Rotational Stability of Proximally Unlocked Retrograde Femoral Nail In Damage Control Surgery – Biomechanical Study

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Research Article

Keywords: Unlocked intramedullary nailing, Damage control orthopaedics, Femoral shaft fractures, Temporary external fixation.

Posted Date: December 8th, 2021

DOI: https://doi.org/10.21203/rs.3.rs-1002602/v1

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Abstract

BACKGROUND: This biomechanical study was performed to look into the rotational stability of retrograde femoral intramedullary nail when it is used without proximal locking as a damage control device for management of femoral shaft fractures in emergency situations. This study compares this technique with the accepted methods for femoral shaft fixations in damage control surgeries. An alternative technique of using lateral compression screw to provide additional rotational stability is described.

METHODS: Experiments were divided into four different sets. Distally locked retrograde nail was passed across the fracture without any proximal fixation in set 1, a compression screw passed from lateral cortex in set 2, a proximal locking screw fixation in set 3. In set 4, Saw bone was fixed with external fixator.

The lateral compression screw group was further sub divided into three subgroups based on the amount of torque applied manually.

The torsion test was applied to create an rotational displacement of 10 degrees and the maximum load required to create the rotational displacement was noted.

RESULTS: Application of a compression screw improved the rotational stability significantly in comparison to no proximal locking. In the subgroup III of lateral compression screw application, the rotational stability was found to be equivalent to stability achieved with Nail with proximal locking and was found to be greater in comparison to external fixator application.

CONCLUSION: This study shows that the addition of a lateral compression screw significantly improves rotational stability and has the potential to be used in emergency lifesaving procedures.

Background

Proximally and distally locked intramedullary nailing (IMN) of femoral shaft fractures is accepted as the standard treatment as part of early total care (ETC) in the hemodynamically stable patient. Unfortunately, in hemodynamically unstable patients, this technique has been associated with greater morbidity and mortality [1,2,3]. Hence calls for less aggressive fixation methods were made. Currently, the use of external fixators as temporary fixation of these fractures as part of damage control orthopaedics (DCO) in these patients is accepted as the treatment of choice [2,4,5].

However, external fixation (EF) in these patients is far from ideal. It affords only partial fracture stability especially in the obese thigh with potential for medullary canal content embolization. Pin site infection is another major drawback that has significant bearing on future management options. Knee stiffness because of soft tissue splinting is a third problem. Nursing in intensive care units (ICU), especially if they have bilateral EF, is a major problem in these patients who require regular turning and physiotherapy. Other complications include continued bleeding from the fracture site and rare vascular injuries (6).
Finally, conversion to standard locked IMN nail is a major procedure that maybe associated with further complications and additional costs (7,8,9,10).

Recent studies have suggested the use of retrograde intramedullary femoral nail (RIMFN) as an alternative to EF as damage control device (11,12). A small diameter nail is passed gently without reaming and is only locked distally. Proximal locking is done at later stage once the patient's condition has stabilized. This technique has been found to be relatively safe, easy and quick. There is no need for a second major surgical procedure thereby minimizing the chance of the second hit associated with later IMN.

However, there are concerns with regards to the rotational stability of the fracture fixation where RIMFN has been used without proximal locking. One option is adding a lateral compression screw proximally, to improve the rotational stability of the construct.

To the authors knowledge there are no studies of the biomechanical performance of RIMFN of shaft fractures without proximal locking in terms of rotational stability.

The current experimental investigation was performed to evaluate the role of a proximal lateral compression screw in rotational stability compared to no proximal fixation and standard proximally locked nail. The rotational stability of nail was also compared with External fixation for this injury.

**Methods**

Twelve fourth generation Sawbones (made of fiber filled epoxy cortical shell and cancellous polyurethane core to mimic young human adult healthy femurs) measuring 455mm in length and reamed to an internal diameter of 13 mm (Sawbones Worldwide / Pacific Research Laboratories, Malmö, Sweden) were used. M/DN Femoral Retrograde Intramedullary nails (Zimmer-Biomet, Warsaw, Indiana, USA) length 380mm, and diameter 10mm, proximal screw size 4.2mm, distal screw size 5.5mm were used.

The femur was potted in a mounting fixture containing two customised iron boxes on either end and placed on a servo-hydraulic testing machine (SM1 MkII Torsion Testing Machine) for mechanical testing (Fig 1).

A torsion force was applied to create an rotational displacement of 10 degrees. No load was exerted axially along the femur during torsion testing, thus avoiding frictional resistance at the fracture site. The load/Torque applied was measured in Newton meters (Nm) using digital torque measuring machine (TeCQuipment E -101 Digital Measuring System)

Experiments were divided into four different sets of three saw bones each.

Group 1: Distally locked RIMFN passed across the fracture without any proximal fixation
Group 2: Distally locked RIMFN passed across the fracture with a 4.2mm blocking bolt (lateral compression screw) was passed through the lateral cortex to compress the nail against the medial cortex (Fig.2).

Group 3: Distally locked RIMFN passed across the fracture with one 4.2mm anterior to posterior proximal locking screw.

Group 4: Saw bone was fixed with external fixators, using two Schanz’s screws in each fragment.

Each set included three saw bones and for each mode of fixation the biomechanical testing was performed three times.

The nail was inserted through the intercondylar notch using the manufacturer’s recommended surgical technique. The nail-head was countersunk 2.0 mm relative to the base of the intercondylar notch. Two distal locking screws were inserted using the nail-mounted drill guide. A transverse osteotomy was performed 18cm above the articular surface ensuring free movement of the proximal fragment in relation the distal fragment-nail composite.

The lateral compression screw (4.2mm) was passed through the lateral cortex at proximal end of the nail (after predrilling the bone with 3.5mm drill) which was identified using an X ray (Fig 2). The torsion force required to introduce the screw was increased progressively in three sub groups of saw bones. In sub group I, after the screw was felt to come in contact with the nail in medullary canal, the screw was advanced for around two to three complete turns. In the second set of saw bones (subgroup II) the screw was advanced further for approximately three turns till the force required to advance the screw was felt to be sufficient to create enough force on the nail to prevent any rotatory moment of nail in the canal. In the third group (sub group III), the torque was applied to the screw till it could not be advanced any further.

The unilateral uniplanar fixator (Sharma Ortho System Pvt Limited, India) was used. Two 6 mm Schanz’s pins were inserted bicortically in each of the proximal and distal fragments. The core drill-holes were 4.5 mm. The pins were connected using a single rod of 11 mm diameter using rod to pin clamps.

Statistical analysis using independent paired T test with significance level of $P<0.05$ was performed.

**Results**

Table 1 shows the results of each individual reading.

**Table 1: Results of biomechanical tests (torque in Nm).**

The mean torsional loads required to create 10 degrees of rotational deformity in set 1, 2, 3, and 4 was 0.19, 1.03, 1.44, and 0.83, respectively. The standard deviation and standard error for each group are shown in Table 2.

Table 2. Mean Torque required to create 10 degrees of rotational displacement for each group.

<table>
<thead>
<tr>
<th></th>
<th>N</th>
<th>Mean (Torque Nm)</th>
<th>Std. Deviation</th>
<th>Std. Error Mean</th>
</tr>
</thead>
<tbody>
<tr>
<td>Nail (NPL)</td>
<td>9</td>
<td>0.1922</td>
<td>0.01563</td>
<td>0.00521</td>
</tr>
<tr>
<td>Nail (B)</td>
<td>9</td>
<td>1.037</td>
<td>0.3295</td>
<td>0.1098</td>
</tr>
<tr>
<td>Nail (PL)</td>
<td>9</td>
<td>1.4444</td>
<td>0.2870</td>
<td>0.0957</td>
</tr>
<tr>
<td>Ex Fix</td>
<td>9</td>
<td>0.8333</td>
<td>0.1240</td>
<td>0.0413</td>
</tr>
</tbody>
</table>

Torsional stability varied between the different groups. As expected, the nail without any proximal screws was found to be the least stable construct (Fig. 3). Application of lateral compression bolt improved the rotational stability significantly in comparison to no proximal locking (Fig. 4). Rotational stability with lateral compression screw was found to be higher than the external fixator group but the difference was not found to be statistically significant (Table 3).

**Table 3: Comparative analysis of all groups.**

<table>
<thead>
<tr>
<th></th>
<th>M</th>
<th>CI</th>
<th>Sig (2-tailed)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Pair 1</td>
<td>0.8444</td>
<td>0.6113 to 1.0775</td>
<td>0.00</td>
</tr>
<tr>
<td>Pair 2</td>
<td>0.2033</td>
<td>-0.454 to 0.4521</td>
<td>0.102</td>
</tr>
<tr>
<td>Pair 3</td>
<td>0.6411</td>
<td>0.5528 to 0.7294</td>
<td>0.00</td>
</tr>
<tr>
<td>Pair 4</td>
<td>0.6111</td>
<td>0.3902 to 0.8320</td>
<td>0.00</td>
</tr>
<tr>
<td>Pair 5</td>
<td>0.4078</td>
<td>0.0990 to 0.7166</td>
<td>0.01</td>
</tr>
</tbody>
</table>

**Pair 1:** Nail with Bolt (lateral compression screw) vs Nail without proximal screw. **Pair 2:** Nail with Bolt (lateral compression screw) vs External Fixator **Pair 3:** External fixator vs Nail without proximal screw **Pair 4:** Proximal locking screw vs External fixator **Pair 5:** Nail with Bolt (lateral compression screw) vs Proximal locking screw

*M:* Difference of means. *CI:* 95% Confidence Interval of difference in means.

Nail with proximal locking screw was found to be most stable rotationally.

On assessment of subgroups in the lateral compression screw group, the means in subgroup I, II and III were 0.800, 0.863 and 1.447 respectively (Table 4).

**Table 4: Mean Torque (Nm) in lateral compression screw sub groups**

<table>
<thead>
<tr>
<th>Sub group</th>
<th>Mean Torque required for 10 degrees of rotational displacement</th>
</tr>
</thead>
<tbody>
<tr>
<td>I</td>
<td>0.800</td>
</tr>
<tr>
<td>II</td>
<td>0.863</td>
</tr>
<tr>
<td>III</td>
<td>1.447</td>
</tr>
</tbody>
</table>

Mean torque in the subgroup III was found to be statistically higher in comparison to sub groups I and II (*P* value < .001). The subgroups were compared with external fixator group and with Nail with proximal locking group (Table 5).

**Table 5: Comparison of Means of sub groups in lateral compression screw with External fixator and Nail with proximal locking**
Nail (PL): Nail with proximal locking. Ex Fix: External fixator

Results showed that the mean torque of subgroup III of lateral compression screw was highest of all groups but it was not statistically more in comparison to Nail with proximal locking. In comparison to external fixator group, sub group III was found to be significantly stable in terms of rotational stability.

**Discussion**

This study employed mechanical testing to evaluate the rotational stability of various constructs used in the treatment of femoral fractures in polytrauma scenarios. The results showed that rotational stability was best achieved using a distally and proximally locked retrograde femoral nail. However, this construct is contraindicated in the hemodynamically unstable polytrauma patient where speed and minimal surgical trauma are of vital importance. In these patients, the current standard of care is application of EF with 2 screws in each fragment (4,5). This construct showed statistically significant lower rotational stability in comparison with the fully locked nail [Mean difference 0.61; 95%CI of difference = 0.39- 0.83; P= 0.00].

Traditionally external fixators have been used as damage control devices in polytrauma patients for femoral fixations. Recent studies of a modified protocol of retrograde nailing for damage control indicate it to be efficient, effective, and safe (11,12). However, passing a nail without proximal locking makes it rotationally unstable which has been a concern against the use of RIMFN as damage control device.

In order to improve the rotational stability, the authors propose the use of screw passed from lateral cortex proximally as a bolt. The screw pushes the nail against the far (medial) cortex and minimizes rotation of the nail in the medullary canal. This technique significantly improves the rotational strength in comparison to no proximal fixation (Fig 4). The mean force required to create the rotational displacement was lower in external fixators in comparison to this technique but this difference was not found to be statistically significant (Table 3). However, when the individual subgroups in lateral screw group were compared with other groups, the subgroup III was found to have highest rotational stability (Fig 5) though the difference in comparison to nail with proximal locking was found to have no statistical significance (Table 5).
This biomechanical study has shown that using a proximal lateral compression screw provides significant rotational stability and is a quick and simple procedure that can be used to temporarily provide rotational stability in emergency situations. Further, it requires only a single C arm exposure to identify the proximal end of the nail thereby decreasing the surgical time and at the same time providing significantly improved stability.

**Abbreviations**

ETC - Early total care  
IMN - Intramedullary nailing  
DCO - Damage control orthopaedics  
EF - External fixation  
ICU - Intensive care units  
RIMFN - Retrograde intramedullary femoral nail

**Declarations**

**Ethics approval and consent to participate:** Not applicable  
**Consent for publication:** Not applicable  
**Availability of data and materials:** All data generated or analysed during this study are included in this published article  
**Competing interests:** The authors declare that they have no competing interests  
**Funding:** This work was supported by Sultan Qaboos University Muscat Oman [RF/MED/SURG/19/01].  
**Acknowledgements:** Not applicable  
**Authors' contributions:**

**RM:** Involved in design and setting of the study. Performed biomechanical tests and collected the data, involved in writing of the manuscript  
**MHNZ:** Did the background research and was involved in design and setting of the study  
**KA:** Involved in designing the biomechanical tests protocol  
**AY:** Involved in writing of the manuscript
SAM: Involved in design and setting of the study. Involved in writing of the manuscript

References

Figures

Figure 1

Demonstrating the customized mounting fixture for the nail ends.
Figure 2

Image intensifier X-ray demonstrating the lateral compression screw application.
**Figure 3**

Mean Torque Nail (NPL): Nail with no proximal locking
Nail (B): Nail with bolt (lateral compression screw)
Nail (PL): Nail with proximal locking
Ex Fix: External fixator
Figure 4

Scatter diagram depicting the torque loads for Nail with no proximal lock and Nail with bolt (lateral compression screw). N.m: Newton meters
Figure 5

Demonstrating mean Torque values of subgroups in comparison to all groups Nail (NPL): Nail with no proximal locking. Nail (B): Nail with bolt (lateral compression screw). Nail (PL): Nail with proximal locking. Ex Fix: External fixator.