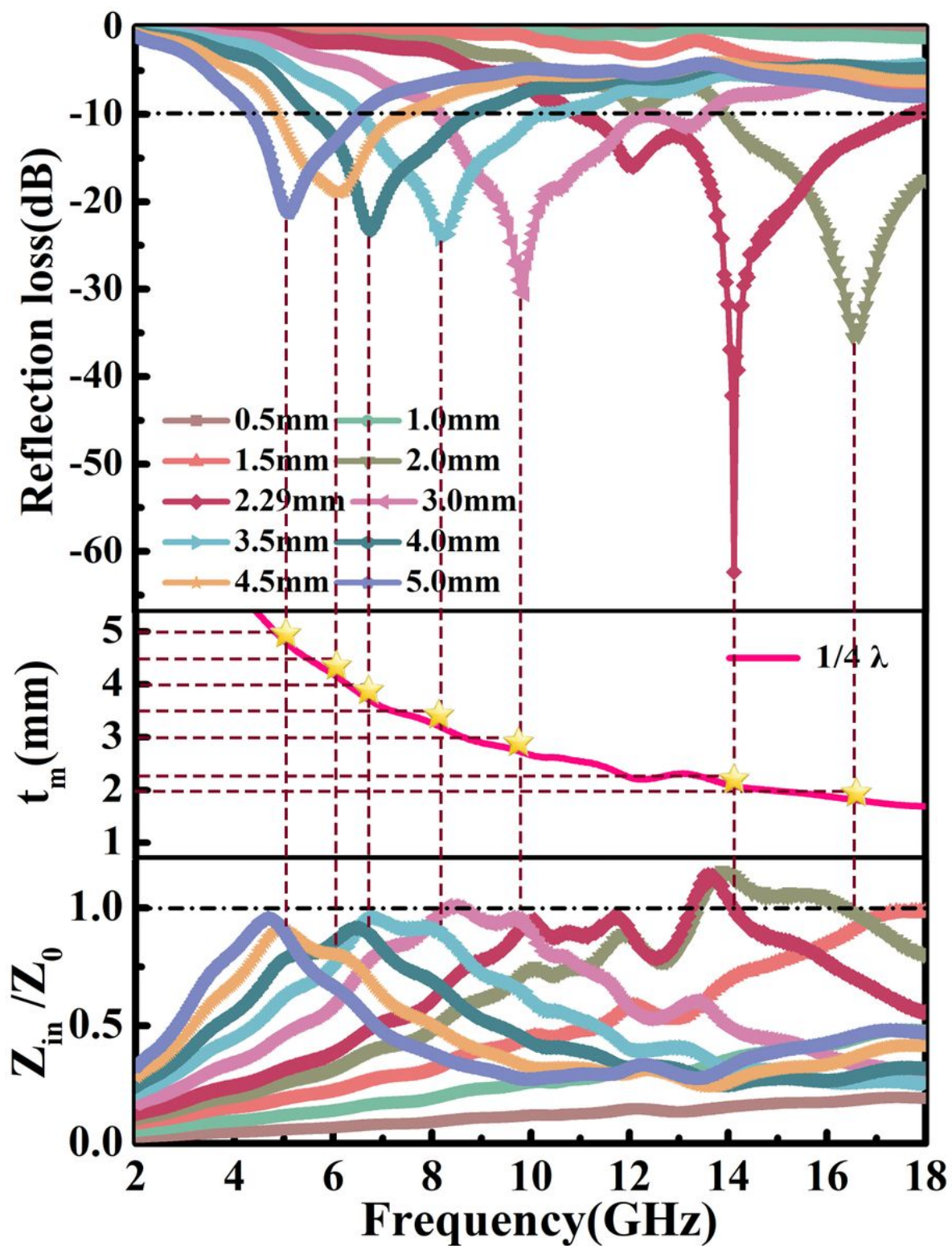


Figure 9

Frequency dependence of reflection loss, matching thickness, and impedance matching (Z_{in}/Z_0) of BDCFs7@ZnO at a filling ratio of 15%.

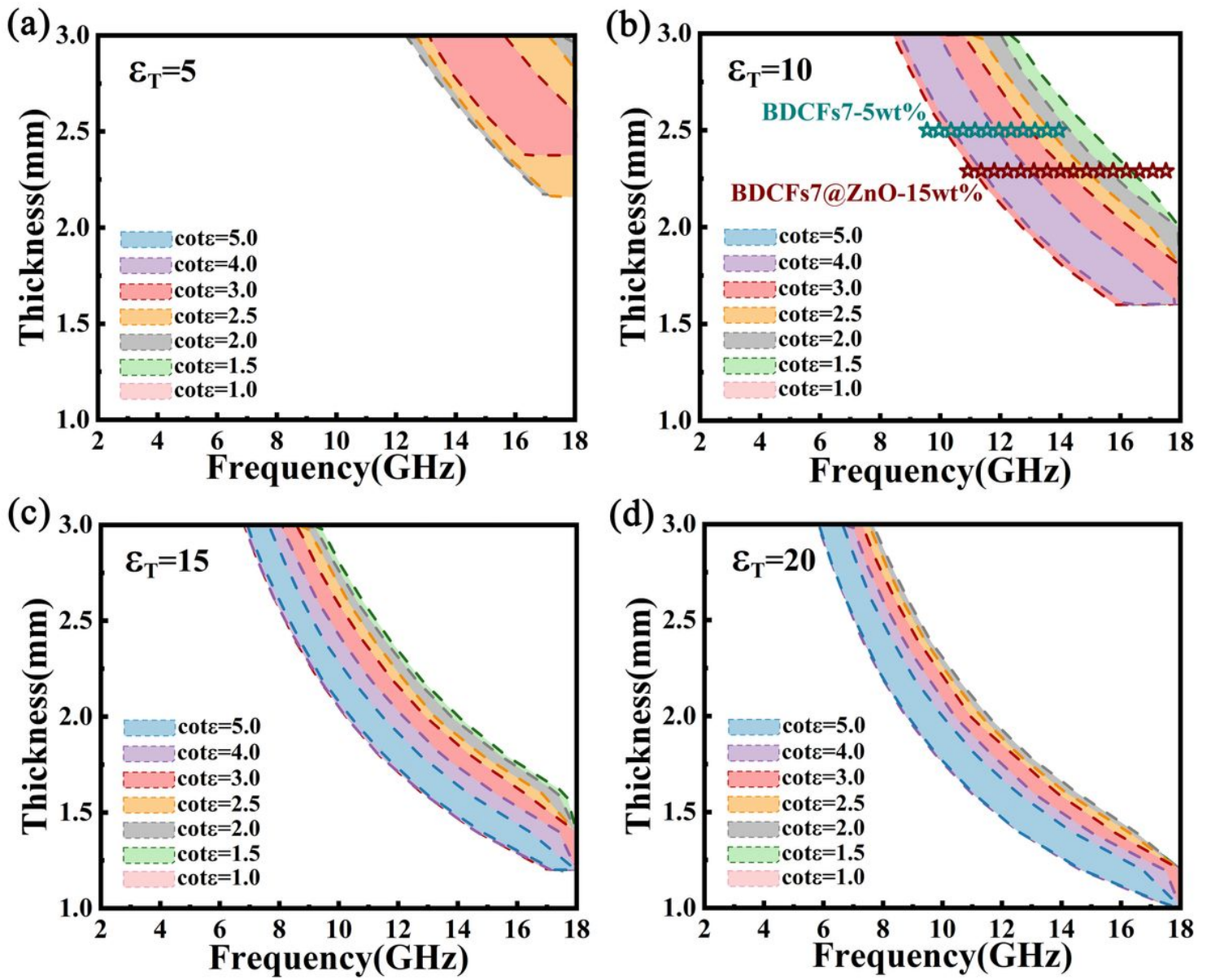


Figure 10

Dielectric sum-quotient model with $\cot\epsilon$ from 1.0 to 5.0: (a) $\epsilon_T=5$, (b) $\epsilon_T=10$, (c) $\epsilon_T=15$ and (d) $\epsilon_T=20$.

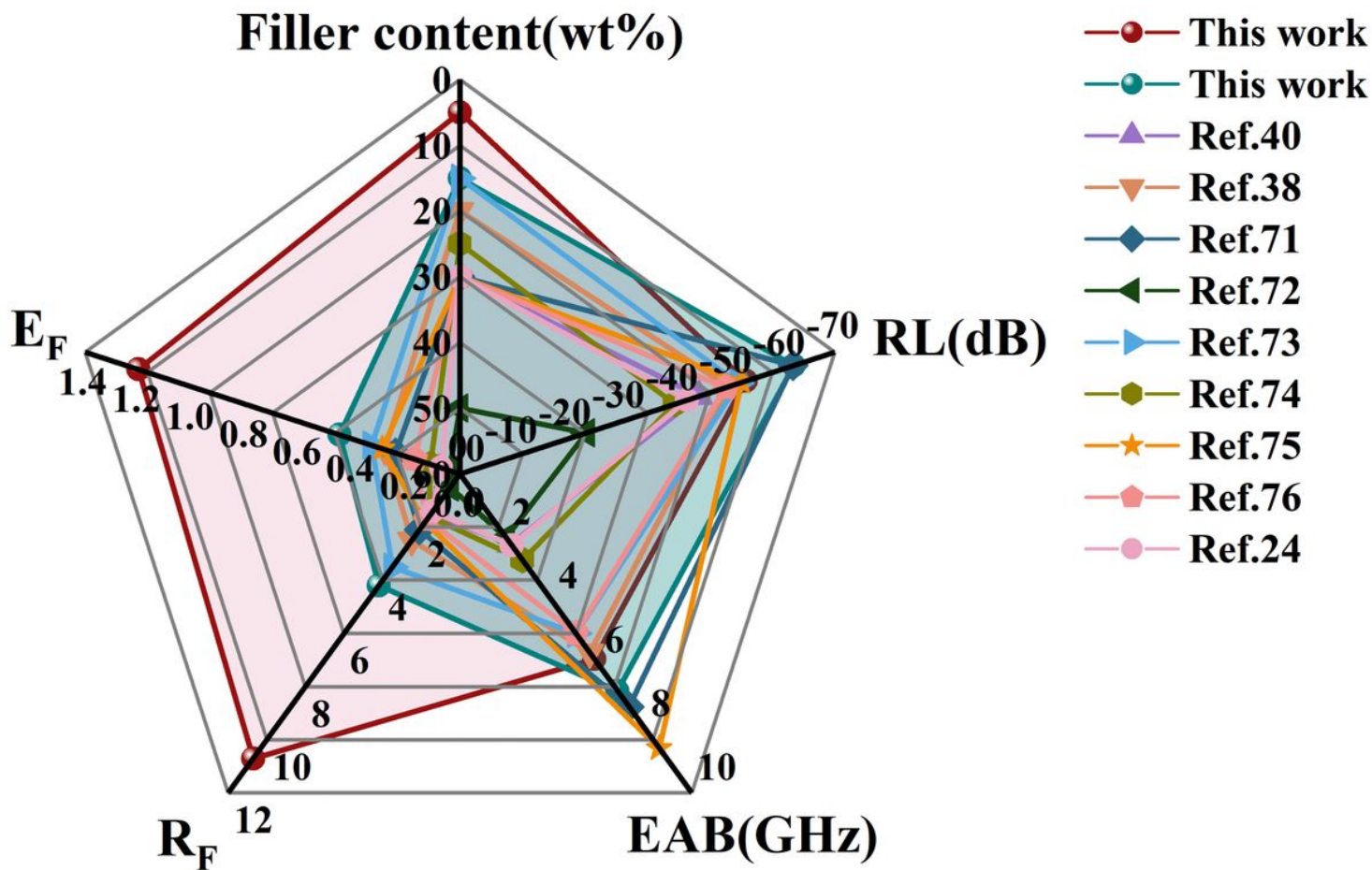


Figure 11

The comparison of EMA performance between this work and other studies.

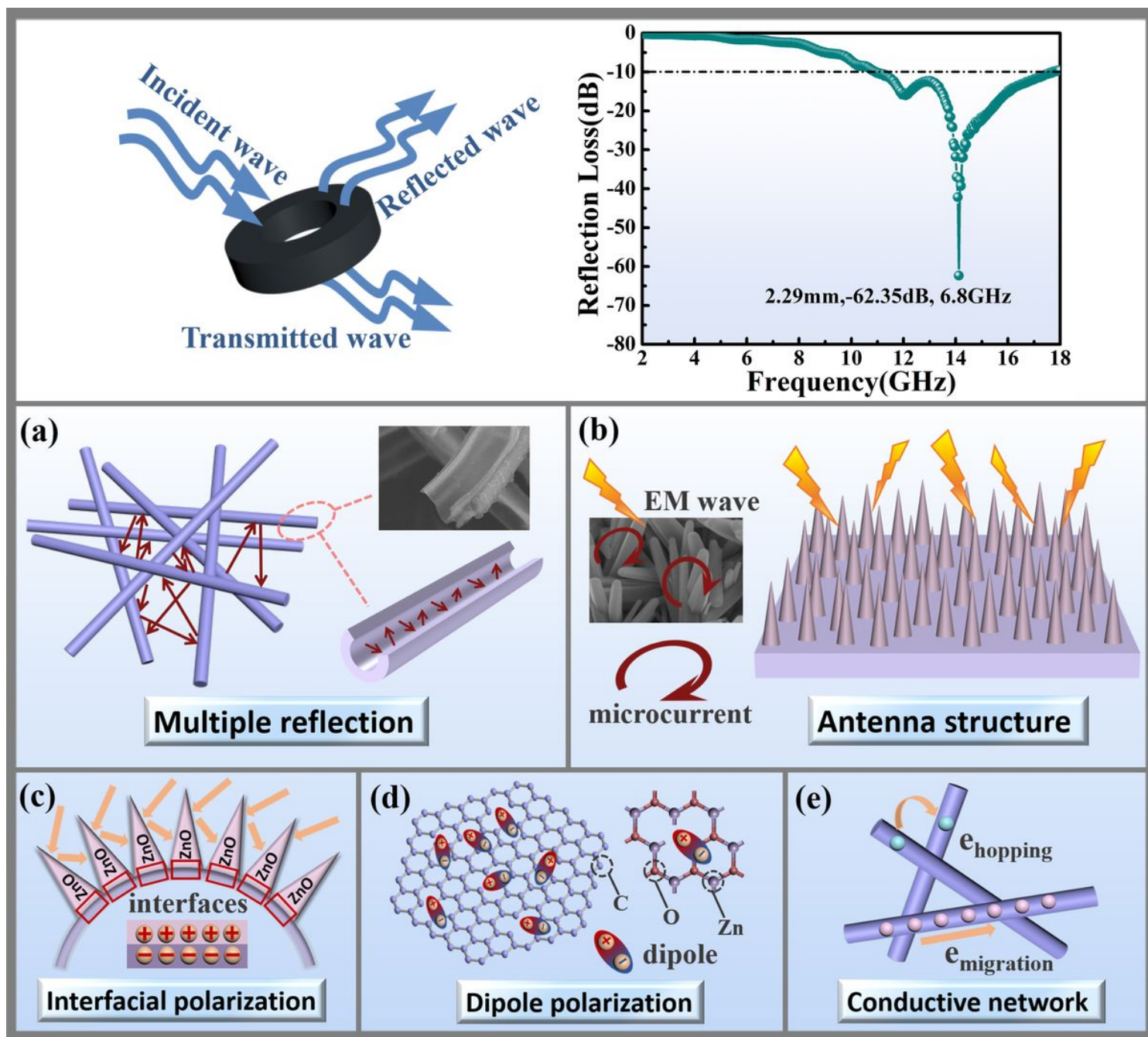


Figure 12

The schematic illustration of the electromagnetic microwave absorption of the BDCFs samples: multiple reflection (a), antenna structure (b), interfacial polarization (c), dipole polarization (d) and conductive network (e).

Supplementary Files

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- [ElectronicSupplementaryMaterial.docx](#)