

ISSI2020: An Approach for Obtaining Material Mechanical Properties in Structure Local Region Based on An Accurate Analysis of Micro-Indentation Test

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Title page

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An Approach for Obtaining Material Mechanical Properties in Structure Local Region Based on An Accurate Analysis of Micro-indentation Test

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Abstract: The welding and other hot or cold processing region behavior in important structures is the key characteristics for the structural integrity assessment, it is necessary to accurately derive the material mechanical properties in the failure driving force (such as stress and strain) analysis in the local area. The hot or cold processing would induce the change and the inhomogeneous of the material mechanical properties in the local processing region of the structure, and it is difficult to obtain the precise mechanical properties in these regions by the traditional material tensile test.

To accurately obtain actual material mechanical properties in the local region of structures, a micro-indentation test system has been established, which incorporated by a CMT6103 Material Test Device, an indenter displacement sensor and a group of special micro-indenter assemblies are established, and a numerical testing inversion analysis method by using ABAQUS software is also proposed in this paper. Based on above test system and analysis platform, an approach to obtain material mechanical properties in local region of structure is proposed and established. The verification experiment and analysis is performed by using a group of various changed mechanical property of 316L austenitic stainless steel through different cold-work hardening. The investigated results indicate the material mechanical properties and the micro-indentation morphological change have evidently relevance, and the material mechanical parameters, such as the yield stress σ_y , the strain hardening exponent n and others could be conveniently and effectively obtained by the proposed approach in this paper.

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Keywords: Structural integrity assessment • Micro-indentation test • Numerical testing inversion analysis • Local material mechanical property

1 Introduction

Manufacturing mechanical structures process including welding and other hot or cold has been broadly adopted in industrial field [1–2]. It is been reported the mechanical property of metal materials will be changed after the cold or hot processing [3–4]. Because the local area involved in hot and cold processing is easy to occur flaw and failure, it is a key area for structural integrity analysis [5]. To obtain the precise mechanical properties of these local structure materials for the structural integrity analysis will be contribute to the further understanding of manufacturing processing [6–7].

It is of great practical significance to develop a test and calibration method to obtain the mechanical property parameters and distribution law of inhomogeneous welded joint materials [8]. Indentation test has been widely used as a non-destructive testing method which does not affect the continued service of equipment and is easy to operate [9–10]. Scholars have done research works on the measurement of mechanical property by indentation method [11–12]. As early as 1961, Stillwell and Tabor [13] proposed to determine the mechanical properties by using the elastic recovery generated through the indenter to press into the material. Bulychiev et al. [14] measured the contact area through the unloaded part of the load-displacement curve, which laid the foundation for the later indentation hardness test. Tabor [15] studied the representative strain of the indentation plastic zone and obtained a series of relations, which played an important role in the subsequent research on the indentation method to characterize the stress and strain. Das et al. [16] studied the constitutive relationship and strength properties of two

high-strength low-alloy steels under different pre-strains by continuous ball indentation method. Wei ZK et al. [17–18] used nano-indentation to study the stress-strain relationship of metal thin film materials, and carried out detailed characterization of the mechanical properties of different metal materials. Shen Lei et al. [19] used the indentation method to accurately measure the residual stress and established the relationship between the indentation bulge and the residual stress. Wu Shengbao et al. [20–21] used continuous ball indentation tests to characterize the mechanical properties of different metal materials in detail. Pamnanil et al. [22] studied the mechanical properties of the weld area with different welding methods in the high-strength and low-alloy steel structure by using the ball indentation test. These researches indicate that it is possible to obtain material property by an indentation test and analysis.

The complex thermal cycle in the welding will cause the major changes in the micro-structure and chemical composition of the material in welded joint, which also would be produce a complicated local stress state in welded joint. To represent the effect of the hot or cold processing on materials, the change of local material mechanical properties is performed by the different degrees of tensile deformation in this paper [23–24]. Thus an approach to obtain the material mechanical properties combined with the ball indentation test and finite element inversion to characterize the mechanics of 316L austenitic stainless steel is discussed and studied.

2 Theoretical Principle

Under the action of external force, the metal material will undergo rapid and instantaneous elastic-plastic deformation [25]. Austenitic stainless steel and nickel-based alloys are widely used in nuclear power structures. The stress-strain relationship curve of this kind of metal can be represented by the stress-strain curve of a typical Linear Elastic-Power hardening material. In the elastic deformation stage, there is a linear correlation between stress and strain. In the plastic deformation stage, there is a power-rate relationship between stress and strain, called Hollomon relationship.

For the metal materials with hardening characteristic [26], the stress-strain curve can be defined as:

$$\sigma = \begin{cases} E\varepsilon & (\sigma \leq \sigma_y) \\ K\varepsilon^n = E\varepsilon_y^{1-n}\varepsilon^n & (\sigma \geq \sigma_y) \end{cases} \quad (1)$$

$$\varepsilon = \varepsilon_y + \varepsilon_p \quad (2)$$

where σ_y is initial yield stress, ε is total strain, ε_y is initial

yield strain, ε_p is plastic strain, E is the Young's modulus of material, K is strength factor, n is the strain hardening exponent.

When $\sigma > \sigma_y$, the plastic stress σ can be expressed by

$$\sigma = \sigma_y \left(1 + \frac{E}{\sigma_y} \varepsilon_p\right)^n \quad (3)$$

The micro-nano indentation test mainly includes two stages of loading and unloading. In the loading phase, the indenter enters the surface of sample, the area will undergo elastic deformation. As the applied load gradually increases, the area with the largest elastic deformation will begin to enter the elastoplastic stage, where plastic deformation occurs [27].

The indentation method is used to obtain the mechanical properties of materials is Oliver-Pharr method [28]. A large number of test studies have shown that the load-depth curve is mainly used to obtain parameters such as hardness and elastic modulus of the material. The mechanical properties of the plastic stage are mainly obtained through the dimensional method. The typical load-depth curve about indentation test is shown in Figure 1. Taking the spherical indenter for the indentation test, Figure 2 shows a schematic diagram of indentation profile geometry of the test material.

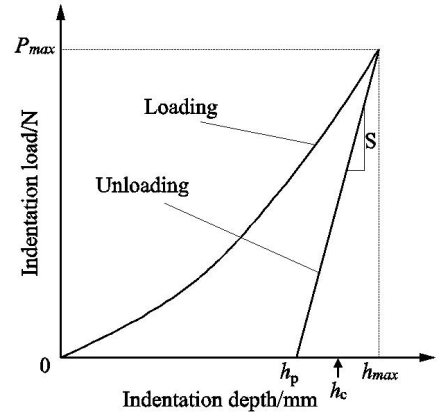


Figure 1 The typical load-depth curve

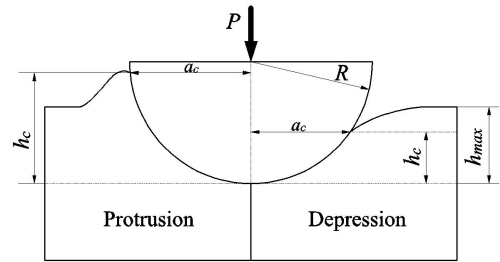


Figure 2 A schematic diagram of indentation profile geometry

In Figure 1 and Figure 2, h_{max} is the maximum depth value in the load-depth curve, P_{max} is the maximum load

value, S is the highest slope value of the unloading curve, h_p is the residual indentation depth, h_c is the contact depth value in the indentation process, a_c is the contact radius in the indentation test, and R is the ball indenter radius.

For a given shape of the indenter, the hardness value of the material can be obtained by

$$H = \frac{P_{max}}{A} \quad (4)$$

where A is indentation contact area, and $A = 2\pi rh_c$.

For the elastic contact theory, ignore the influence of microscopic materials in the direction and size effect errors, the impact of border effects, and the geometric size of the gauge length section of the sample is much larger than the maximum indentation depth. The surface of the sample is a geometric plane, and is considered to be an isotropic material, such as

$$E_{IT} = \frac{1 - \nu^2}{\frac{1}{E_r} - \frac{1 - \nu_i^2}{E_i}} \quad (5)$$

where E_{IT} is the Elastic modulus of the sample material, ν is the Poisson's ratio of the sample material. E_i is the Elastic modulus of the indenter material, ν_i is the Poisson's ratio of the indenter material. Diamond is usually selected as the indenter material, where $E_i = 1140\text{GPa}$, $\nu = 0.07$.

In the study of plastic parameter identification, the optimization method is usually used to calculate the plastic mechanical parameters in the indentation process. Through indentation test simulation of a large number of materials with different parameter combinations, optimize and fit the input parameters and output results, establish the relationship between press-in measurable parameters and material parameters, and solve the required mechanical parameters. Where

$$\log P = \log \left[2.8\pi k c^{n+2} \left(\frac{0.2}{R} \right)^n \right] + m \log a \quad (6)$$

where $a = \sqrt{2Rh - h^2}$, $m = n + 2$, and n can be calculated from the slope of $\log P$ and $\log a$ curve.

To simplify the relationship between the analysis parameters and the identification parameters, and reduce the sensitivity of test errors, it has become a concern for this type of method. The accuracy and stability of the analysis method and the comparison verification with the uniaxial tensile test results are important links in the identification of plastic mechanical properties.

For the ball indenter, T Zhang established the

relationship between σ_y and W_u/W_t . D Ma established the relationship between σ_b and W_u/W_t [29]. Where W_u is unloading work, W_t is the total work from loading to complete unloading.

Based on the description of the related literature on the relationship between the work obtained by the load-depth curve and the mechanical properties of the material, the paper focuses on the relationship between unloading work and total work to predict material strength performance. The load-depth curve is composed of plastic work and elastic work. The sum of the two is the total indentation work. The schematic diagram of the composition is shown in Figure 3.

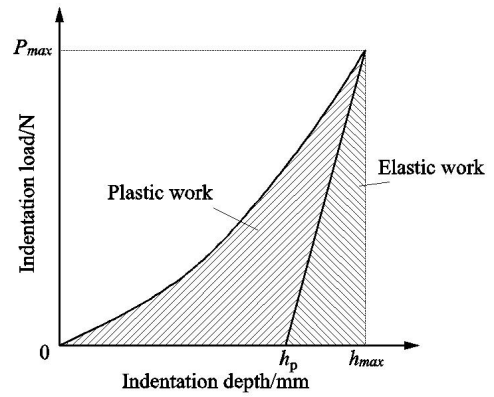


Figure 3 Composition of indentation work

The physical quantities involved in the pressing process include material parameters (E , ν , σ_y , n), indenter geometric parameters (R), control variable (h , h_{max}). E and h are selected as basic quantities, and the indentation loads P , W_u , W_t are expressed by the basic quantities.

In the loading stage, the load P can be expressed as

$$P = f_F(E, \nu, \sigma_y, n, R, h) \quad (7)$$

According to the definition of total indentation work, where

$$W_t = \int_0^{h_{max}} P dh = \frac{E h_{max}^3}{3} \prod_1 \left(\frac{\sigma_y}{E}, \nu, n, R \right) \quad (8)$$

The unloading work can be expressed as

$$W_u = \int_{h_p}^{h_{max}} P dh = E h_{max}^3 \prod_2 \left(\frac{\sigma_y}{E}, \nu, n, R \right) \quad (9)$$

Through the Eq. (7), Eq. (8) and Eq. (9), the relationship between unloading work and total indentation work can be obtained as

$$Y = \frac{W_u}{W_t} = \prod_3 \left(\frac{\sigma_y}{E}, \nu, n, R \right) \quad (10)$$

3 Indentation Test

3.1 Sample Preparation

In this paper, 316L austenitic stainless steel is processed into standard tensile specimens for testing. The geometric dimensions of the specimens are shown in Figure 4. The specimens is stretched to the gauge length of the sample to 2mm, 4mm, 6mm respectively by using the tensile testing machine, that is, the tensile elongation are 10%, 20%, and 30%, for expressing the changes in the mechanical properties of materials by hot and cold processing.

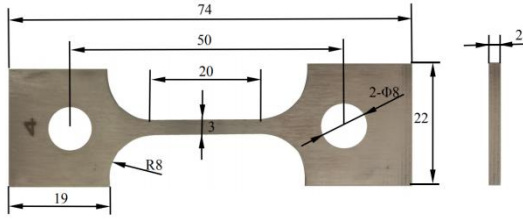


Figure 4 Plate-shaped tensile specimen

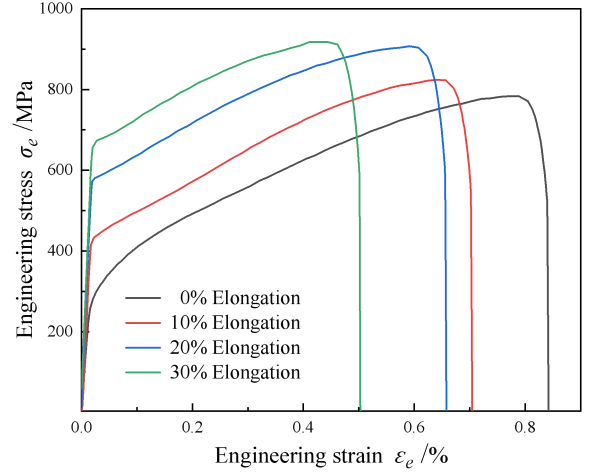
To remove the scratches on the surface and avoid the influence of surface roughness of the sample on the test results, the surface of the sample is evenly polished with 600#, 1000#, 1500#, 2000# waterproof abrasive paper before the test, and replaced different types of waterproof abrasive paper, the sample needs to rotate 90°. After the sanding process is completed, use the metallographic polishing machine to polish the sample, the particle size is 1W, the sample scratches are not obvious after polishing to the microscope.

Figure 5a shows the engineering stress-strain curve of 316L austenitic stainless steel with different cold working rates obtained through tensile experiments. The engineering stress-strain curve obtained is transformed into a true stress-strain curve by Eq. (11) and Eq. (12), as shown in Figure 5b.

$$\varepsilon_t = \int_{l_0}^l \frac{dl}{l} = \ln \left(\frac{l}{l_0} \right) = \ln(1 + \varepsilon_e) \quad (11)$$

$$\sigma_t = \sigma_e (1 + \varepsilon_e) \quad (12)$$

a



b

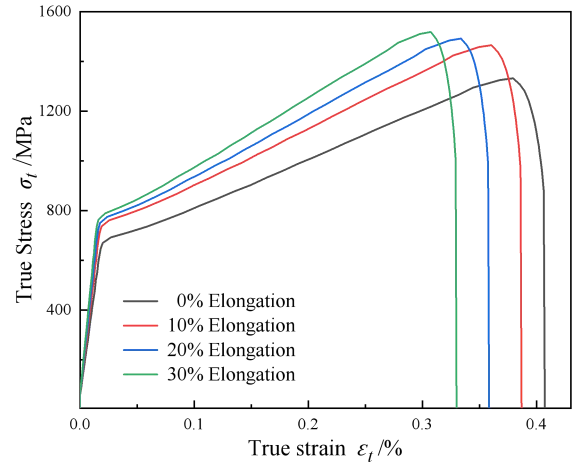


Figure 5 **a** Engineering stress-strain curve under different elongations; **b** true stress-strain curve under different elongations

3.2 Parameter Setting of Indentation Test

The indentation test platform has been modified on the basis of the electronic universal testing machine. Figure 6 shows the modified indentation test platform.

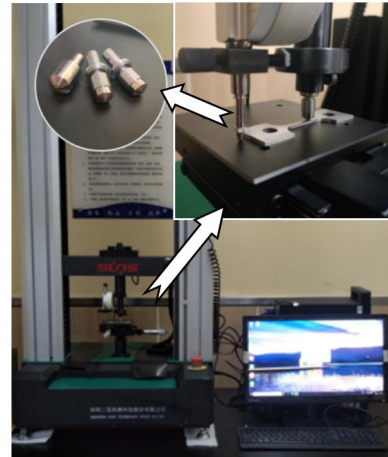


Figure 6 Indentation test system platform

The specific modified ideas of the system are: the loading system adopts the electronic drive system of the electronic universal testing machine; the upper chuck of the testing machine is improved to be able to hold different types of indenters, and the lower chuck is changed to a sample platform that can be adjusted autonomously in two dimensions. A high-precision displacement sensor is installed on the side of the indenter to ensure synchronous acquisition of indentation depth. The accuracy of the high-precision displacement sensor is 0.5% of the full scale, and the resolution reaches 0.1 μ m, and its accuracy satisfy the requirements of the indentation test.

The parameters for setting the indentation test are ball indenter radius, loading and unloading rate, loading and unloading load. The parameter settings of the test platform are as follows:

(1) Ball indenter radius

The ball indenter cannot be greater than one third of the tested sample. Considering the micro-loss characteristics of indentation testing technology, the cemented carbide spherical indenter with a radius of 0.25 mm be used in the indentation test, its dimensional accuracy is ± 0.001 mm;

(2) Loading and unloading rate

The loading rate is set to 0.5 mm/min, and the unloading rate is set to 0.1 mm/min in the indentation test. The loading process takes a long time, and more data needs to be collected. During unloading process, the elastic recovery of the indentation depth is mainly measured. Therefore, the unloading rate is set faster than the loading rate to ensure that the data collected during the entire indentation process is more appropriate.

(3) Loading and unloading load

The loading load of the indentation test is set to 300 N, and the unloading load is set to 3 N. The indentation load with an indentation depth of 0.1~0.2 mm needs to be between 150~300 N. The unloaded load only needs to rebound after the indentation.

After setting the relevant parameters of the indentation system, the ball indentation test is on performed on tested materials with different elongations to obtain the indentation response results.

4 Finite Element Model

The finite element analysis software ABAQUS is used for indentation simulation test in this paper. The indentation process is completely symmetric, to facilitate the calculation and ensure the validity of the calculation results, this paper establishes a quarter of the three-dimensional model.

In the finite element inversion, the radius of the indenter, the thickness of the tested sample and the setting of related test parameters are all corresponding to the indentation test.

The Elastic modulus of 316L austenitic stainless steel without pre-deformation, elongation of 10%, 20%, and 30% is set to 210GPa, and the Poisson's ratio is set to 0.3. The material parameters in the plastic phase are the true stress-strain values obtained from uniaxial tensile tests. For the setting of the material parameters of the indenter, the Elastic modulus is set to 1×10^{31} GPa, and the Poisson's ratio is set to 0.3. In the indentation process, the indenter is set as a rigid body.

The finite element inversion adopts displacement loading method, the loading displacement in the loading analysis step is 0.2 mm, the unloading displacement in the unloading analysis step is 0 mm. The bottom of the tested sample is set in the Y direction, and the indenter is set to only move in the Y direction. The boundary condition constraints are shown in Figure 7.

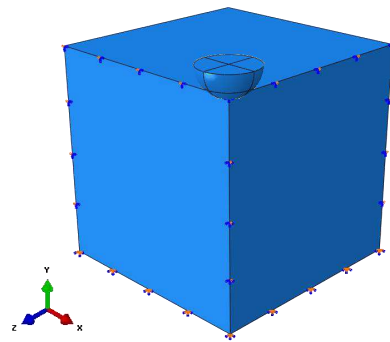


Figure 7 The boundary condition constraints

The quality and quantity of meshes in finite element calculations are critical to the results of calculations. The quality of the grid directly affects the accuracy of the simulation calculation. Reasonable division of the grid can effectively improve the computational efficiency of the finite element model. In this model, the size of the grid is a three-dimensional element grid (CPS4R), and the total number of division units is 44910. The mesh of the contact part of the sample with indenter needs to be refined. The mesh refinement model is shown in Figure 8.

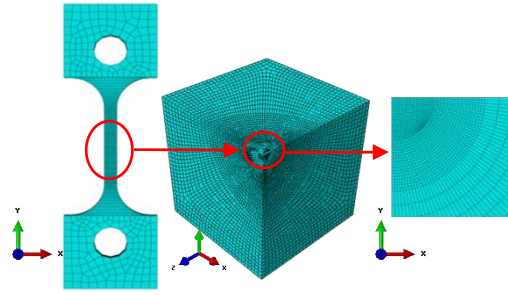


Figure 8 The mesh refinement model

The analysis steps in the finite element inversion are the preloading process, pressing-in process and unloading process. Setting the preloading step mainly requires the indenter to contact the sample to ensure the accuracy of displacement during the indentation process. The press-in step is set to displacement control. Setting the unloading step is mainly to calculate the mechanical properties of the material in the elastic phase. In the contact analysis, the friction coefficient f between the indenter and the sample is set to 0.3.

5 Results and Discussions

5.1 Indentation Test Results

The load-depth curves obtained by the indentation test of austenitic stainless steel with no pre-deformation and 10%, 20%, 30% elongations under the indentation load of 0~300 N are shown in Figure 9.

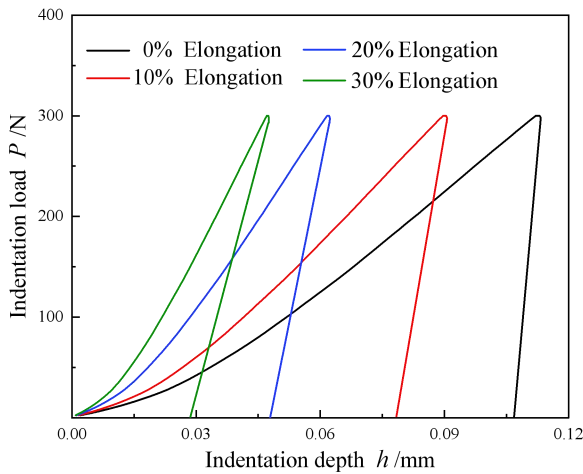


Figure 9 The load-depth curve obtained by indentation test under different elongations

It can be seen from Figure 9 that the loading and unloading trends of the curves are roughly the same. The slope of the curve in the loading phase gradually increases with the increase of the pre-deformation degree, indicating that the elastic model of the material also increases. During the unloading stage, the load value per unit area also gradually increases.

After the pre-deformation of the austenitic stainless steel material, the load-depth curve is clearly shifted to the left, indicating that the material becomes harder after pre-deformation, resulting in a smaller indentation response and a smaller residual indentation depth value.

According to the parameters of load-depth curve and the Oliver-Pharr method, the Elastic modulus and hardness values of 316 austenitic stainless steel under different elongations is shown in Figure 10. It can be seen that the Elastic modulus of the material gradually increases with the increase of the pre-deformation degree, but the change rate gradually decreases.

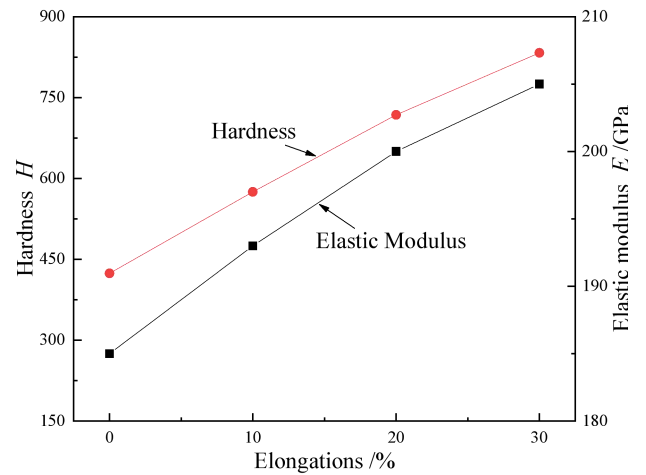


Figure 10 Change law of Elastic modulus and hardness under different elongations

When the material is not pre-deformed, the Elastic modulus is 185 GPa, and when the elongation is 30%, the Elastic modulus is 203 GPa. For the indentation hardness, as the degree of pre-deformation gradually increases, the indentation hardness of the material also increases. When the material is not pre-deformed, the indentation hardness is 424 MPa, and when the elongation is 30%, the indentation hardness reaches 833 MPa.

The indentation method obtains the plastic mechanical parameters of austenitic stainless steel mainly relies on the load-depth curve to calculate the yield strength, yield strain and hardening exponent.

For the calculation of yield strength, the area of the curve is used to estimate the energy in the indentation process, and then the strength value is calculated by the obtained energy. The hardening exponent is calculated by the self-similarity theory and the logarithmic slope between the load and the residual indentation area in the load-depth curve. The calculated unloading work, total indentation work, ratio and yield strength are shown in Table 1.

Table 1 Load-depth curve parameters of austenitic stainless

steel and mechanical parameters with different elongations

Elongation %	Unloading work W_u	Total work W_t	Yield strength σ_y /(MPa)	Tensile strength σ_b /(MPa)	Ratio Y
0	1.52	37.88	350	1331	0.040
10	2.61	50.57	474	1362	0.052
20	4.13	62.93	596	1401	0.066
30	5.46	73.47	685	1452	0.074

The yield strength and tensile strength in Table 1 are respectively linearly fitted to the ratio Y , and the fitted curve diagrams are shown in Figure 11a and b. The correlation coefficient are $R^2=0.998$ and $R^2=0.999$, respectively. The the linear relations about Eq. (13) and Eq. (14) are obtained as

$$\sigma_y = 9682.38Y - 35.32647 \quad (13)$$

$$\sigma_b = 3632.4Y + 1180.8 \quad (14)$$

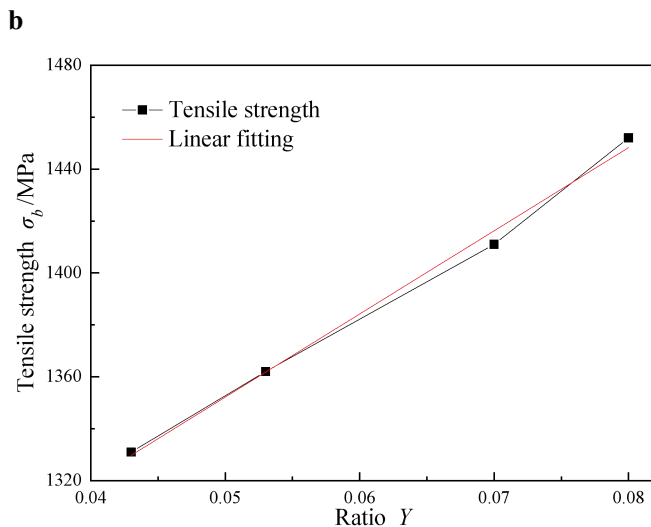
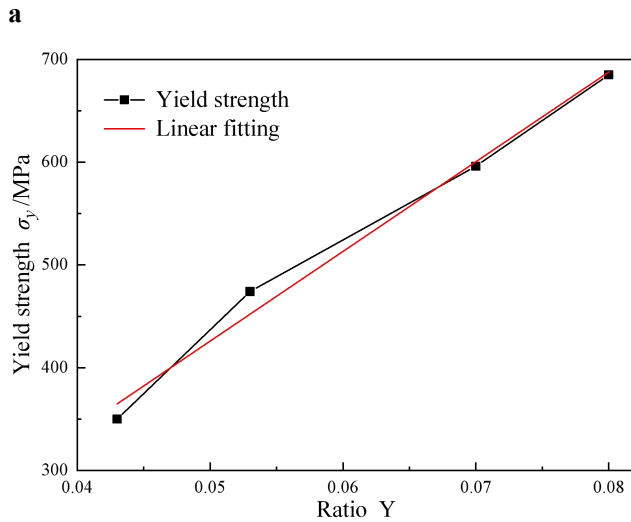


Figure 11 a Fitting curve of yield strength and ratio Y ; **b** fitting curve of tensile strength and ratio Y

The hardening exponent values of materials with different elongations are shown in Figure 12. It can be seen that as the pre-deformation degree of austenitic stainless steel increases, the hardening exponent also increases.

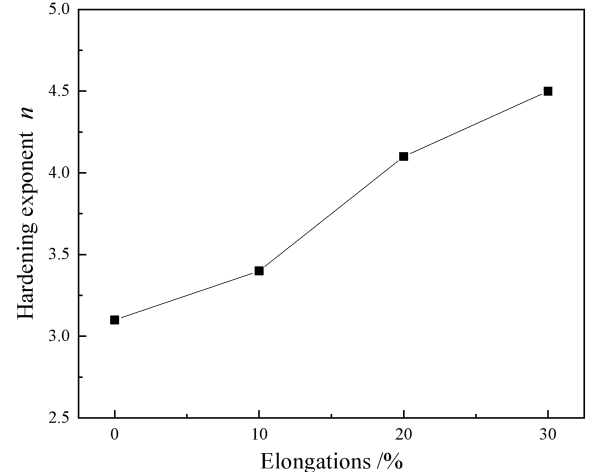


Figure 12 Change law of hardening exponent under different elongations

In addition, there is a linear increase relationship between the hardening exponent and the elongations. When the sample is not pre-deformed, the hardening exponent is 3.4. When the elongation is 30%, the hardening exponent reaches 4.5. After the cold working process, the work hardening occurs inside the material, which leads to an increase in the plastic property of the material, so that the hardening exponent of the material also increases.

5.2 Finite Element Inversion Analysis Results

Figure 13 shows the load-depth curve of 316L austenitic stainless steel under four different elongations through indentation simulation.

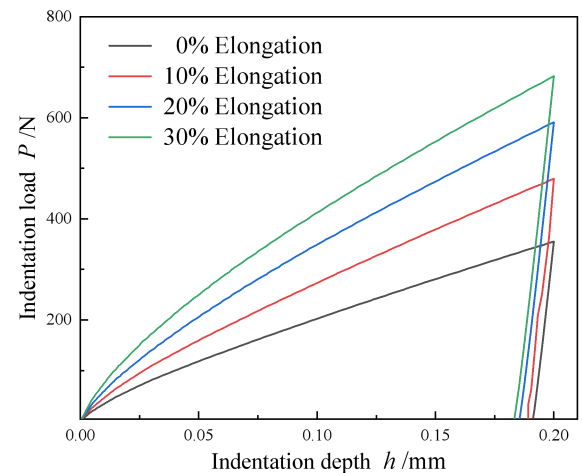


Figure 13 The load-depth curve obtained by finite element inversion under different elongations

It can be seen that the indentation simulation process of materials with different elongations is roughly the same. The loading curve during the pressing process shows a nonlinear trend. As the elongation increases, the required indentation force gradually increases. It shows that with the gradual increase of the elongation, the Elastic modulus and hardness of the tested material both increase.

In addition, the unloading displacements of the four unloading curves have obvious differences.

Pre-deformation has a certain effect on the rebound of the material. As the elongation increases, the residual depth of the sample gradually decreases. The material undergoes plastic deformation after pre-stretching, resulting in an increase in its yield strength and hardness. The load-depth curve obtained by the finite element inversion is consistent with the trend of the indentation test, so the accuracy of the indentation simulation is considered to be higher.

The indentation morphology of austenitic stainless steel with different elongations is obtained by finite element simulation. Figure 14a and b show the indentation process of 10% elongation.

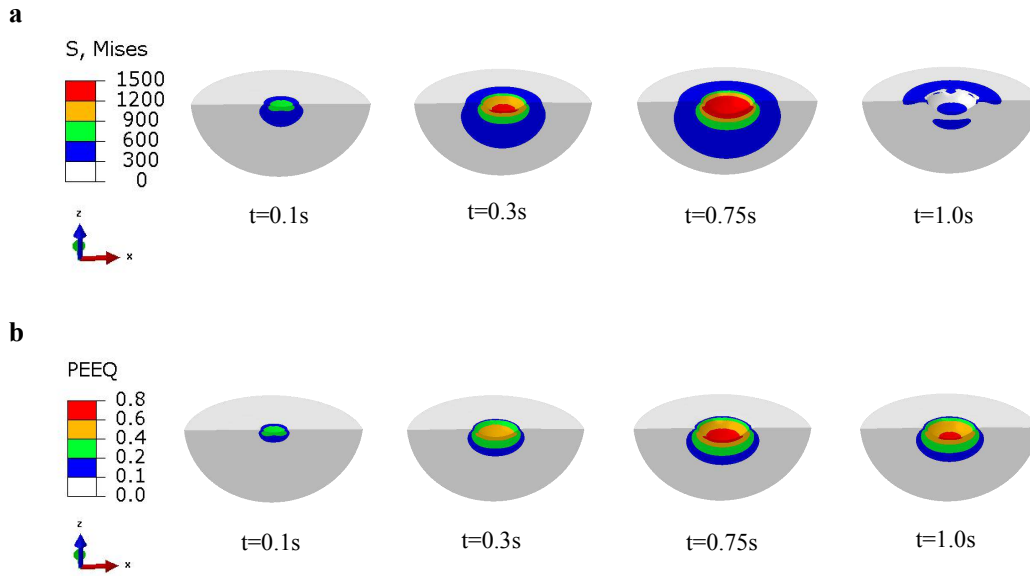


Figure 14 **a** Mises stress of indentation process under 10% elongation; **b** equivalent plastic strain (PEEQ) of indentation process under 10% elongation

Figure 14a of $t=0.1s$, $t=0.3s$, $t=0.75s$ show the loading stage of the pressing process. It can be seen that as the pressing depth increases, the maximum principal stress of Mises gradually increases. Figure 14a of $t=1.0s$ shows the unloading stage of the indentation test. Compared with the stress cloud diagram at the maximum depth of the loading stage, it can be seen that after unloading, the material has gone through the elastic recovery stage, and the maximum principal stress of Mises is reduced. Figure 14b shows the equivalent plastic strain (PEEQ) of the indentation process. During the loading phase, PEEQ increases as the depth of the indentation. After the indenter is pressed into the maximum indentation depth, the unloading begins. When the maximum depth is reached, the indenter begins to unload. The unloaded material passes through the elastic release stage, its strain and strain range are reduced.

The displacement increment on the same path of the material surface on the side in contact with the indenter is analyzed, as shown in Figure 15.

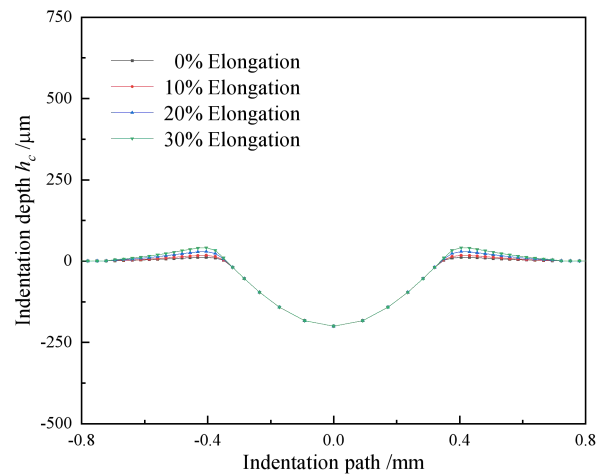


Figure 15 Comparison of maximum indentation morphology under different elongations

It can be seen from the Figure 15 that the displacement increment trend of materials with different elongations on the indentation path is the same. The materials in contact with the area under the indenter will first produce elastic deformation because of the indenter. As the load continues to increase, the indenter will continue to press down, and the material will undergo plastic deformation, and the downward increment will gradually increase. The material in the area around the indenter gradually accumulated. The maximum protrusion of undeformed material is $28.603\mu\text{m}$, the maximum protrusion of 10% elongation is $29.954\mu\text{m}$, the maximum protrusion of 20% elongation is $34.418\mu\text{m}$, and the maximum protrusion of 30% elongation is $39.406\mu\text{m}$.

5.3 Comparison of Results

The mechanical properties of materials with different elongations obtained in the indentation test need to be verified. The results obtained in the uniaxial tensile test are the agreed true values.

Figure 16a and b show the comparison between the mechanical properties of austenitic stainless steel 316L calculated by the indentation test and the uniaxial tensile test under the different elongation conditions.

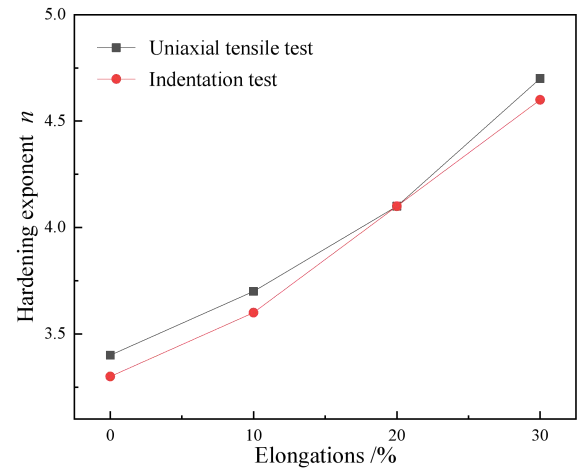
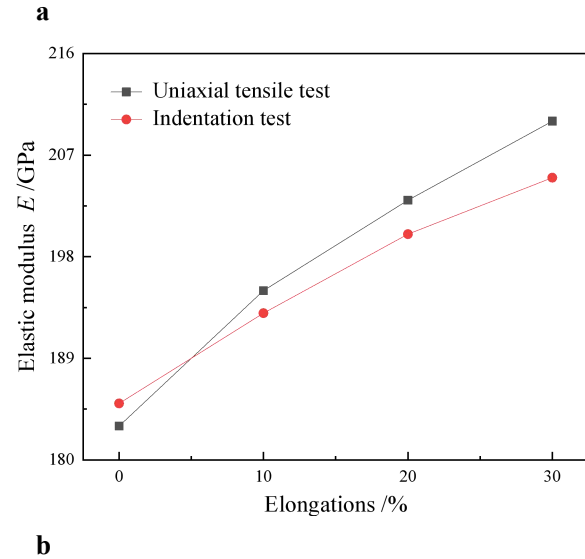
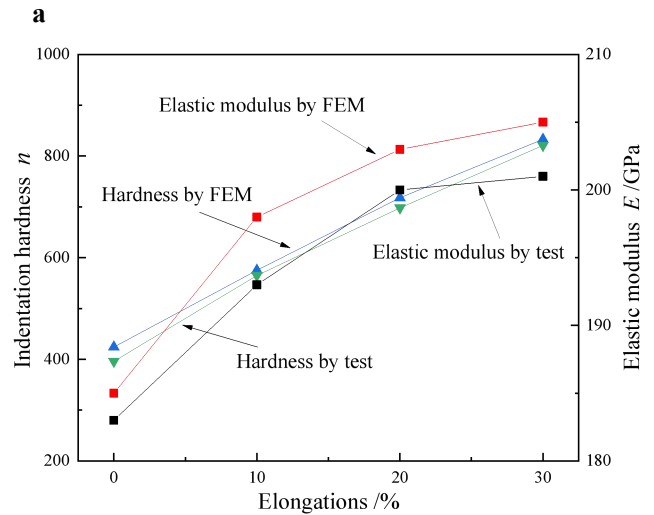


Figure 16 Comparison of mechanical parameters obtained by indentation test and tensile test under different elongations: **a** Elastic modulus; **b** hardening exponent

It can be seen from Figure 16 that the mechanical property parameters of austenitic stainless steel at different elongations obtained by the indentation test are relatively close to the uniaxial tensile test. The mechanical properties calculated by the indentation test have high accuracy and a small error range. The errors of elastic modulus are all less than 3%. The errors of the hardening exponent are less than 5%.

To verify the accuracy of the finite element model, it is necessary to verify the indentation test results obtained by the finite element method to ensure the accuracy of mechanical parameters. Figure 17a and b show the comparison of the deviation of the mechanical parameters calculated by the indentation test and the finite element method.



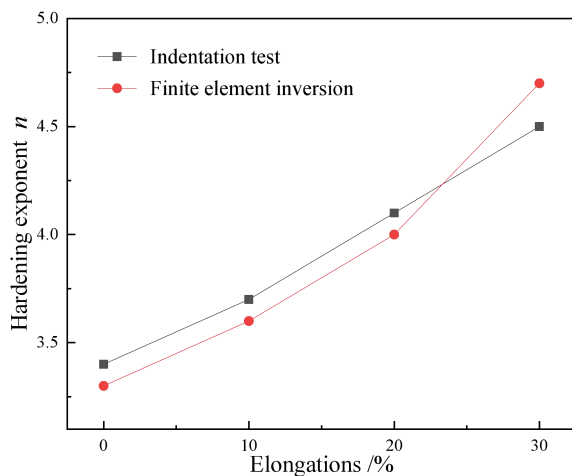


Figure 17 Comparison of mechanical parameters obtained by indentation test and finite element method with different elongations: **a** Elastic modulus and hardness; **b** hardening exponent

It can be seen from the Figure 17 that the mechanical properties have little difference between the indentation test and finite element simulation under different elongations, thereby the accuracy of the established finite element model is confirmed. The error of Elastic modulus are below 3%, and the error of indentation hardness is about 5%. The error of the hardening exponent is about 5%, and the reason for the larger error is the small transition zone between the elasticity and plasticity of the stress-strain curve, but it is within the acceptable range.

6 Conclusions

This paper mainly uses the micron-level indentation test system built by the laboratory to perform indentation tests on austenitic stainless steel 316L under different elongations, with the aid of finite element inversion analysis, the indentation process simulation was realized, and the mechanical performance parameters were compared. The following conclusions can be drawn from this study:

- (1) A suitable test program was developed for indentation test, and the load-depth curves of austenitic stainless steel 316L under different elongations were obtained. As the elongation increases, the curve shifts to the left, the resulting indentation response becomes smaller, and the residual indentation depth value becomes smaller.
- (2) The indentation test model was established using the finite element software ABAQUS, and the relevant mechanical property parameters of materials with different elongations were obtained by inversion analysis. Comparing them with the indentation test, the

deviations are all within 5%, which ensures the accuracy of the finite element model.

- (3) Compared with the test results obtained from the tensile test based on the plate-shaped tensile specimen, the deviations of the elastic-plastic material mechanical parameters, such as yield stress, Elastic modulus, hardening exponent and others are within 5% obtained through the indentation test and the finite element inversion analysis.
- (4) It provides a reasonable and effective structural integrity evaluation to obtain the actual material mechanical property of the welding and other hot or cold working areas in key structures.

7 Declaration

Acknowledgements

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Availability of data and materials

The datasets supporting the conclusions of this article are included within the article.

Authors' contributions

The author' contributions are as follows: HX was in charge of the whole trial; JH wrote the manuscript; JZ and YX assisted with sampling and laboratory analyses. All authors read and approved the final manuscript.

Competing interests

The authors declare no competing financial interests.

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Figures

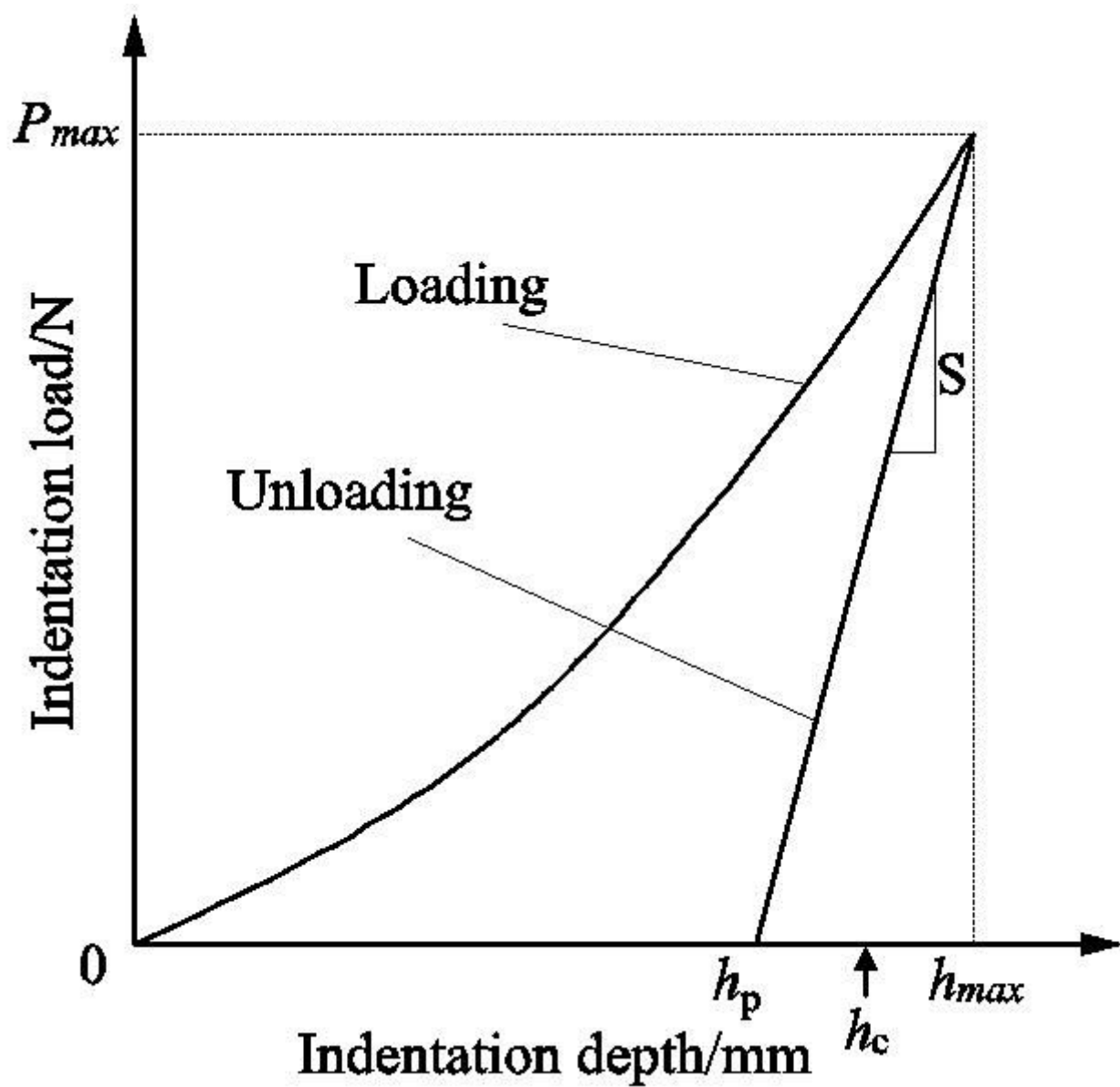


Figure 1

The typical load-depth curve.

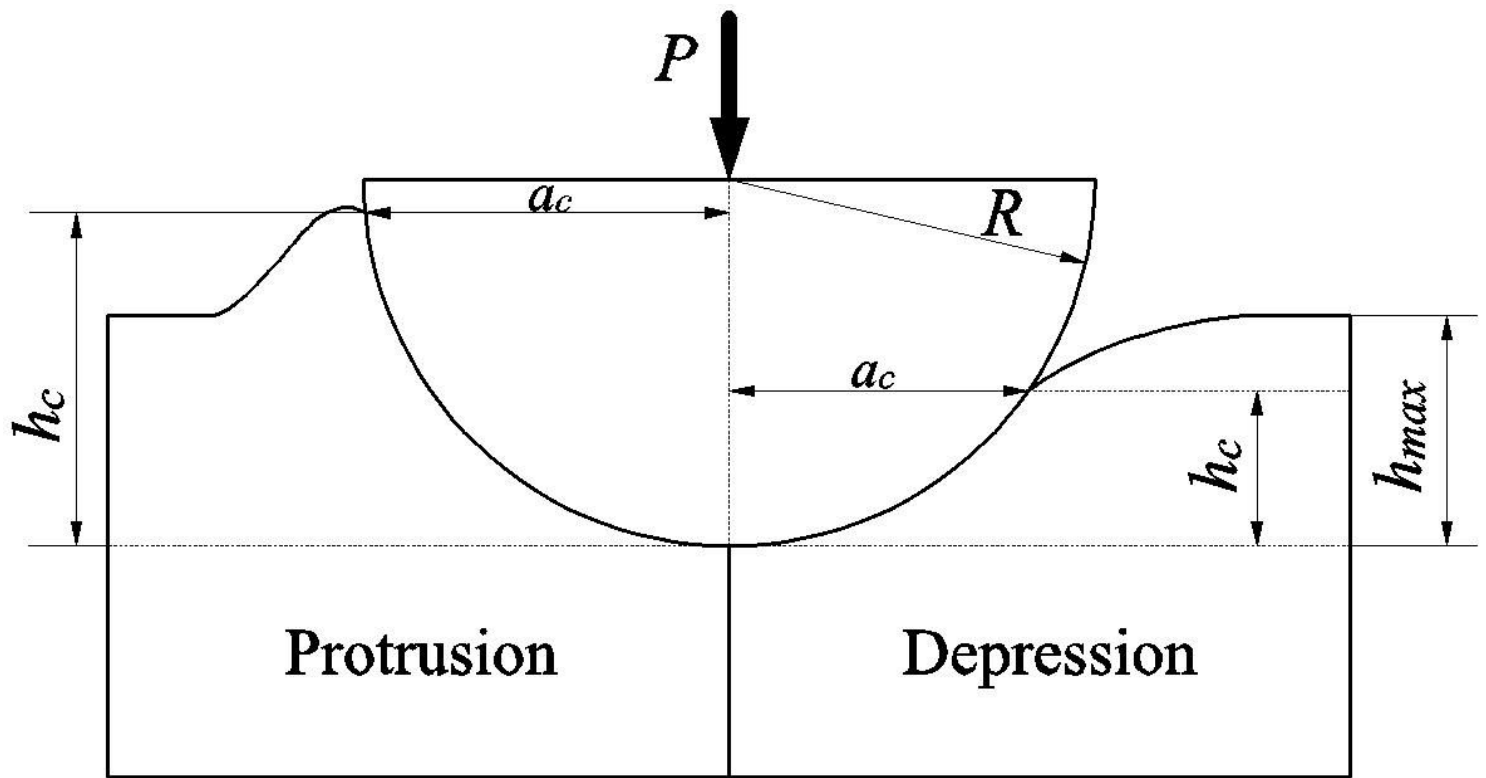


Figure 2

A schematic diagram of indentation profile geometry.

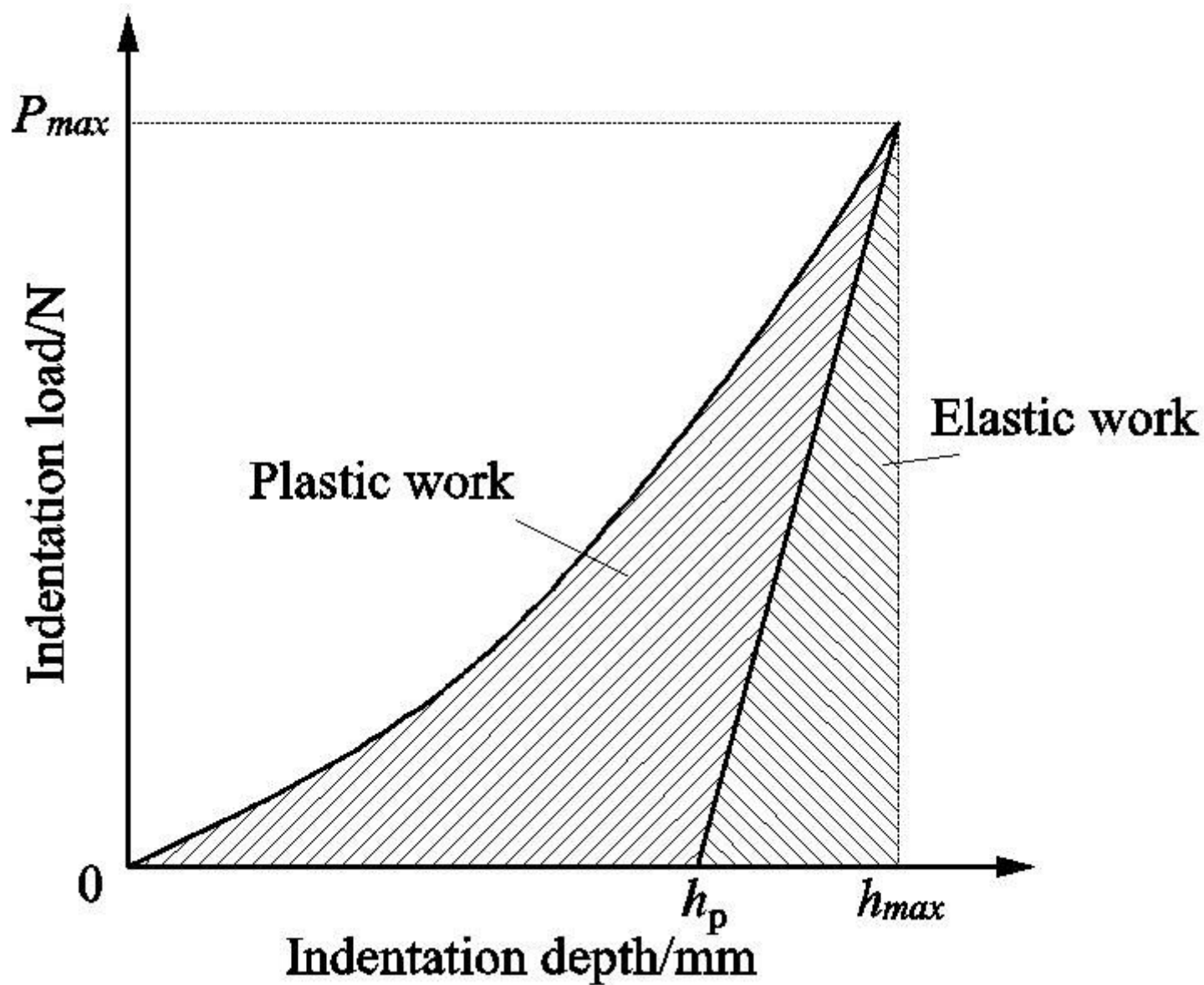


Figure 3

Composition of indentation work.

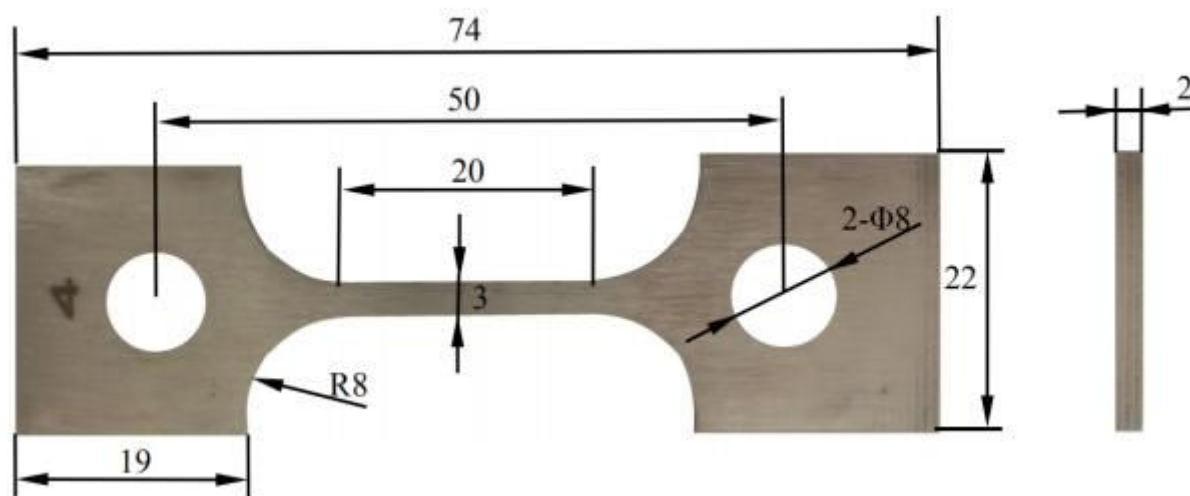
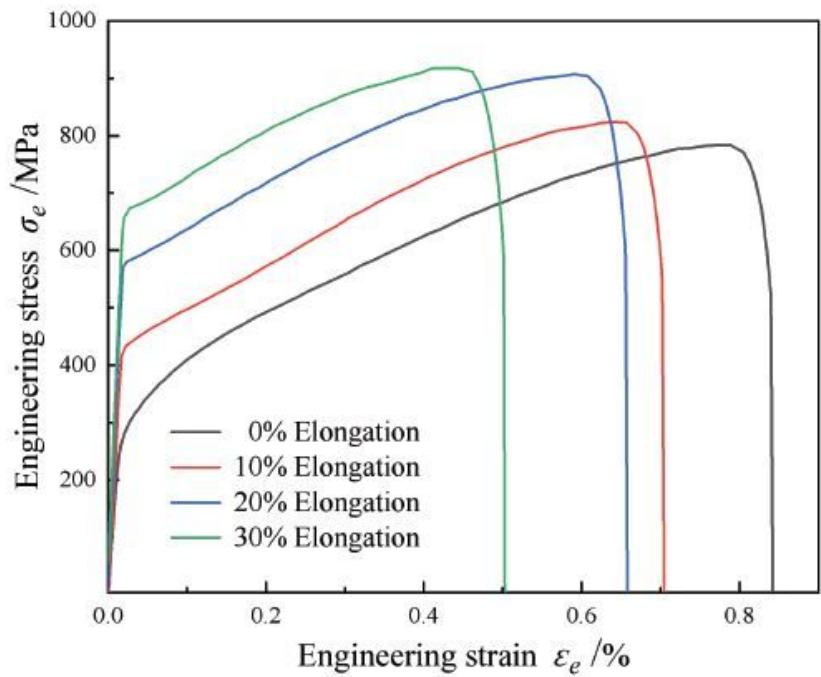


Figure 4

Plate-shaped tensile specimen.

a



b

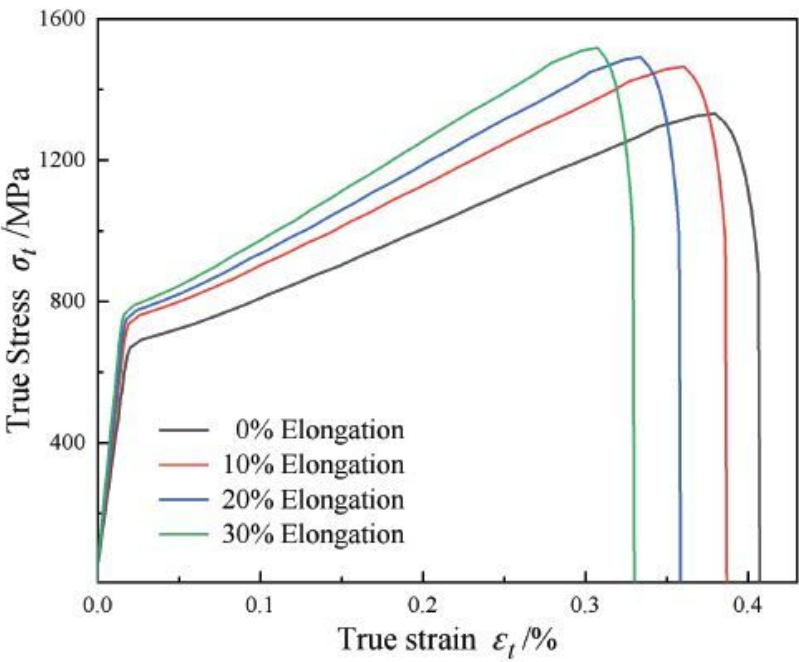


Figure 5

a Engineering stress-strain curve under different elongations; b true stress-strain curve under different elongations.

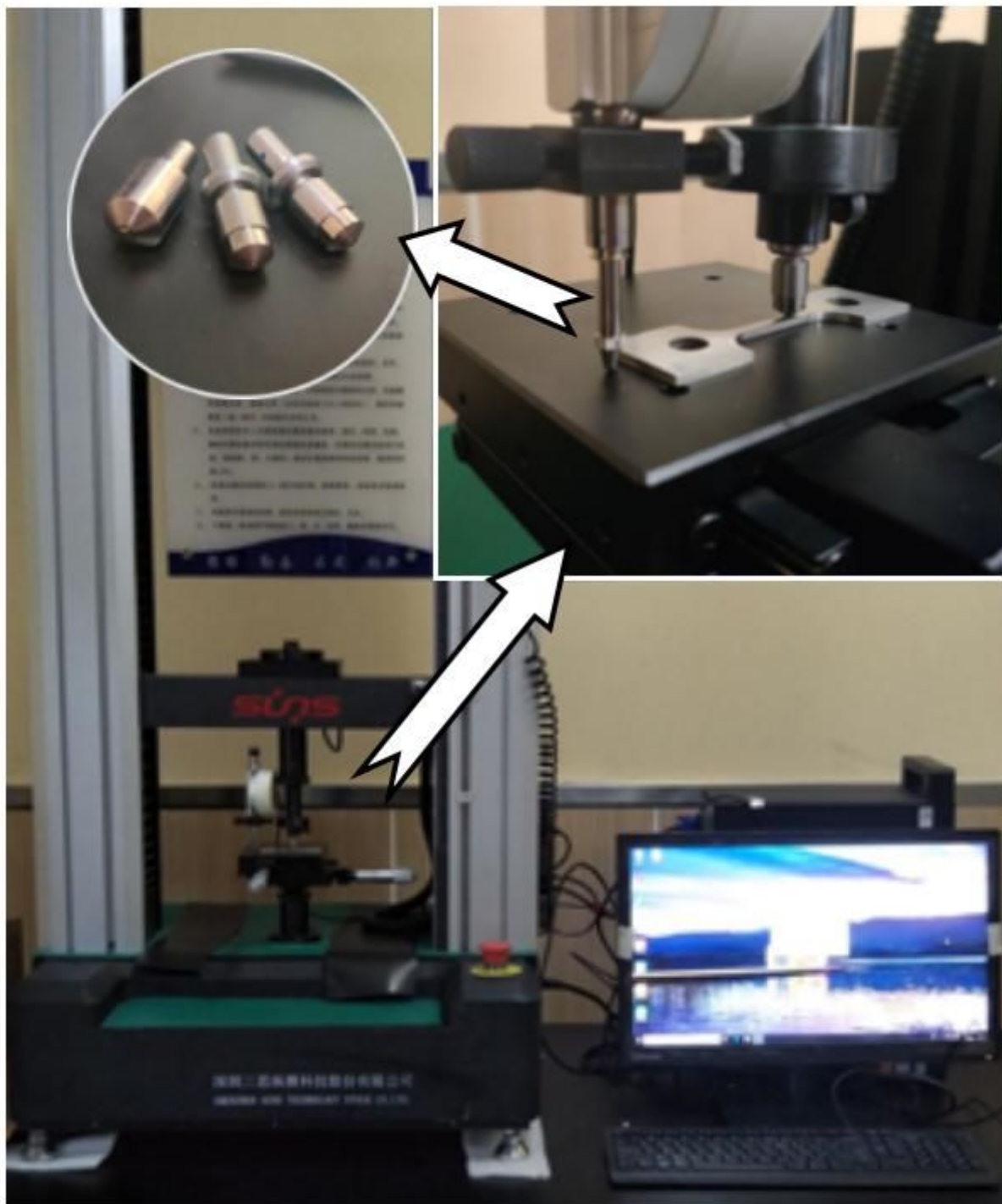


Figure 6

Indentation test system platform

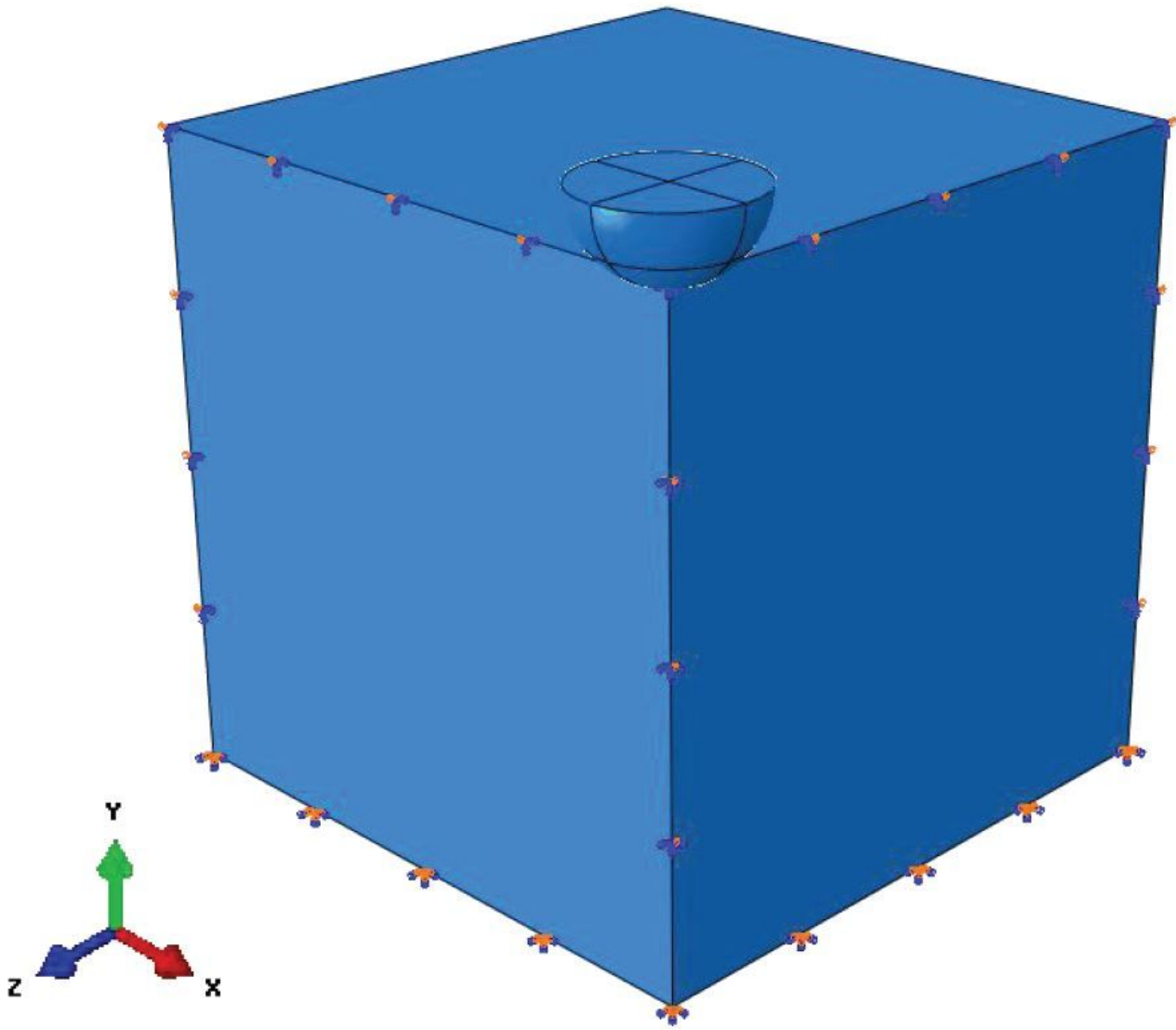


Figure 7

The boundary condition constraints

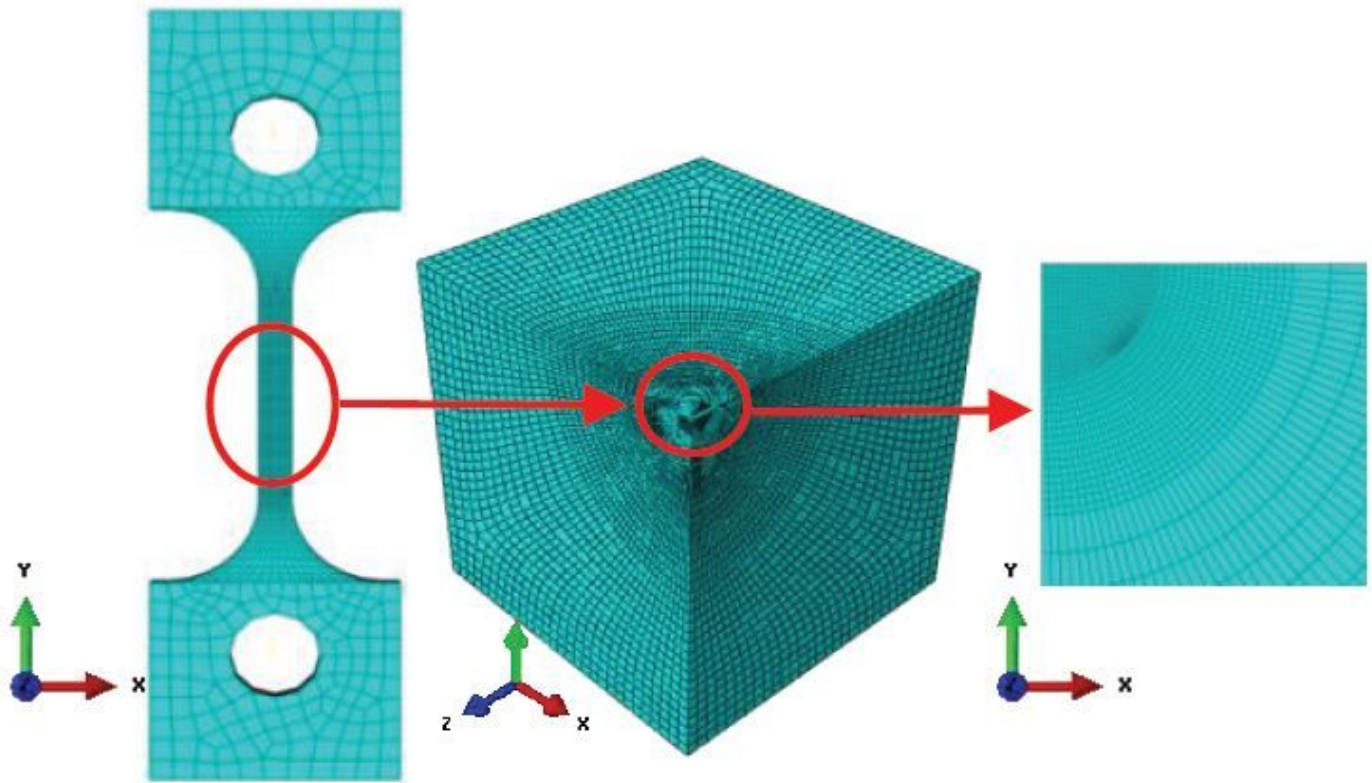


Figure 8

The mesh refinement model

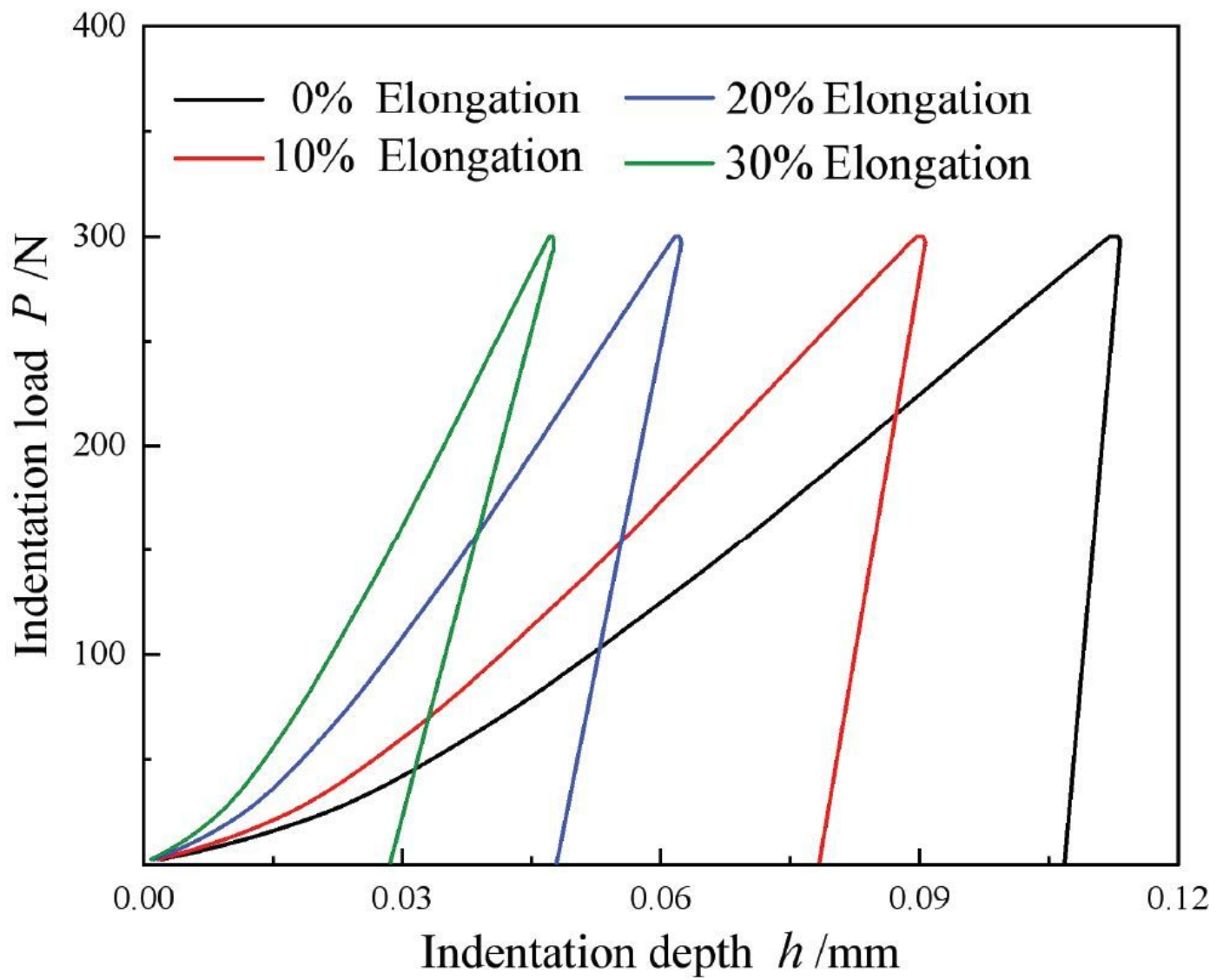


Figure 9

The load-depth curve obtained by indentation test under different elongations

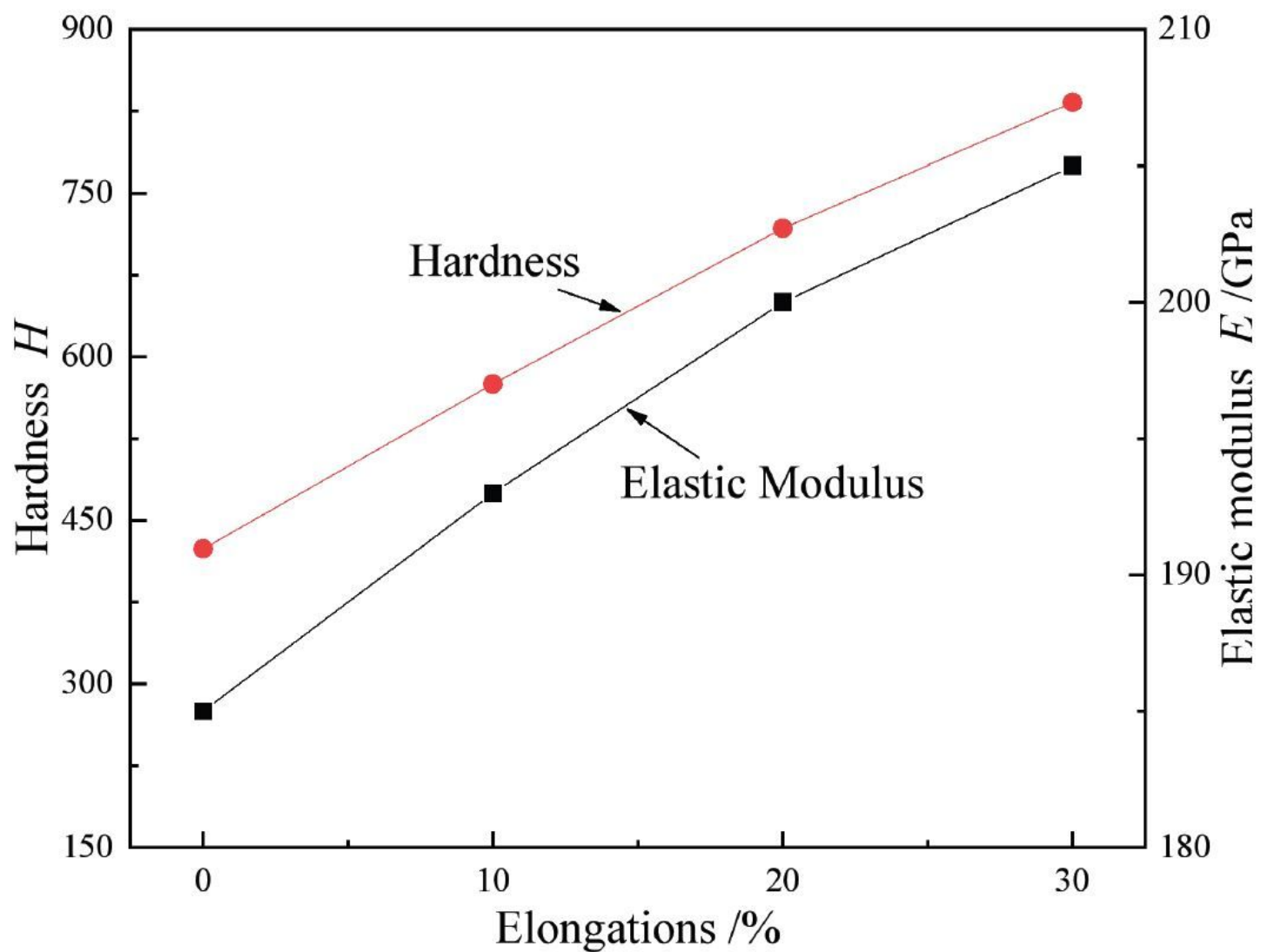
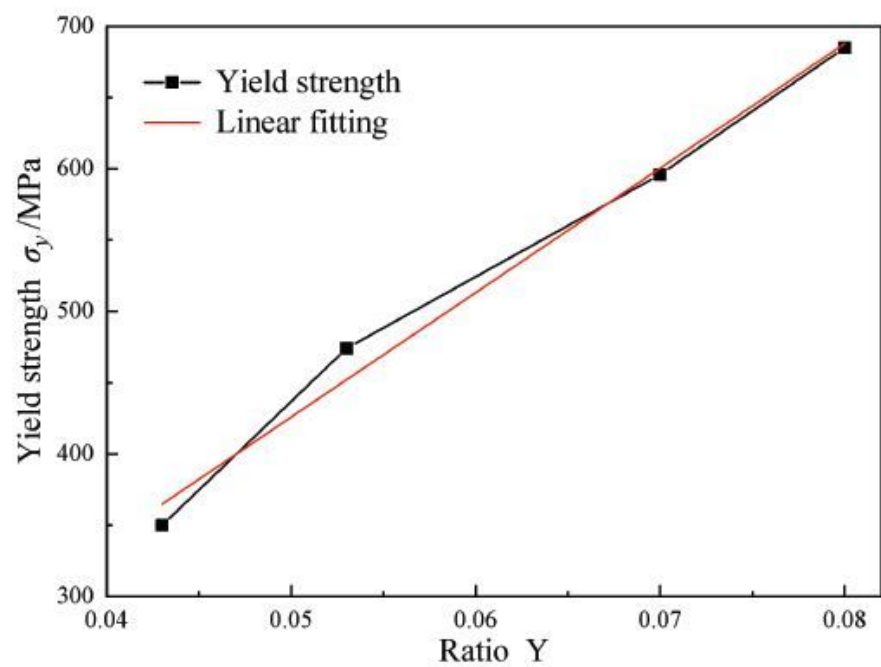


Figure 10

Change law of Elastic modulus and hardness under different elongations

a



b

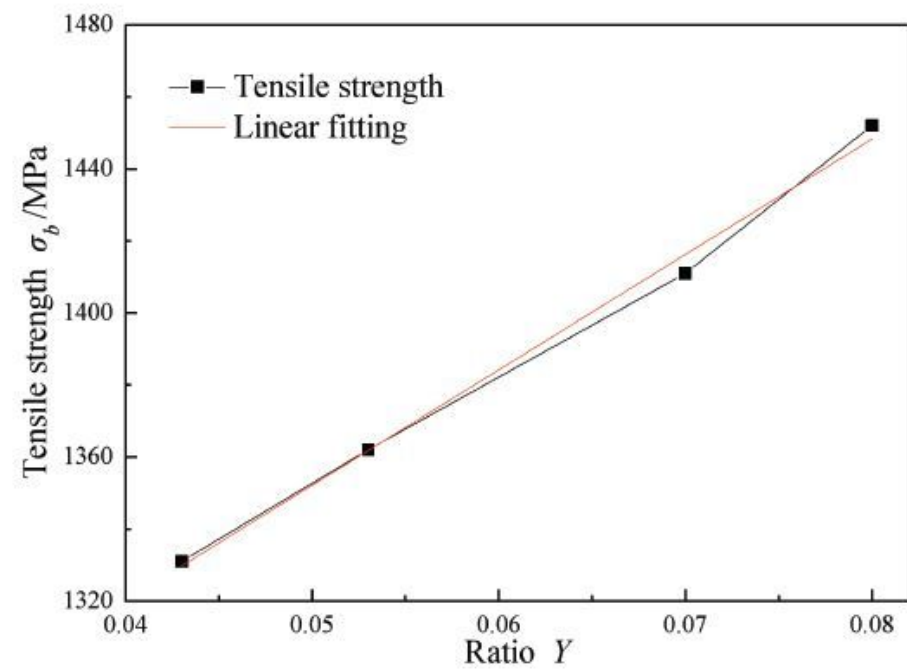


Figure 11

a Fitting curve of yield strength and ratio Y ; b fitting curve of tensile strength and ratio Y

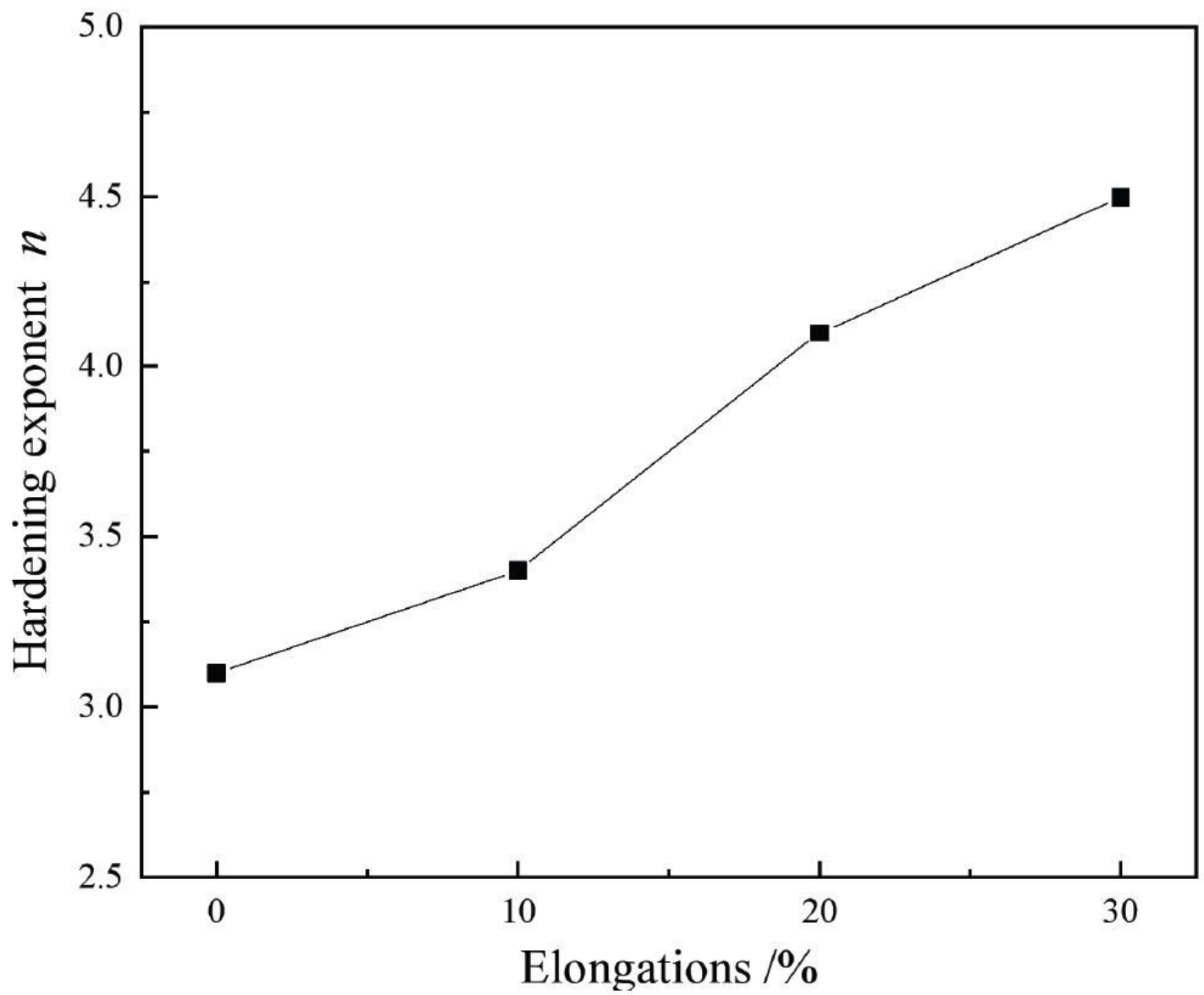


Figure 12

Change law of hardening exponent under different elongations

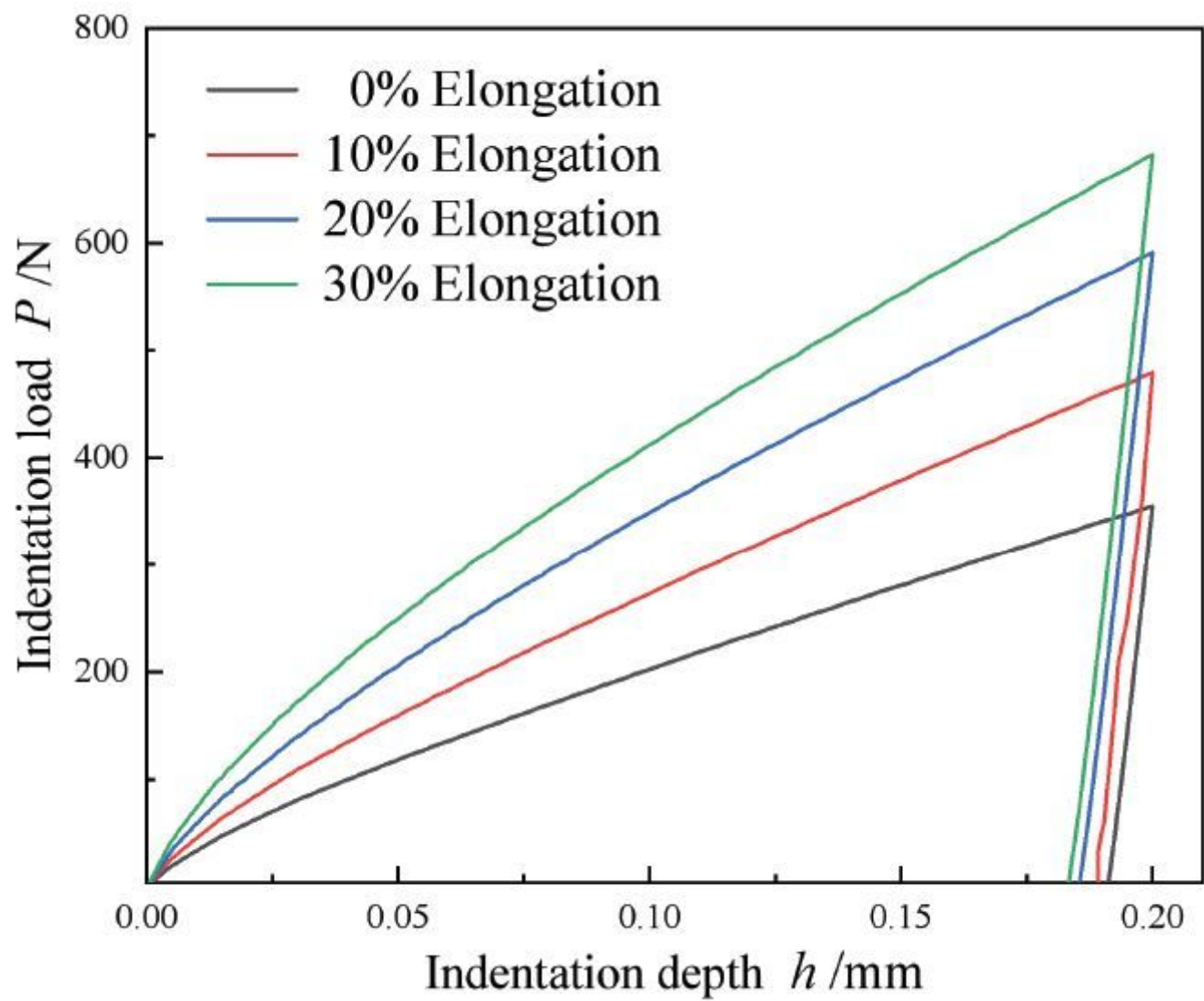


Figure 13

The load-depth curve obtained by finite element reversion under different elongations

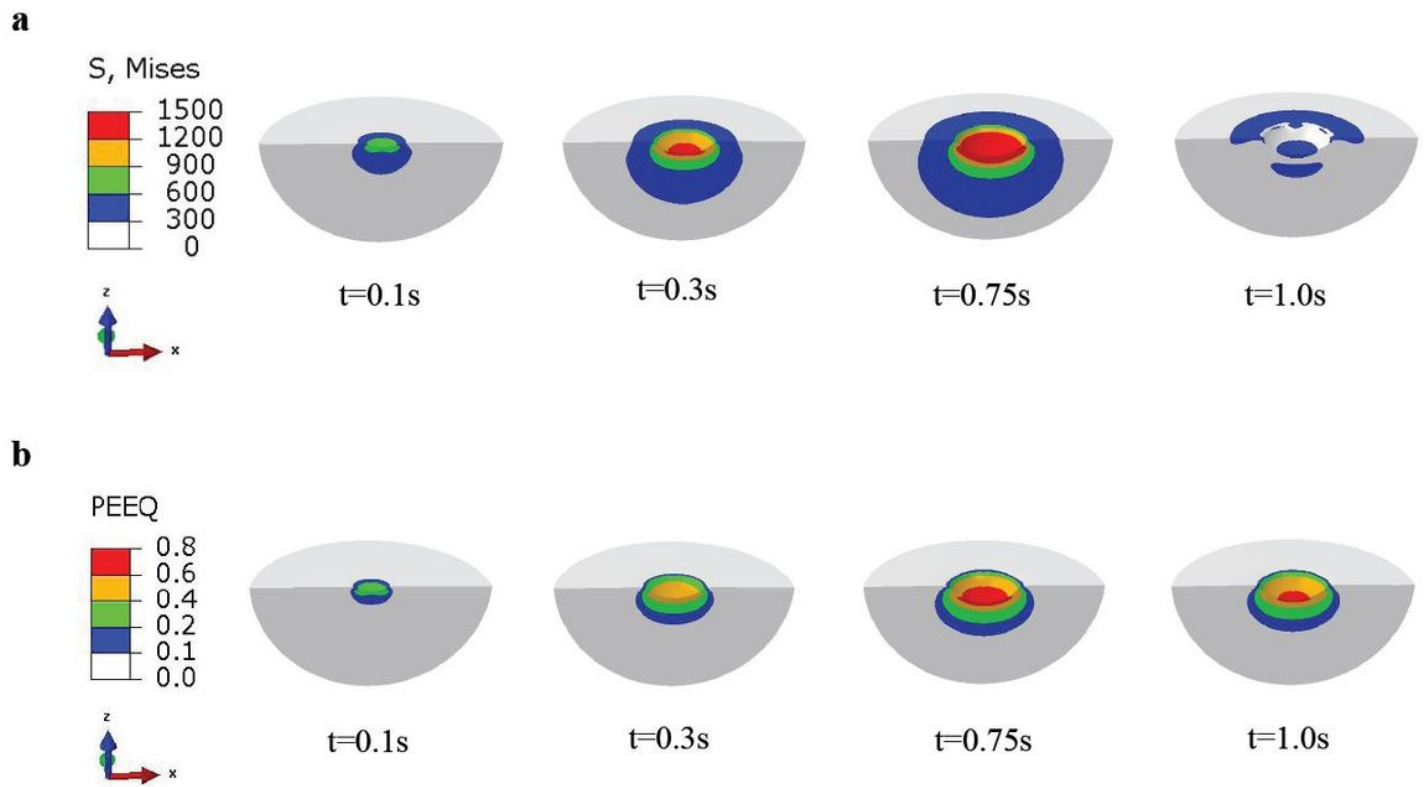


Figure 14

Mises stress of indentation process under 10% elongation; b equivalent plastic strain (PEEQ) of indentation process under 10% elongation

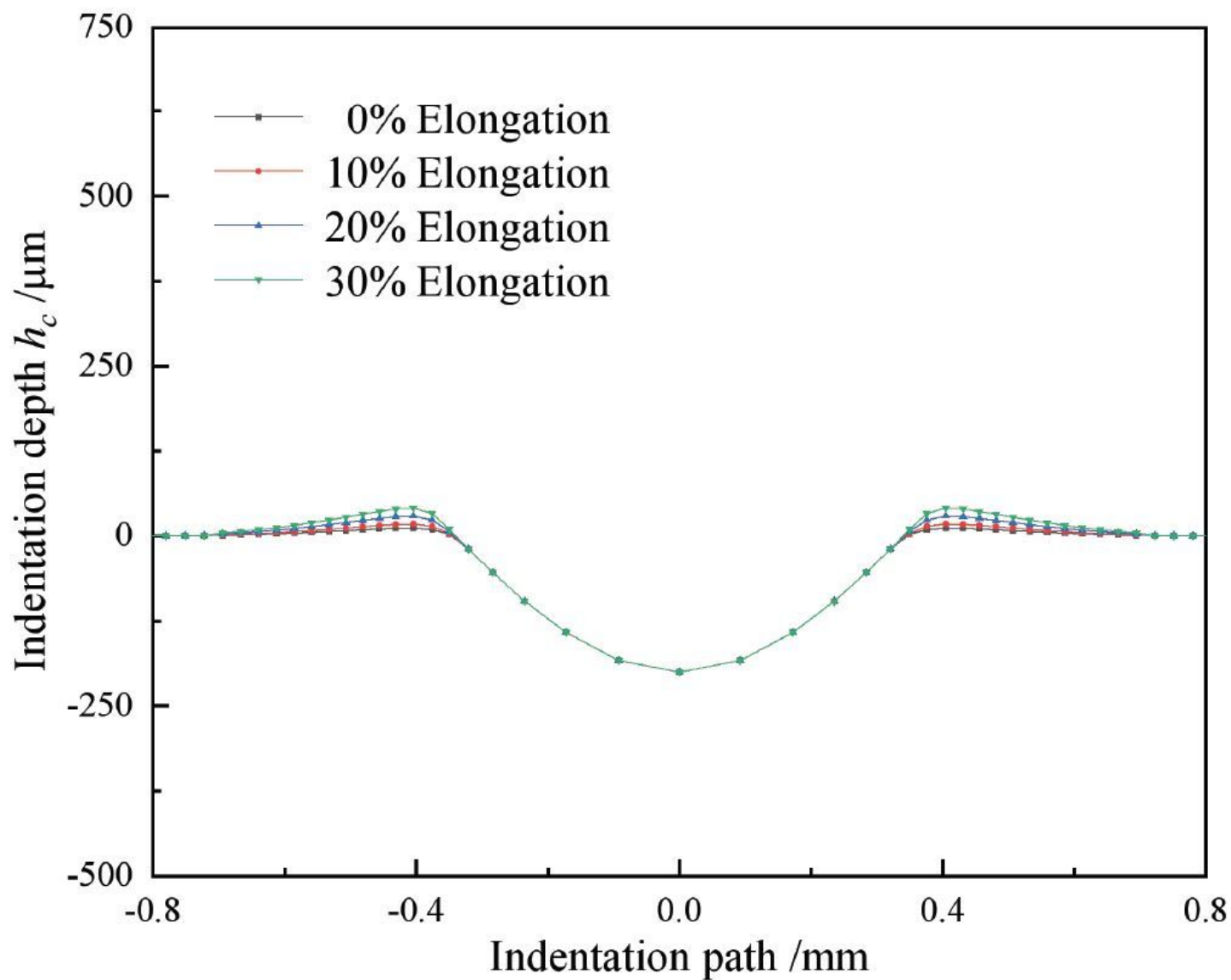


Figure 15

Comparison of maximum indentation morphology under different elongations

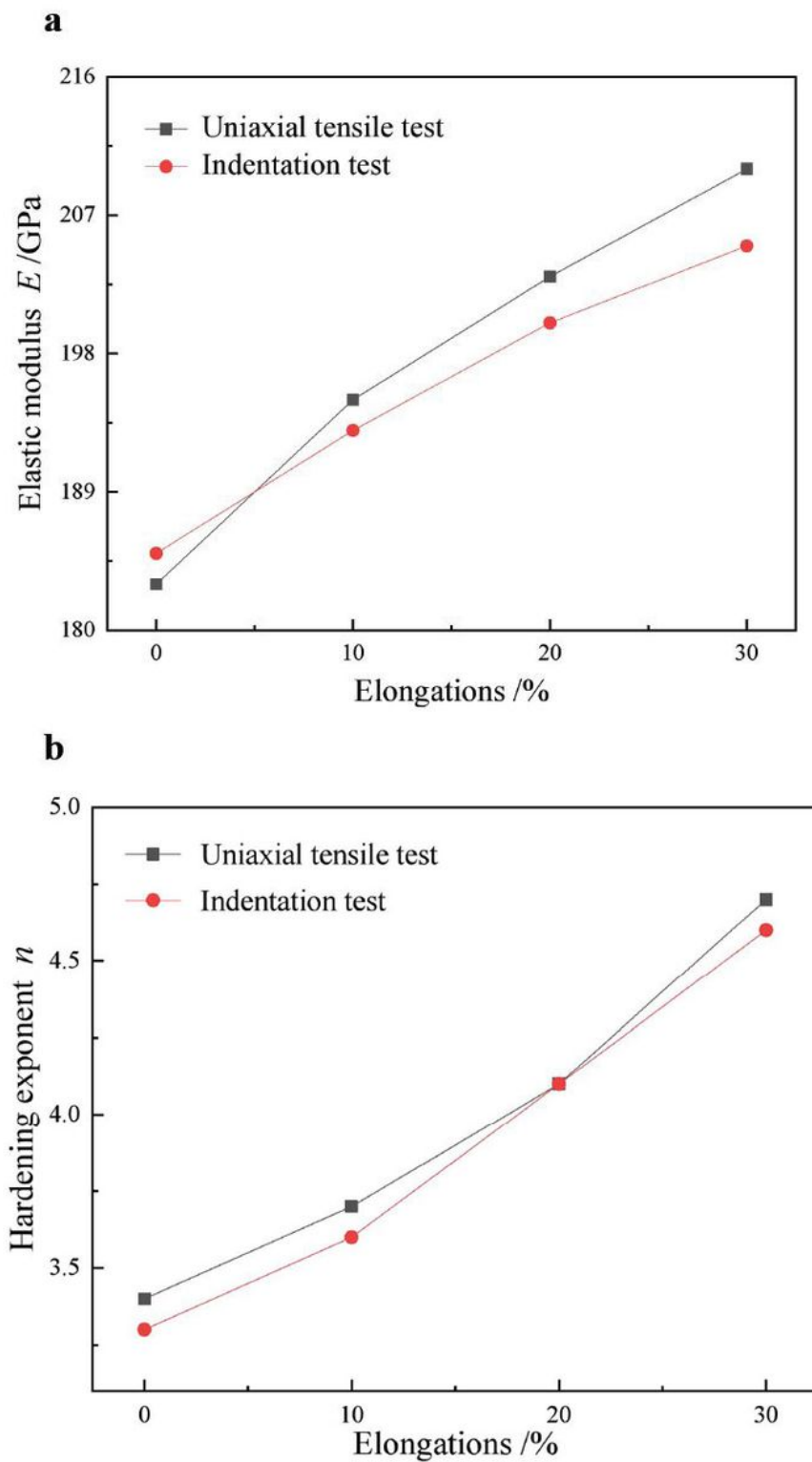


Figure 16

Comparison of mechanical parameters obtained by indentation test and tensile test under different elongations: a Elastic modulus; b hardening exponent

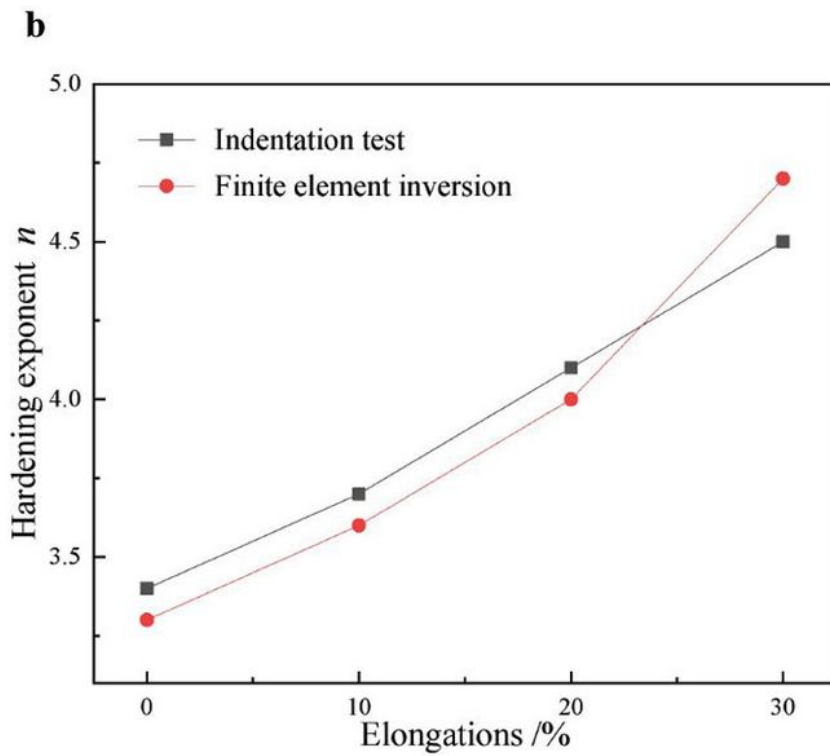
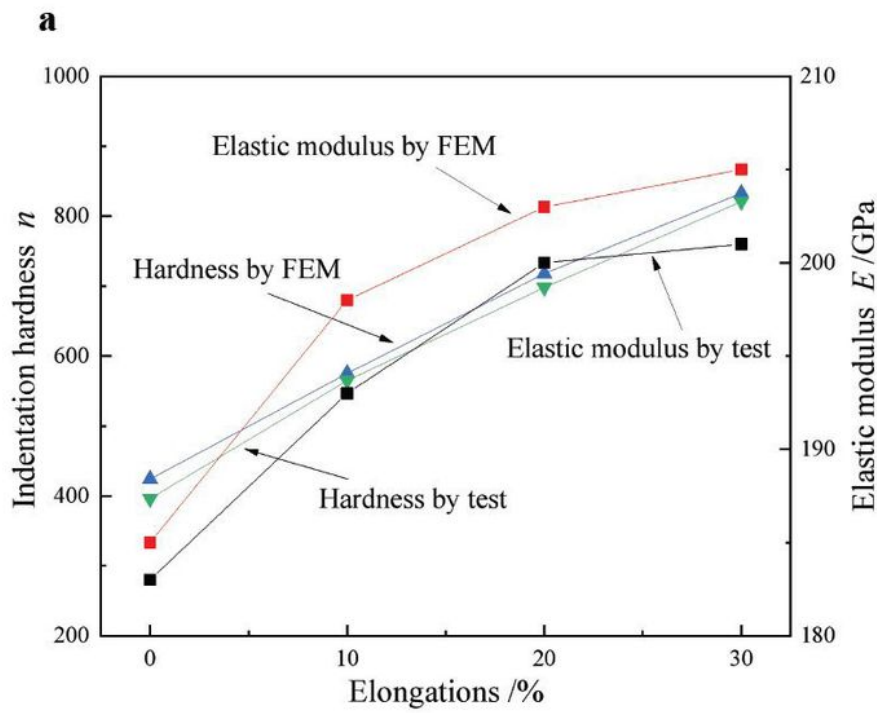


Figure 17

Comparison of mechanical parameters obtained by indentation test and finite element method with different elongations: a Elastic modulus and hardness; b hardening exponent